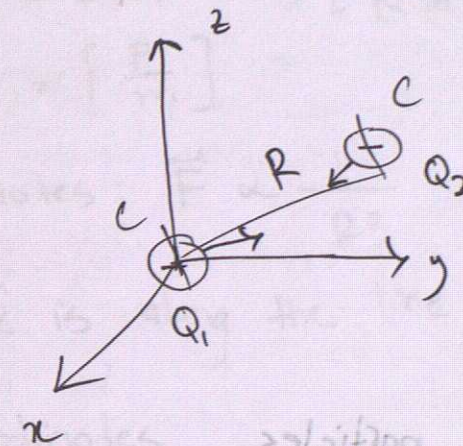


Maxwell's Equations

Faraday's Law: $\nabla \times \vec{E} = 0$

Ampere's Law: $\nabla \times \vec{H} = \vec{J}$

Coulomb's Law



$$|\vec{F}_e| = k \frac{Q_1 Q_2}{R^2}$$

- a) $|\vec{F}_e|$ depends on Q_1, Q_2
- b) $|\vec{F}_e| \propto \frac{1}{R^2}$ $\swarrow$ R is distance b/w Q_1, Q_2
- c) Direction of force $|\vec{F}_e|$ acted along line connecting Q_1, Q_2
- d) like charges: repel
opposite charges: attract

$$\vec{F}_e = k \frac{Q_1 Q_2}{R^2}$$

$\downarrow$ [N] $\downarrow$ [C²] $\downarrow$ [m²]

$$\vec{F}_e = \frac{Q_1 Q_2}{4\pi \epsilon_0 R^2}$$

$\epsilon_0 = 8.85 \times 10^{-12} \text{ (F/m)}$

permability for free space

$$\therefore k = \frac{1}{4\pi \epsilon_0}$$

Week 1: Lecture 1

Maxwell's Equations

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} \quad \nabla \cdot \vec{D} = \rho$$

$$\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t} \quad \nabla \cdot \vec{B} = 0$$

• under static conditions, $\vec{E}$ and $\vec{B}$ are decoupled

• math tools needed

↳ vector algebra

↳ vector calculus

Electric Charge

• an intrinsic characteristic of particles

making an object

→ same sign $\Rightarrow$ repel

→ opposite sign $\Rightarrow$ attract

call it "q" or "Q"

• charge can be transferred, but not created or destroyed

• unit charge

$$\text{electron} = -1.6 \times 10^{-19} \text{ [C]}$$

q_1

q_2

$\vec{F}$

Coulomb's Law

• gives the amount of force b/n two point charges:

$$\vec{F} = k \frac{q_1 q_2}{r^2} \hat{r} \quad k = \text{electrostatic constant}$$

$$= 8.99 \times 10^9 \approx 9 \times 10^9 \left[\frac{\text{N} \cdot \text{m}^2}{\text{C}^2} \right]$$

$\epsilon_0 = \text{permittivity}$

$$= 8.85 \times 10^{-12} \left[\frac{\text{C}^2}{\text{N} \cdot \text{m}^2} \right]$$

$$= \left[\frac{\text{F}}{\text{m}} \right]$$

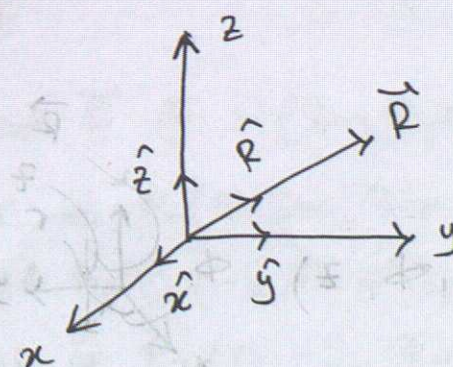
$$= \frac{1}{4\pi\epsilon_0}$$

• Notes: $\vec{F} \propto \frac{1}{r^2}$ and $F \propto q_1 q_2$

• $\hat{r}$ is along the line connecting q_1 and q_2

Coordinates

→ Cartesian (rectangular): (x, y, z)



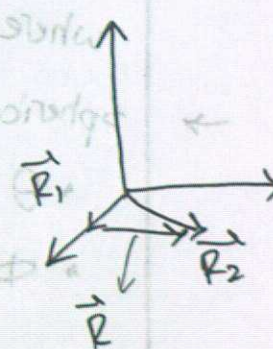
$$\vec{r} = x\hat{x} + y\hat{y} + z\hat{z}$$

$$\hat{r} = \frac{\vec{r}}{|\vec{r}|} = \frac{x\hat{x} + y\hat{y} + z\hat{z}}{\sqrt{x^2 + y^2 + z^2}}$$

→ Position vector: is a directed distance from origin to a point

• need to decide on $\begin{cases} \text{a common origin} \\ \text{a coordinate system} \end{cases}$

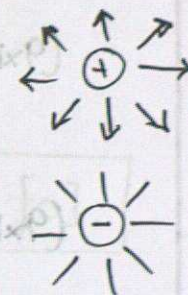
$$\text{e.g. } \vec{r}_1 = 8\hat{x} \text{ (m)} \quad \vec{r}_2 = 4\hat{x} + 8\hat{y} \text{ (m)}$$



Electric Field ($\vec{E}$)

- is a vector field defined in terms of electrostatic force ($\vec{F}$) that is exerted on a positive test charge (q) at every point in space

$$\vec{E} = \frac{\vec{F}}{q_0} = \frac{1}{4\pi\epsilon_0} \frac{q}{r^2} \hat{r} \quad [V/m] \text{ or } [N/C]$$



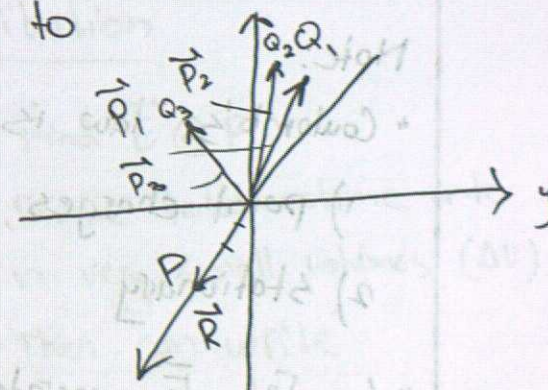
- $\vec{E}$ is one way to explain $\vec{F}$ by considering $\vec{E}$ around each charge
- Direction of $\vec{E}$ is same as $\vec{F}$ that acts on positive test charge
- Field exists regardless of q_0
- charge q (not test charge) is not affected by its own $\vec{E}$.

Ex: Find $\vec{E}$ @ $P(3m, 0, 0)$ due to

$Q_1 = 1\mu C$ @ $P_1(0, 2m, 3m)$

$Q_2 = -2\mu C$ @ $P_2(-2, 0, 3m)$

$Q_3 = 3\mu C$ @ $P_3(0, -2, 3m)$



Knownledge: $\vec{E}_{total} = \sum_{i=1}^3 \frac{Q_i}{4\pi\epsilon_0} \frac{(\vec{R} - \vec{R}_i)}{|\vec{R} - \vec{R}_i|^3}$

$k = 9 \times 10^9$

→ Distance Vector: is the separation b/n two points

e.g. $\vec{R} = \vec{R}_2 - \vec{R}_1$

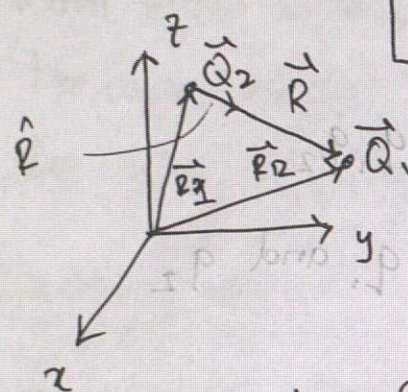
$= 4\hat{x} + 8\hat{y} - 8\hat{x} = -4\hat{x} + 8\hat{y} \text{ (m)}$

Electric Force

+ Coulomb's Law:

$$\vec{F} = \frac{1}{4\pi\epsilon_0} \frac{q_1 q_2}{r^2} \hat{r}$$

unit vector $\hat{r}$
distance r

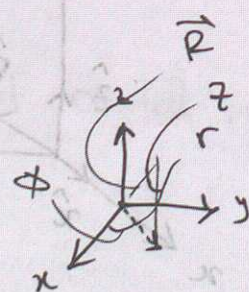


$$\vec{F} = \frac{1}{4\pi\epsilon_0} \frac{q_1 q_2}{|\vec{R}_2 - \vec{R}_1|^2} \frac{\vec{R}_2 - \vec{R}_1}{|\vec{R}_2 - \vec{R}_1|}$$

$$\vec{F} = \frac{1}{4\pi\epsilon_0} \frac{q_1 q_2}{|\vec{R}_2 - \vec{R}_1|^3} (\vec{R}_2 - \vec{R}_1)$$

units are [N]

$$\hat{r} = \frac{\vec{R}_2 - \vec{R}_1}{|\vec{R}_2 - \vec{R}_1|}$$



→ Cylindrical Coordinate: (r, ϕ, z)

$$\vec{R} = r\hat{r} + z\hat{z}$$

where $\hat{r} = \cos\phi\hat{x} + \sin\phi\hat{y}$

→ Spherical Coordinate: (R, θ, ϕ)

• θ is angle from (+)ve z-axis

• ϕ is angle from (+)ve x-axis (on xy plane)

$$\vec{R} = 3\hat{x}, \vec{R}_1 = 2\hat{y} + 3\hat{z}, \vec{R}_2 = -2\hat{x} + 3\hat{z}, \vec{R}_3 = -2\hat{y} + 3\hat{z}$$

$$\vec{E} = (9 \times 10^9)(10^{-6}) \frac{3\hat{x} + 2\hat{y} - 3\hat{z}}{(\sqrt{3^2 + 2^2 + 3^2})^3} +$$

$$(9 \times 10^9)(-2 \times 10^{-6}) \frac{3\hat{x} + 2\hat{x} - 3\hat{z}}{(\sqrt{3^2 + 2^2 + 3^2})^3} +$$

$$(9 \times 10^9)(3 \times 10^{-6}) \frac{3\hat{x} + 2\hat{y} - 3\hat{z}}{(\sqrt{3^2 + 2^2 + 3^2})^3}$$

$$\vec{E} = 591.8\hat{x} + 348.4\hat{y} - 773.1\hat{z} \left[\frac{V}{m} \right] \text{ or } \left[\frac{N}{C} \right]$$

H.W.

Ex: $\vec{E} = ?$ @ $P(3m, 0^\circ, 0m)$ (cylindrical coordinates)

$$Q_1 = 1\mu C @ P_1(2m, 90^\circ, 3m)$$

$$Q_2 = -2\mu C @ P_2(2m, 180^\circ, 3m)$$

$$Q_3 = 3\mu C @ P_3(2m, 270^\circ, 3m)$$

Note:

* Coulomb's law is valid if charges are:

1) point charges, and

2) stationary

* So far, $\vec{E}$ generated by a single point charge

* How about $\left\{ \begin{array}{l} \rightarrow \text{line charge} \\ \rightarrow \text{surface charge} \\ \rightarrow \text{volume charge} \end{array} \right\} \rightarrow \left\{ \begin{array}{l} \text{uniform} \\ \text{non uniform} \end{array} \right.$

charge distribution in 3D $\left\{ \begin{array}{l} \text{rect.} \\ \text{cylind.} \\ \text{sph.} \end{array} \right.$

Charge Densities

* at atomic scale, charge distribution is discrete

$$\rho_v = \lim_{\Delta V \rightarrow 0} \frac{\Delta q}{\Delta V} = \frac{dq}{dV} \Rightarrow dq = \rho_v dV$$

↳ volume charge density

then total charge $q = \int_V \rho_v dV = \iiint \rho_v dV [C]$

if ρ_v is uniform, $q = \rho_v V [C]$

* surface charge density (ρ_s) (C/m^2)

$$\rho_s = \lim_{\Delta s \rightarrow 0} \frac{\Delta q}{\Delta s} = \frac{dq}{ds} \Rightarrow q = \int_s \rho_s ds [C]$$

* line charge density (ρ_l) (C/m)

$$\rho_l = \lim_{\Delta l \rightarrow 0} \frac{\Delta q}{\Delta l} = \frac{dq}{dl} \Rightarrow q = \int_l \rho_l dl [C]$$

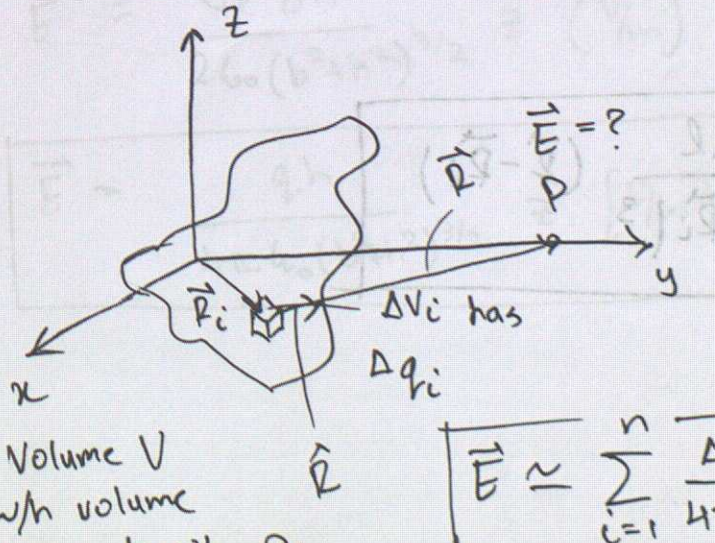
4.3.2

Electric Field due to a Charge Distribution

- Find $\vec{E}$ @ P

- Divide total volume into n very small volumes (ΔV)

- Then can write



$\Delta q = \rho_v \Delta V$ and

$$\vec{E} \approx \sum_{i=1}^n \frac{\Delta q_i}{4\pi\epsilon_0 |\vec{R} - \vec{R}_i|^3} (\vec{R} - \vec{R}_i)$$

Volume V w/ volume charge density ρ_v

• at the limit when

$n \rightarrow \infty \Rightarrow \Delta V = dV$ and E becomes exact to
 $\Delta q = dq$

$$\Rightarrow \vec{E} = \lim_{n \rightarrow \infty} \sum_{i=1}^n \frac{\Delta q_i}{4\pi\epsilon_0 |\vec{r} - \vec{r}_i|^3} (\vec{r} - \vec{r}_i)$$

$$\vec{E} = \frac{1}{4\pi\epsilon_0} \int_V \frac{\rho dV}{|\vec{r} - \vec{r}_i|^3} (\vec{r} - \vec{r}_i) \quad \text{where } dq = \rho dV$$

$$\vec{E} = \frac{1}{4\pi\epsilon_0} \iiint_V \frac{\rho dV}{|\vec{r} - \vec{r}_i|^3} (\vec{r} - \vec{r}_i) \quad \left[\frac{V}{m} \right]$$

• similarly, $\vec{E}$ due to surface charge distribution

$$\vec{E} = \frac{1}{4\pi\epsilon_0} \iint_S \frac{\rho_s dS}{|\vec{r} - \vec{r}_i|^3} (\vec{r} - \vec{r}_i)$$

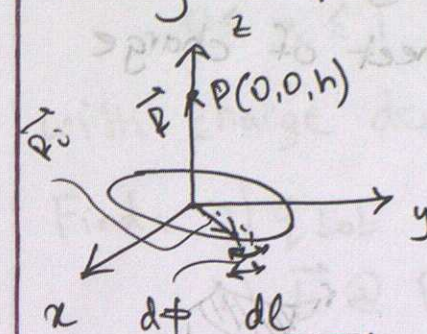
• for line

$$\vec{E} = \frac{1}{4\pi\epsilon_0} \int_L \frac{\rho_l dl}{|\vec{r} - \vec{r}_i|^3} (\vec{r} - \vec{r}_i)$$

Week 1: lecture 3

Jan 10, 2024

Ex: A ring of radius b and uniform line charge density of positive ρ_l , find $\vec{E}$ @ $P(x,y,z) = (0,0,h)$



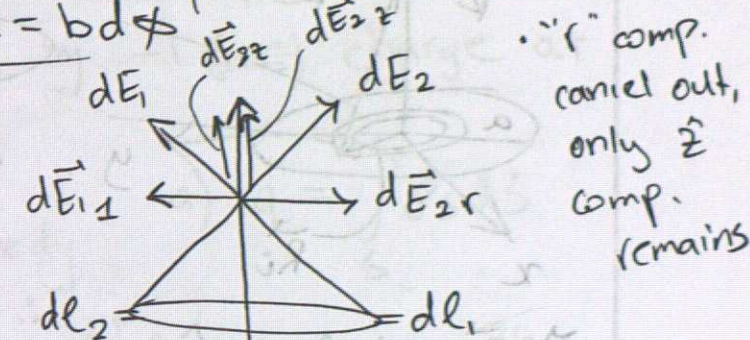
$$d\vec{E} = \frac{1}{4\pi\epsilon_0} \frac{\rho_l dl}{|\vec{r} - \vec{r}_i|^3} (\vec{r} - \vec{r}_i)$$

need dl , $\vec{r}$, and $\vec{r}_i$

$$dq = \rho_l dl$$

$$dl = b d\phi$$

$$\vec{r} - \vec{r}_i = h\hat{z} - b\hat{r} = -b\hat{r} + h\hat{z}$$



"r" comp. cancel out, only $\hat{z}$ comp. remains

$$d\vec{E} = \frac{1}{4\pi\epsilon_0} \frac{\rho_l b d\phi}{(b^2 + h^2)^{3/2}} (-b\hat{r} + h\hat{z})$$

0, cancels out

$$\vec{E} = \frac{\rho_l b h}{4\pi\epsilon_0 (b^2 + h^2)^{3/2}} \int_0^{2\pi} d\phi \hat{z}$$

recall $q = 2\pi b \rho_l$

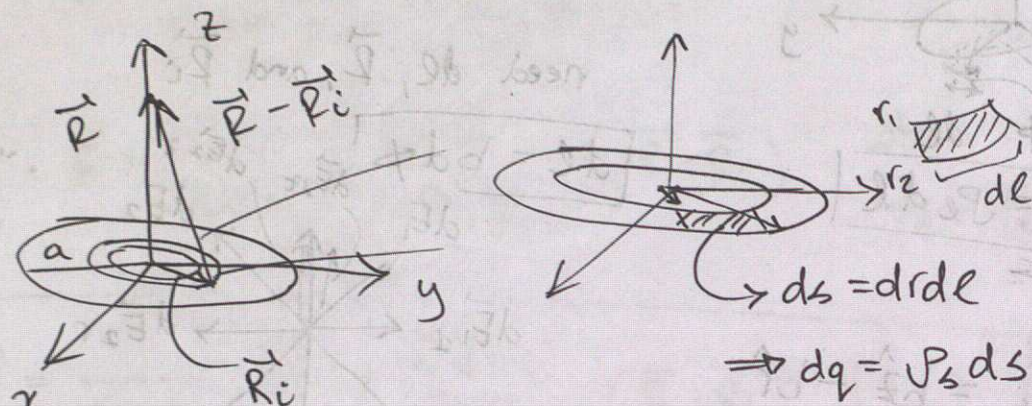
$$\vec{E} = \frac{\rho_l b h}{2\epsilon_0 (b^2 + h^2)^{3/2}} \hat{z} \quad \left[\frac{V}{m} \right]$$

$$\Rightarrow \rho_l = \frac{q}{2\pi b}$$

$$\vec{E} = \frac{qh}{4\pi\epsilon_0 (b^2 + h^2)^{3/2}} \hat{z} \quad \left[\frac{V}{m} \right]$$

electric field in terms of "q" instead of charge density

- Ex: Find $\vec{E}$ @ $P=(0,0,h)$ due to a disk of radius a and uniform charge density distribution ρ_s then evaluate $\vec{E}$ due to infinite sheet of charge density ρ_s by letting $a \rightarrow \infty$



$$\vec{r} - \vec{r}_i = h\hat{z} - r\hat{r}$$

$$= -r\hat{r} + h\hat{z}, \text{ we know } d\vec{E} = \frac{1}{4\pi\epsilon_0} \frac{\rho_s ds}{|\vec{r} - \vec{r}_i|^3} (\vec{r} - \vec{r}_i)$$

$$d\vec{E} = \frac{\rho_s}{4\pi\epsilon_0} \frac{-r\hat{r} + h\hat{z}}{(r^2 + h^2)^{3/2}} r dr d\phi$$

0 due to symmetry

$$d\vec{E} = \frac{\rho_s}{4\pi\epsilon_0} \frac{h}{(r^2 + h^2)^{3/2}} r dr d\phi$$

$$\vec{E} = \frac{\rho_s h}{4\pi\epsilon_0} \int_0^a \int_0^{2\pi} \frac{r}{(r^2 + h^2)^{3/2}} dr d\phi$$

$$= \frac{\rho_s h}{2\epsilon_0} \int_0^a \frac{r dr}{(r^2 + h^2)^{3/2}}$$

$$\Rightarrow \vec{E} = \frac{\rho_s}{2\epsilon_0} \left[1 - \frac{h}{\sqrt{a^2 + h^2}} \right] \hat{z} \quad [V/m]$$

Ex: Given that sheet of

$$0 \leq x \leq 1 \text{ (m)} \text{ on } z=0 \text{ plane}$$

$$0 \leq y \leq 1$$

with charge density of $\rho_s = xy(x^2 + y^2 + 25)^{3/2} \left[\frac{nC}{m^2} \right]$

Find: a) q_{tot}

b) $\vec{E}$ @ $P(0,0,5)$ m

c) force experienced by -1 charge at $(0,0,5)$ m

a) $q = \int \rho_s ds$

$ds = dx dy$

$q = \int_0^1 \int_0^1 xy(x^2 + y^2 + 25)^{3/2} dx dy$

$q = 33.15 \text{ [nC]}$

b) $d\vec{E} = \frac{\rho_s ds}{4\pi\epsilon_0 |\vec{r} - \vec{r}_i|^3} (\vec{r} - \vec{r}_i)$

$$\vec{r} - \vec{r}_i = 5\hat{z} - (x\hat{x} + y\hat{y}) = -x\hat{x} - y\hat{y} + 5\hat{z}$$

$$d\vec{E} = \frac{\rho_s dx dy}{4\pi\epsilon_0 (x^2 + y^2 + 25)^{3/2}} (-x\hat{x} - y\hat{y} + 5\hat{z})$$

$$d\vec{E} = \frac{xy(x^2 + y^2 + 25)^{3/2}}{4\pi\epsilon_0 (x^2 + y^2 + 25)^{3/2}} (-x\hat{x} - y\hat{y} + 5\hat{z}) dx dy$$

$$\vec{E} = -1.5\hat{x} - 1.5\hat{y} + 11.25\hat{z} \quad [V/m]$$

Today: Gauss' Law

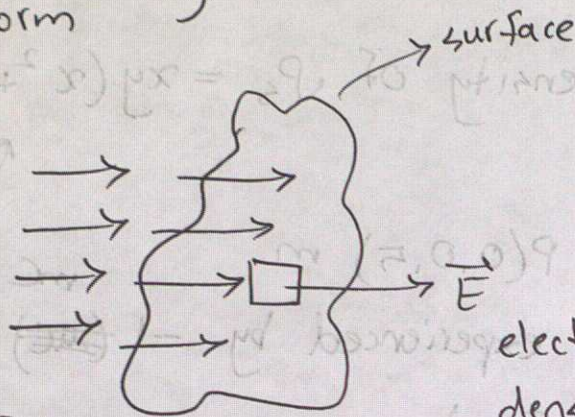
- integral form
- point form

examples

Consider:

electric field intensity

$$\left[\frac{N}{C} \right] \text{ or } \left[\frac{V}{m} \right]$$



electric field

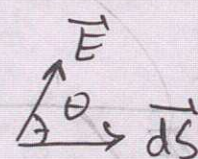
density $\vec{D}$ [C/m^2]

$$\vec{D} = \epsilon_0 \vec{E}$$

- * Find out how much $\vec{E}$ comes out

if $\theta = 0 \rightarrow \text{max flux}$

$\theta = 90^\circ \rightarrow 0 \text{ flux}$



$$\Rightarrow \boxed{E dS \cos \theta = \vec{E} \cdot d\vec{S}}$$

Gauss's Law (1777-1855)

- * constitutes one of the fundamental laws of electromagnetism

- * states that total electric flux (Φ , Ψ) through any closed surface is equal to the total charge enclosed by that surface (Gaussian surface)

$$\boxed{\Phi = Q_{enc}} \quad \boxed{\Phi = \oint_S \vec{D} \cdot d\vec{S}} \rightarrow$$

$$\boxed{\oint_S \vec{D} \cdot d\vec{S} = Q_{enc}} \Rightarrow \boxed{\epsilon_0 \oint_S \vec{E} \cdot d\vec{S} = Q_{enc}} \quad \text{integral form of Gauss Law}$$

$\vec{D} = \epsilon_0 \vec{E}$

Differential Form Gauss Law

- * first Maxwell equation

$$\boxed{\vec{\nabla} \cdot \vec{D} = \rho_V}$$

"divergence" of $\vec{D}$ is ρ_V
now let's derive integral form from here

$$\int_V \vec{\nabla} \cdot \vec{D} dV = \int_V \rho_V dV \quad \text{①}$$

$$\text{and we know } \int_V \rho_V dV = Q_{enc, tot} \quad \text{②}$$

now apply divergence theorem (aka Gauss's theorem)

- * states that closed surface integral of a vector equals the volume integral of the divergence of the vector

$$\int_V \vec{\nabla} \cdot \vec{A} dV = \oint_S \vec{A} \cdot d\vec{S} \Rightarrow \text{can write } \int_V \vec{\nabla} \cdot \vec{D} dV = \oint_S \vec{D} \cdot d\vec{S} \quad \text{③}$$

- * combining ①, ②, and ③

$$\Rightarrow \boxed{\oint_S \vec{D} \cdot d\vec{S} = Q_{enc}}$$

voila! integral form

Notes: depending on convenience, I can go back and forth b/n forms

- * Gauss's law is an alternative form of Coulomb's law
- * is more convenient to use when symmetry exists

Gaussian Surface

- + hypothetical surface
- + must enclose all the space I care about
- + must make use of symmetry

Ex: uniformly charged sphere

- radius a [m]
- uniform charge density ρ_v [C/m³]
- Find $\vec{E}$ everywhere



Knowing $\oint \vec{E} \cdot d\vec{s} = Q_{enc}$

$$Q_{enc} = \int_V \rho_v dv = \rho_v \int_V dv = \rho_v \frac{4}{3} \pi r^3 [C]$$

$$\oint \vec{E} \cdot d\vec{s} = Q_{enc} \Rightarrow \oint |\vec{E}| ds = Q_{enc}$$

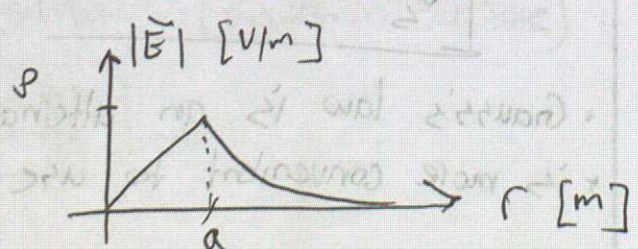
$$\epsilon_0 E \cdot 4\pi r^2 = \rho_v \frac{4}{3} \pi r^3 \Rightarrow \vec{E} = \frac{\rho_v}{3\epsilon_0} r \hat{r} [V/m]$$

since $\vec{D} = \epsilon_0 \vec{E} \Rightarrow \vec{D} = \frac{\rho_v}{3} r \hat{r}$

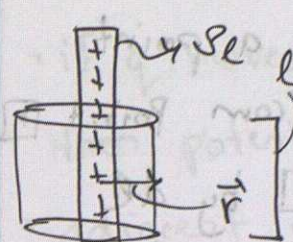
$$Q_{enc} = \rho_v \frac{4}{3} \pi a^3$$

$$\epsilon_0 E 4\pi r^2 = \rho_v \frac{4}{3} \pi a^3$$

$$\therefore \vec{E} = \begin{cases} \frac{\rho_v}{3\epsilon_0} r \hat{r} & 0 < r < a \\ \frac{\rho_v}{3\epsilon_0} a \hat{r} & r = a \\ \frac{\rho_v a^3}{3\epsilon_0} \cdot \frac{1}{r^2} \hat{r} & r > a \end{cases}$$



Ex: Infinite line charge with density charge ρ_l [C/m]



Find $\vec{E}$ @ distance r

$$\oint \vec{E} \cdot d\vec{s} = Q_{enc} \Rightarrow \vec{E} = \frac{\rho_l}{2\pi\epsilon_0} \cdot \frac{1}{r} \hat{r} [V/m]$$

$$\epsilon_0 E (2\pi r l) = \rho_l l$$

Note: contributions from top+bottom = 0 since $\vec{E}$ is tangential to surface

Ex: Thin spherical shell with $Q_{tot} = +q$

Find $\vec{E}$ everywhere

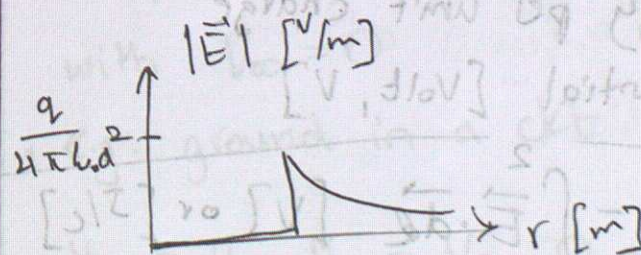
$$\oint \vec{E} \cdot d\vec{s} = Q_{enc}$$

inside: $r < a$

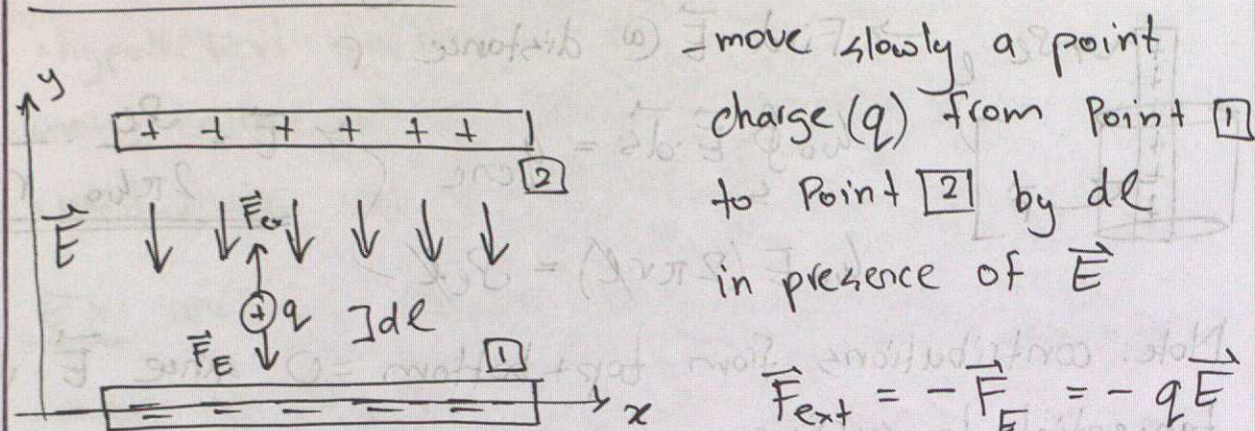
$$Q_{enc} = 0 \Rightarrow \vec{E} = 0$$

$$\text{outside: } r > a \Rightarrow \epsilon_0 E 4\pi r^2 = q \Rightarrow \vec{E} = \frac{q}{4\pi\epsilon_0} \cdot \frac{1}{r^2} \hat{r} [V/m]$$

$$\text{on: } r = a \Rightarrow \vec{E} = \frac{q}{4\pi\epsilon_0 a^2} \hat{r} [V/m]$$



Electric Potential



$$dW = -\vec{F}_E \cdot d\vec{l}$$

* Note: negative sign indicates that work is done by an external agent

* Knowing $\vec{F}_E = q\vec{E} \Rightarrow dW = -q\vec{E} \cdot d\vec{l}$

$$W = -q \int_{\text{initial}}^{\text{final}} \vec{E} \cdot d\vec{l} \quad \leftarrow \text{electric potential energy [J]}$$

Electric Potential (aka voltage, potential)

* Electric potential energy per unit charge is called electric potential [Volt, V]

$$V_{21} = V_2 - V_1 = \frac{W}{q} = - \int_1^2 \vec{E} \cdot d\vec{l} \quad [V] \text{ or } [J/C]$$

Equipotential Surfaces

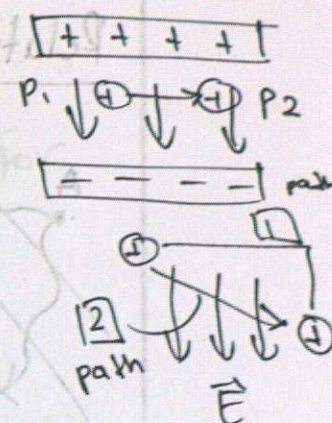
* if q moves along surface $\perp$ to $\vec{E}$, then potential doesn't change

* adjacent points ^{with} the same electric potential make equipotential surface

* hence work done by electrostatic force = 0 in going from P_1 to P_2

* Note: work done by electrostatic force is independent of path ... taking path 1 or 2 are same

* do example on 4-8 page 184



Relative Potential

$$V_{21} = V_2 - V_1 = - \int_1^2 \vec{E} \cdot d\vec{l} \quad \text{is the voltage b/n two points}$$

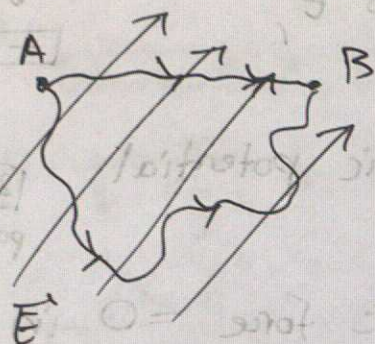
Absolute Potential

* is potential w.r.t. a reference considered at infinity with $V_{\infty} = 0$

* e.g: ground in a ckt

$$V_{21} = V_2 - V_1 = V_2 - 0 \Rightarrow V = - \int_{\infty}^2 \vec{E} \cdot d\vec{l}$$

Relation B/n E and V (Maxwell's Equ.)



* Consider, knowing that potential gain is independent of path

$$V_{AB} + V_{BA} = 0$$

* recognize that physically that no net work is done in moving q along any closed path

$$\oint_C \vec{E} \cdot d\vec{\ell} = 0$$

$\vec{E}$ is conservative field
"aka KVL"

Stoke's Theorem

* surface integral of curl of a vector field over a surface bounded by a closed path is equal to the line integral of the vector around that path

$$\oint_C \vec{E} \cdot d\vec{\ell} = \int_S (\nabla \times \vec{E}) \cdot d\vec{S}$$

* knowing $\oint_C \vec{E} \cdot d\vec{\ell} = 0 \Rightarrow \boxed{\nabla \times \vec{E} = 0}$

* point form of 2nd Maxwell equation for static electric field

Derive $\vec{E}$ from V

* dV b/n two points separated by $d\vec{\ell}$ in presence of $\vec{E}$ is $dV = -\vec{E} \cdot d\vec{\ell}$

* $\vec{E}$ in cartesian coordinate $\rightarrow$ plug into here

$$\vec{E} = E_x \hat{x} + E_y \hat{y} + E_z \hat{z}$$

$$\Rightarrow dV = -(E_x \hat{x} + E_y \hat{y} + E_z \hat{z}) \cdot (dx \hat{x} + dy \hat{y} + dz \hat{z})$$

$$dV = -(E_x dx + E_y dy + E_z dz)$$

$$\text{implies } E_x = -\frac{\partial V}{\partial x} \quad E_y = -\frac{\partial V}{\partial y} \quad E_z = -\frac{\partial V}{\partial z}$$

$$\vec{E} = E_x \hat{x} + E_y \hat{y} + E_z \hat{z} = -\left(\frac{\partial V}{\partial x} \hat{x} + \frac{\partial V}{\partial y} \hat{y} + \frac{\partial V}{\partial z} \hat{z}\right)$$

$$\boxed{\vec{E} = -\nabla V} \rightarrow \text{gradient of } V$$

* physically, (-)ve sign implies that if V increases as $+q$ moves along a path, then $\vec{E}$ has an opposite direction

Poisson's Equation

+ recall $\nabla \cdot \vec{D} = \rho_v$ (point form of Gauss Law)

$$\vec{D} = \epsilon_0 \vec{E} \Rightarrow \nabla \cdot \vec{E} = \frac{\rho_v}{\epsilon_0}$$

+ knowing $\vec{E} = -\nabla V$

$$\nabla \cdot (-\nabla V) = \frac{\rho_v}{\epsilon_0}$$

$$\boxed{\nabla^2 V = -\frac{\rho_v}{\epsilon_0}}$$

$$\left(\nabla^2 V = \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2} \right)$$

$$\text{where } V = \frac{1}{4\pi\epsilon_0} \int \frac{\rho_v}{R'} dv$$

+ if charge is zero in a region, then
if $\rho = 0 \Rightarrow \rho_v = 0$

$$\Rightarrow \boxed{\nabla^2 V = 0} \leftarrow \text{Laplace's Equation}$$

Week 2: Lecture 3

Jan 17, 2025

Ex: Given $V = \frac{10}{r^2} \sin\theta \cos\phi$

a) Find $\vec{D}$ @ $(2, \frac{\pi}{2}, 0)$

b) Find work done in moving $10 \mu\text{C}$ point charge from point A $(1, 30^\circ, 120^\circ)$ to B $(4, 90^\circ, 60^\circ)$

a) $\vec{D} = \epsilon_0 \vec{E}$, $\vec{E} = -\nabla V$

$$\nabla = \left(\frac{\partial}{\partial r} \hat{r} + \frac{1}{r} \frac{\partial}{\partial \theta} \hat{\theta} + \frac{1}{r \sin\theta} \frac{\partial}{\partial \phi} \hat{\phi} \right) \leftarrow \text{aid sheet}$$

$$\vec{E} = -\nabla V = - \left(\frac{\partial}{\partial r} V \hat{r} + \frac{1}{r} \frac{\partial}{\partial \theta} V \hat{\theta} + \frac{1}{r \sin\theta} \frac{\partial}{\partial \phi} V \hat{\phi} \right)$$

$$\vec{E} = - \left(10 \sin\theta \cos\phi \left(\frac{-2}{r^3} \right) \hat{r} + \frac{1}{r} \frac{10 \cos\phi}{r^2} (\cos\theta) \hat{\theta} + \frac{10}{r^2} \cdot \frac{\sin\theta}{r \sin\theta} (-\sin\phi) \hat{\phi} \right)$$

$$\vec{E} = 2.5 \text{ [V/m]} \Rightarrow \vec{D} = \epsilon_0 \vec{E} = 2.5 \epsilon_0 \text{ [C/m}^2\text{]}$$

b) $V = \frac{W}{q}$, $V_{BA} = V_B - V_A = - \int_A^B \vec{E} \cdot d\vec{l}$

$$W = 28.125 \mu\text{J}$$

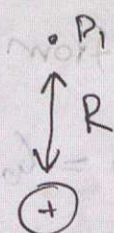
$V_B > V_A \Rightarrow V_B - V_A > 0$
so work is done by

external agent

Find V due to P.C. @ Point P_i

- + take test charge q_0 from P_i to infinity
- + since path independent, then choose simplest path

$\Rightarrow$ Radial $d\vec{r} = dr \hat{r}$
 $\vec{E} = E_r \hat{r}$



$\vec{E} \cdot d\vec{r} = E dr$

$V_2 - V_1 = \underbrace{V_{\text{final}}}_{=0} - V_{\text{initial}} = - \int_{\text{in}}^{\text{fin}} \vec{E} \cdot d\vec{r}$

$-V_{\text{in}} = - \int_R^{\infty} E dr' \Rightarrow V_{\text{in}} = \int_R^{\infty} \frac{q}{4\pi\epsilon_0 r'^2} dr'$

$V = \frac{q}{4\pi\epsilon_0} \left(-\frac{1}{r'} \right)_R^{\infty} = \frac{q}{4\pi\epsilon_0} \left(-\frac{1}{\infty} + \frac{1}{R} \right)$

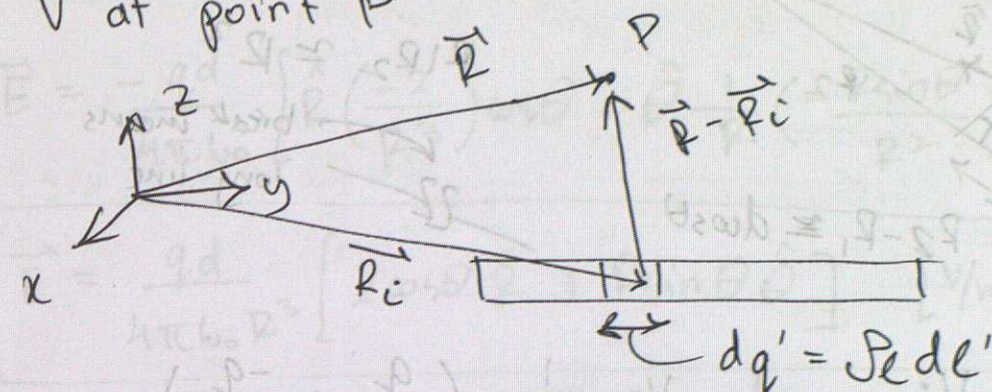
$V = \frac{q}{4\pi\epsilon_0} \cdot \frac{1}{R} [V]$

• potential due to many point charges

$V = \frac{1}{4\pi\epsilon_0} \sum_{i=1}^n \frac{q_i}{|\vec{r} - \vec{r}_i|}$

* If charge distribution is continuous, then

V at point P

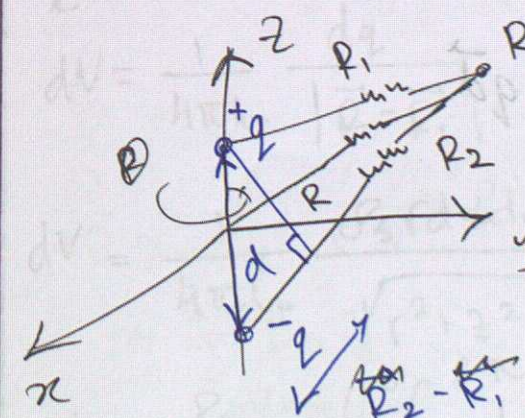


$V = \frac{1}{4\pi\epsilon_0} \int \frac{\rho dl}{|\vec{r} - \vec{r}_i|}$

... line, but replace l and ρdl with $s, \rho_s ds$ and $V, \rho_v dv$

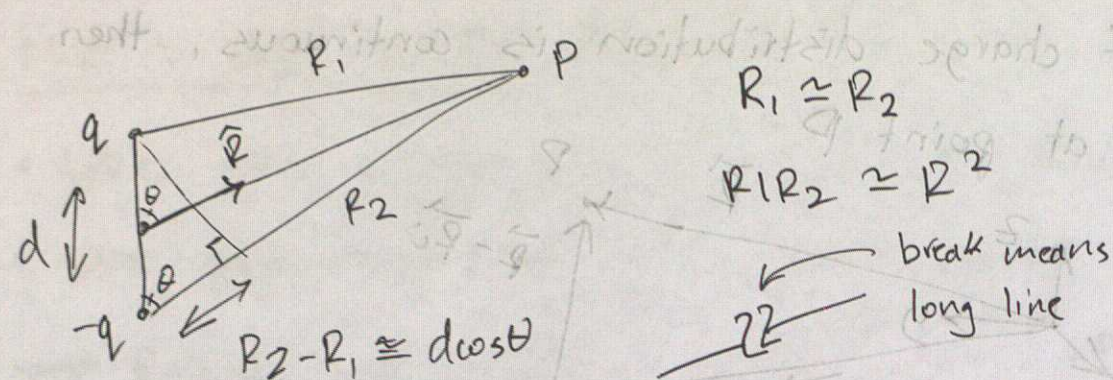
Electric Dipole

* is two equal point charges of opposite signs separated by small distance "d"



consider drawing where $R \gg d$... Find V and E at P

$r_2 - r_1 \approx d \cos \theta$



$$V = \sum_{i=1}^2 V_i \quad \text{and} \quad V = \frac{1}{4\pi\epsilon_0} \left(\frac{q}{R_1} + \frac{-q}{R_2} \right)$$

$$V = \frac{q}{4\pi\epsilon_0} \left(\frac{R_2 - R_1}{R_1 R_2} \right) \quad \leftarrow \begin{array}{l} R_2 - R_1 \approx d \cos \theta \\ R_2 R_1 \approx R^2 \end{array}$$

$$\Rightarrow V = \frac{q d \cos \theta}{4\pi\epsilon_0 R^2}$$

Note: $q d \cos \theta = q \vec{d} \cdot \hat{r}$

Define: Dipole moment as $\vec{P} = q \vec{d}$

$$\Rightarrow V = \frac{\vec{P} \cdot \hat{r}}{4\pi\epsilon_0 R^2} \quad [V]$$

Find $\vec{E}$ from V

$\vec{E} = -\nabla V$ and spherical coordinates

Knowing from Table

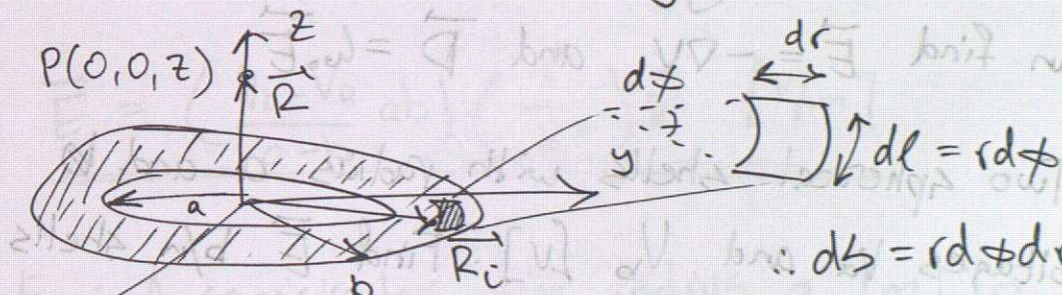
$$\vec{E} = - \left(\hat{r} \frac{\partial V}{\partial R} + \hat{\theta} \frac{1}{R} \frac{\partial V}{\partial \theta} + \hat{\phi} \frac{1}{R \sin \theta} \frac{\partial V}{\partial \phi} \right)$$

$$\vec{E} = -\nabla \left(\frac{q d \cos \theta}{4\pi\epsilon_0 R^2} \right)$$

$$\vec{E} = -\frac{q d}{4\pi\epsilon_0} \left[\hat{r} \left(\frac{-2}{R^3} \right) \cos \theta + \hat{\theta} \frac{1}{R} \left(-\frac{R \sin \theta}{R^2} \right) \right]$$

$$\vec{E} = \frac{q d}{4\pi\epsilon_0 R^3} \left[2 \cos \theta \hat{r} + R \sin \theta \hat{\theta} \right] \quad [V/m]$$

Ex: A disk with a hole in the middle (Annulus) with uniform charge density ρ_s [C/m^2], Find V @ P



$$dV = \frac{1}{4\pi\epsilon_0} \frac{dq}{|\vec{R} - \vec{R}_i|}$$

$$dq = \rho_s r d\phi dr$$

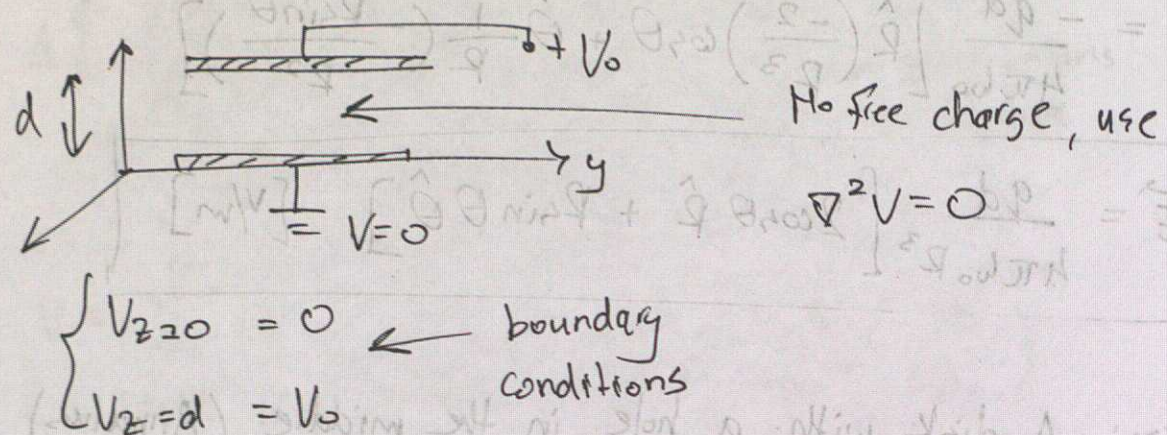
$$\vec{R} - \vec{R}_i = -r \hat{r} + z \hat{z}$$

$$dV = \frac{1}{4\pi\epsilon_0} \frac{\rho_s r d\phi dr}{\sqrt{r^2 + z^2}} \quad \rightarrow \quad V = \frac{\rho_s}{2\epsilon_0} \int \frac{1}{2} u^{-1/2} du$$

$$V = \frac{\rho_s}{4\pi\epsilon_0} \int_a^b \int_0^{2\pi} \frac{r d\phi dr}{\sqrt{r^2 + z^2}} = \frac{\rho_s}{2\epsilon_0} \left(\sqrt{b^2 + z^2} - \sqrt{a^2 + z^2} \right)$$

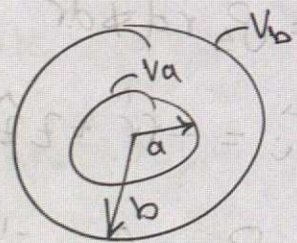
$$u = r^2 + z^2 \Rightarrow dr = \frac{1}{2r} du$$

Note: Poisson's and Laplace's equations are used to calculate V in regions with boundary conditions.



This provides V at any point inside capacitor then can find $\vec{E} = -\nabla V$ and $\vec{D} = \epsilon_0 \vec{E}$

Ex: Two spherical shells with radius a and b and voltages V_a and V_b [V]. Find $\vec{E}$ b/n shells



Knowledge: $\nabla^2 V = 0$, $a < R < b$

From Table:

$$\nabla^2 V = \frac{1}{R^2} \frac{\partial}{\partial R} \left(R^2 \frac{\partial V}{\partial R} \right) + \frac{1}{R^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial V}{\partial \theta} \right) + \dots$$

$$\Rightarrow \frac{1}{R^2} \frac{\partial}{\partial R} \left(R^2 \frac{\partial V}{\partial R} \right) = 0 \quad \text{since } \theta \text{ and } \phi \text{ are equipotential}$$

$$R \neq 0, \text{ so } \frac{\partial}{\partial R} \left(R^2 \frac{\partial V}{\partial R} \right) = 0 \quad \text{constant}$$

$$R^2 \frac{\partial V}{\partial R} = A$$

$$\Rightarrow \frac{\partial V}{\partial R} = \frac{A}{R^2} \Rightarrow V = -\frac{A}{R} + B$$

$$\begin{cases} V_a = -\frac{A}{R_a} + B \\ V_b = -\frac{A}{R_b} + B \end{cases} \Rightarrow \begin{aligned} A &= \frac{V_a - V_b}{\frac{1}{a} - \frac{1}{b}} \\ B &= \frac{aV_a - bV_b}{a - b} \end{aligned}$$

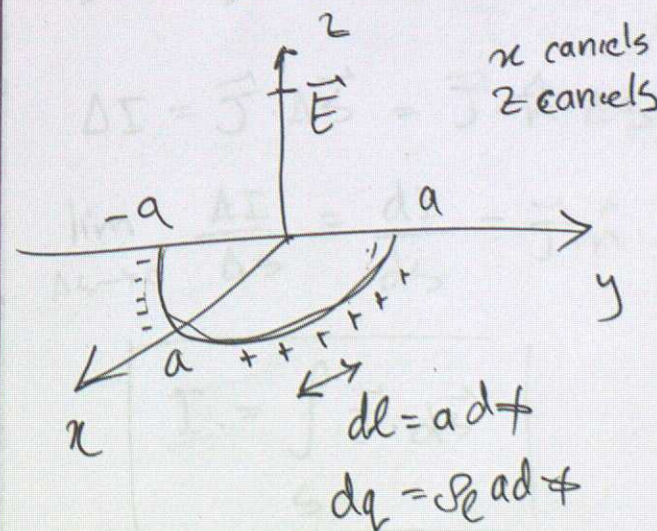
$$V = \left(\frac{V_b - V_a}{a - b} ab \right) \frac{1}{R} + \frac{aV_a - bV_b}{a - b} \quad [V]$$

$$\vec{E} = -\nabla V = -\frac{\partial V}{\partial R} \hat{r} \Rightarrow \frac{\partial}{\partial R} \left(\frac{1}{R} \right) = -\frac{1}{R^2}$$

$$\vec{E} = \left(\frac{V_b - V_a}{a - b} ab \right) \left(\frac{1}{R^2} \right) \hat{r} \quad [V/m]$$

Ex: A semicircular wire radius a [m] in xy -plane with $-\frac{\pi}{2} \leq \phi \leq \frac{\pi}{2}$ nonuniform charge density

$\rho_L = \rho_0 \sin \phi$ [C/m] ... Find $\vec{E}$ @ $(0,0,z)$



x cancels
 z cancels

$$\rho_L = \rho_0 \sin \left(-\frac{\pi}{2} \right) = -\rho_0$$

$$\rho_L = \rho_0 \sin \left(\frac{\pi}{2} \right) = \rho_0$$

$$\rho_L = \begin{cases} +ve & \text{for } 0 < \phi \leq \frac{\pi}{2} \\ -ve & \text{for } -\frac{\pi}{2} \leq \phi < 0 \end{cases}$$

$$\vec{r} = z\hat{z} \Rightarrow \vec{r} - \vec{r}_i = -a\cos\phi\hat{x} - a\sin\phi\hat{y} + z\hat{z}$$

$$\vec{r}_i = a\hat{r}$$

$$= a\cos\phi\hat{x} + a\sin\phi\hat{y}$$

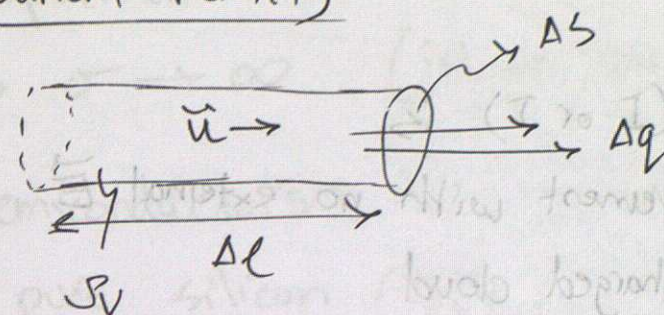
$$d\vec{E} = \frac{\rho_0 \sin\phi a d\phi}{4\pi\epsilon_0} \frac{-a\cos\phi\hat{x} - a\sin\phi\hat{y} + z\hat{z}}{(a^2\cos^2\phi + a^2\sin^2\phi + z^2)^{3/2}}$$

$$\vec{E} = \frac{-\rho_0 a^2}{8\epsilon_0 (a^2 + z^2)^{3/2}} \hat{y} \left[\frac{V}{m} \right]$$

Week 3: Lecture 2

Jan 22, 2025

Current Density



consider charges that move through ΔS with velocity $\vec{u}$

$$\Delta q = \rho_v dV \text{ and}$$

$$\Delta l = u \Delta t$$

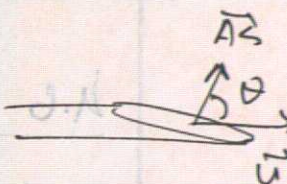
$$\Delta V = \Delta l \Delta S$$

$$\Delta q = u \Delta t \Delta S$$

$$\Delta q = \rho_v u \Delta t \Delta S \quad dV = \Delta l \Delta S$$

$$\Delta q = \rho_v u \Delta t \Delta S$$

* in general, to account for effective ΔS



$$\Rightarrow \Delta q = \rho_v u \Delta t \Delta S \cos\theta$$

$$\Delta q = \rho_v \Delta t \vec{u} \cdot \vec{\Delta S}$$

$$\Delta I = \frac{\Delta q}{\Delta t} = \frac{\rho_v \Delta t \vec{u} \cdot \vec{\Delta S}}{\Delta t} = \rho_v \vec{u} \cdot \vec{\Delta S}$$

Define $\vec{J} = \rho_v \vec{u}$ current density $\rightarrow \Delta I = \vec{J} \cdot \vec{\Delta S}$

$$[A] = [C/s] = [I] \Rightarrow [\vec{J}] = [A/m^2]$$

$$\Delta I = \vec{J} \cdot \vec{\Delta S} = \vec{J} \cdot \hat{n} \Delta S \Rightarrow \frac{\Delta I}{\Delta S} = \vec{J} \cdot \hat{n}$$

$$\lim_{\Delta S \rightarrow 0} \frac{\Delta I}{\Delta S} = \frac{dI}{dS} = \vec{J} \cdot \hat{n} \Rightarrow \int dI = \int \vec{J} \cdot d\vec{S}$$

$$I = \int_S \vec{J} \cdot d\vec{S}$$

Types of Currents

- + convection current (I or J) is
 - due to charge movement with no external $\vec{E}$
 - e.g.: wind driven charged cloud
- + conduction current (I or J)
 - charged particles moving due to electric field

4.6 Conductors

Conductivity: ($\sigma = \left[\frac{J}{E} \right] = \left[\frac{A}{V \cdot m} \right]$)

- + is how easily electrons can travel in a material under $\vec{E}$ applied

Conductors:

- + have abundance of free electrons
- + e.g.: metals, mercury (10^6 s/m)
- + note: as $\uparrow$ temperature, $\downarrow \sigma$

Insulator:

- + does not have free electrons
- + $\sigma: 10^{-10} - 10^{-17} \text{ [s/m]}$
- + perfect dielectric, $\sigma = 0$

Superconductor:

- + $\sigma \rightarrow \infty$ (irl, we cool down to 0°K)

Semiconductors:

- + pure silicon (Si)
- + can add impurities to increase free electrons or holes (by doping)

Drift Velocity:

+ in a conductor:

- when $i = 0$

Then free electrons move randomly at a speed of $\approx 10^6 \text{ m/s}$

- + when $i \neq 0$

then free electrons still move randomly but at the same time, "drift" in opposite to $\vec{E}$ direction at a drift velocity $\approx \frac{10^{-5}}{10^{-4}} \text{ [m/s]}$

+ Drift velocity in presence of $\vec{E}$ is given

→ for electrons by: $\vec{u}_e = -\mu_e \vec{E}$ → electron mobility μ_e (material property)

$\mu_e = \left[\frac{\text{m}^2}{\text{V} \cdot \text{s}} \right]$, a measure of how quickly an electron moves through a solid material

→ for holes: $\vec{u}_h = \mu_h \vec{E}$ $\vec{u}_h = \mu_h \vec{E}$

μ_h : "hole mobility"

+ Recall: $\vec{J} = \rho_v \vec{u}$

↳ total current density for both $\vec{J}_e$ and $\vec{J}_h$

⇒ $\vec{J} = \vec{J}_e + \vec{J}_h = \rho_{ve} \vec{u}_e + \rho_{vh} \vec{u}_h$ [A/m²]

where $\rho_{ve} = -N_e e$

number of electrons is $-e$

$\rho_{vh} = N_h e$

number of holes is e

∴ can write

$\vec{J} = (-\rho_{ve} \mu_e + \rho_{vh} \mu_h) \vec{E} = \sigma \vec{E}$

conductivity

* good conductor

$\vec{J} = \sigma \vec{E}$

$N_h \mu_h \ll N_e \mu_e$

⇒ $\sigma = -\rho_{ve} \mu_e = N_e \mu_e e$

+ Perfect conductor: $\sigma \rightarrow \infty$, $\vec{E} = \frac{\vec{J}}{\sigma} = 0$

$V = RI$
 $V = (0)I$

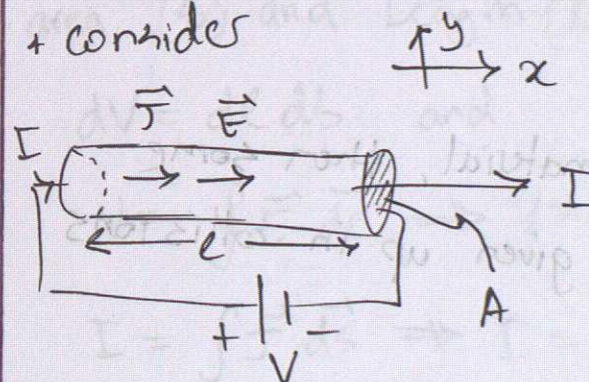
+ perfect insulator $\sigma = 0$, $\vec{J} = 0$

+ please do example 4-10

4-6.2 Resistance

+ a measure of opposition to flow of current

+ consider



$V = -\int_l \vec{E} \cdot d\vec{l} = El$ [V]

$I = \int_s \vec{J} \cdot d\vec{s}$ and $\vec{J} = \sigma \vec{E}$ [A]

↳ $I = \int_s \sigma \vec{E} \cdot d\vec{s} = \sigma EA$
↑
area

Ohm's Law

$R = \frac{V}{I} = \frac{El}{\sigma EA} \Rightarrow R = \frac{l}{\sigma A}$ ← definition of R

To Ask:

- * constants like ϵ_0 , e , k not given
- * electric current/electron mobility formula not given $\rho_v = -N_e e$...
- * W341: last example, why not also spherical

Ohm's Law

$$R = \frac{\ell}{\sigma A} \quad \text{and} \quad R = \frac{V}{I} = \frac{-\int_{\ell} \vec{E} \cdot d\vec{\ell}}{\int_S \sigma \vec{E} \cdot d\vec{s}} \quad [\Omega]$$

$$R = \frac{-\int_{\ell} \vec{E} \cdot d\vec{\ell}}{\int_S \sigma \vec{E} \cdot d\vec{s}}$$

$$G = \frac{1}{R} = \frac{\int_S \sigma \vec{E} \cdot d\vec{s}}{-\int_{\ell} \vec{E} \cdot d\vec{\ell}} \quad [S] \text{ or } [\text{Siemens}]$$

conductance

Joule's Law

- when charge moves thru a material, then some of the charge energy is given up in collisions with atoms of material
- called dissipated power (P)
- then moving $dq = \rho_v dv$ requires a force $d\vec{F} = dq \vec{E}$
 $\therefore d\vec{F} = \rho_v dv \vec{E}$
- work is $dW = d\vec{F} \cdot d\vec{\ell} = \rho_v dv \vec{E} \cdot d\vec{\ell}$
- and the increment in power dissipated is

$$dP = \frac{dW}{dt} = \rho_v dv \vec{E} \cdot \frac{d\vec{\ell}}{dt} = \rho_v dv \vec{E} \cdot \vec{u}_e$$

velocity of electron

* Rearrange $\Rightarrow dP = \vec{E} \cdot \rho_v \vec{u}_e dv$

* Recall $\vec{J} = \rho_v \vec{u}_e$
 $\Rightarrow dP = \vec{E} \cdot \vec{J} dv$ and integrate, also $\vec{J} = \sigma \vec{E}$

$$P = \int_V \vec{E} \cdot \vec{J} dv \Rightarrow P = \int_V \sigma E^2 dv$$

* this is known as Joule's Law

* Suppose a conductor has uniform cross-section area (S) and Length (L), then

$$dv = d\ell dS \quad \text{and}$$

$$V = -\int \vec{E} \cdot d\vec{\ell} \Rightarrow V = EL \Rightarrow E = \frac{V}{L} \quad [V/m]$$

$$I = \int \vec{J} \cdot d\vec{s} \Rightarrow I = JS \Rightarrow J = \frac{I}{S} \quad [A/m^2]$$

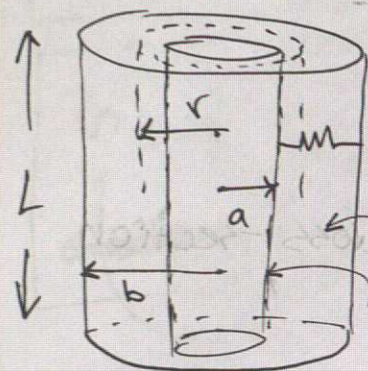
* ~~$P = \int \vec{E} \cdot \vec{J} dv$~~ $P = \int \vec{E} d\ell \int \vec{J} dS$

$$= \frac{V}{L} \int d\ell \frac{I}{S} \int dS$$

$$P = VI \quad \leftarrow \text{more common form of Joule's Law in ckt theory}$$

Ex 1: Coaxial resistor. Find Resistance (R) b/n inner ($r=a$) and outer ($r=b$) of two perfectly conducting coaxial cylinders of length L filled with a material with conductivity σ [S/m] where inner shell has a charge of Q [C] on it.

Knowledge



$$R = \frac{-\int_c \vec{E} \cdot d\vec{c}}{\int_s \vec{E} \cdot d\vec{s}}$$

to find $\vec{E}$, use Gauss law

$$\oint_s \vec{E} \cdot d\vec{s} = Q_{enc} = Q$$

$$E \cdot 2\pi r L = Q$$

$$\vec{E} = \frac{Q}{2\pi b L} \cdot \frac{1}{r} \hat{r} \text{ or } \hat{r}$$

$$V = -\int_c \vec{E} \cdot d\vec{c} = V_a - V_b$$

$$= -\int_b^a \vec{E} \cdot d\vec{c}$$

$$= -\int_b^a \frac{Q}{2\pi b L} \cdot \frac{1}{r} \hat{r} \cdot \hat{r} dr$$

$$V_{ab} = -\frac{Q}{2\pi b L} \int_b^a \frac{dr}{r} = -\frac{Q}{2\pi b L} \ln\left(\frac{a}{b}\right)$$

$$V_{ab} = \frac{Q}{2\pi b L} \ln\left(\frac{b}{a}\right)$$

$$I = \int_s \sigma \frac{Q}{2\pi b L} \cdot \frac{1}{r} \hat{r} \cdot r d\phi dz \hat{r} = \frac{\sigma Q}{2\pi b L} \int_0^{2\pi} d\phi \int_0^L dz$$

$$I = \frac{\sigma Q}{b} \text{ [A]}$$

$$\Rightarrow R = \frac{-\int_c \vec{E} \cdot d\vec{c}}{\int_s \vec{E} \cdot d\vec{s}} = \frac{\frac{Q}{2\pi b L} \ln\left(\frac{b}{a}\right)}{\frac{\sigma Q}{b}} = \frac{1}{2\pi \sigma L} \ln\left(\frac{b}{a}\right) \text{ [}\Omega\text{]}$$

Ex 2: Consider a 10 cm diameter cylinder with $\sigma = 10^{-3}$ [S/m] and $\vec{E} = 12r \hat{z}$ [V/m]. Find P in 1 [m] length of this cylinder

$$P = \int \vec{E} \cdot \vec{J} dV = \int \sigma E^2 dV \leftarrow \text{choose second}$$

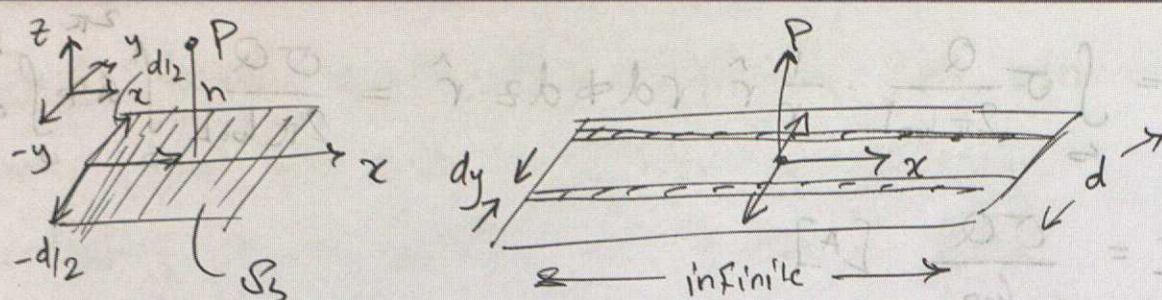
$$P = \sigma \int_0^{1\text{m}} \int_0^{2\pi} \int_0^{0.05\text{m}} (12 \times 10^2 r)^2 r dr d\phi dz$$

$$= (10^{-3}) (144 \times 10^4) \left(\frac{1}{4} (5 \times 10^{-2})^4\right) (2\pi) (1\text{m})$$

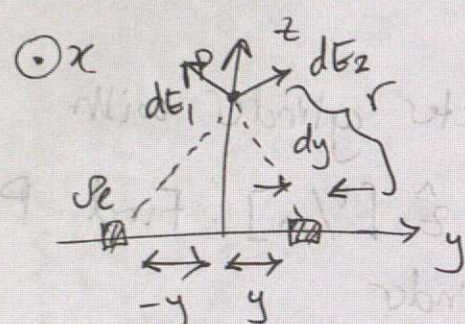
$$\underline{P = 14.1 \text{ mW}}$$

Tutorial 3

4.21



$$\vec{E} = \hat{z} \frac{\rho_s}{2\epsilon_0} \quad \rho_c = \rho_s dy$$



$$dE_1 = \hat{r} \frac{\rho_c}{2\pi\epsilon_0 r} = dE_2$$

$$dE = dE_1 + dE_2$$

$$= \hat{r} \frac{2\rho_c}{2\pi\epsilon_0 r} \cos\theta$$

$$= \hat{r} \frac{\rho_s dy}{2\pi\epsilon_0 r} \cos\theta$$

$$E = \int_0^{d/2} dE = \int_0^{d/2} \frac{\rho_s dy}{\pi\epsilon_0 r} \cos\theta$$

$$= \frac{\rho_s}{\pi\epsilon_0} \int_0^{d/2} \frac{\cos\theta}{r} dy$$

$$= \frac{\rho_s}{\pi\epsilon_0} \int_0^{d/2} \frac{\cos\theta}{h/\cos\theta} \cdot \frac{h}{\cos^2\theta} d\theta$$

$$= \frac{\rho_s}{2\pi\epsilon_0} \frac{\rho_s}{\pi\epsilon_0} \int_0^{\theta_0} \frac{h}{h} d\theta$$

$$= \frac{\rho_s}{\pi\epsilon_0} [\theta_0 - 0] \Rightarrow \vec{E} = \frac{\rho_s}{\pi\epsilon_0} \tan^{-1}\left(\frac{d}{2h}\right) \hat{z}$$

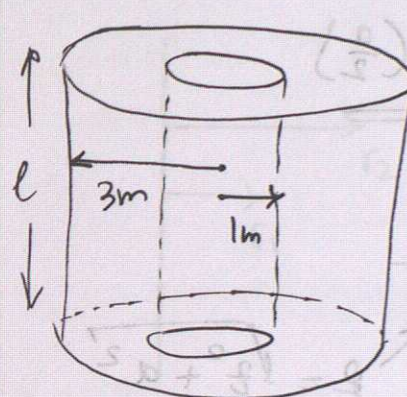
when considering $d \rightarrow \infty$, $\theta_0 = \tan^{-1}\left(\frac{d}{2h}\right) \rightarrow \frac{\pi}{2}$

$$\Rightarrow \vec{E} = \frac{\rho_s}{\pi\epsilon_0} \cdot \frac{\pi}{2} = \frac{\rho_s}{2\epsilon_0} \hat{z}$$

4.27

Gauss's Law: $\oint \vec{E} \cdot d\vec{s} = \frac{Q_{enc}}{\epsilon_0}$ and $\vec{D} = \epsilon_0 \vec{E}$

$$\Rightarrow \oint \vec{D} \cdot d\vec{s} = Q_{enc} \quad \text{a) } r < 1\text{m}, Q_{enc} = 0$$



$$\therefore \vec{D} = 0$$

$$\text{b) } 1 < r < 3\text{m}$$

$$\oint \vec{D} \cdot d\vec{s} = D(2\pi r l) = Q_{enc}$$

$$D(2\pi r l) = \rho_{vo} \pi l (r^2 - 1)$$

$$\vec{D} = \frac{\rho_{vo} (r^2 - 1)}{2r} \hat{r}$$

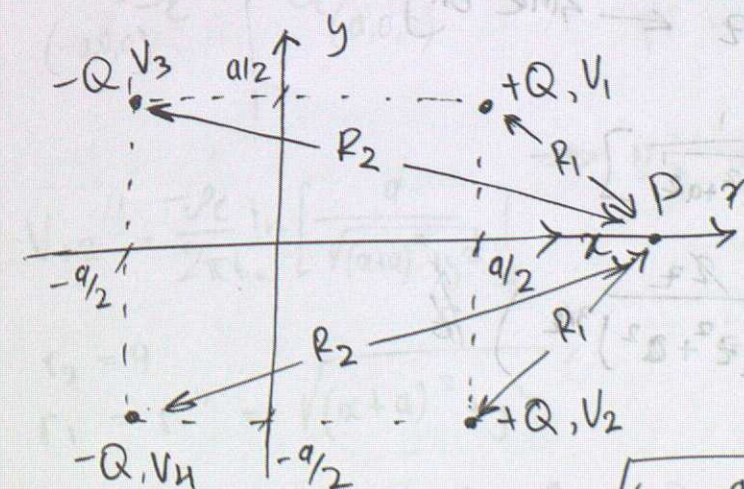
$$\text{c) } r > 3\text{m}$$

$$\oint \vec{D} \cdot d\vec{s} = D(2\pi r l)$$

$$D(2\pi r l) = (\pi 3^2 - \pi 1^2) l \rho_{vo}$$

$$\vec{D} = \frac{8\rho_{vo}}{2r} = \frac{4\rho_{vo}}{r} \hat{r}$$

4.30



$$V = \frac{q}{4\pi\epsilon_0 r}$$

$$\Rightarrow V_1 = V_2 = \frac{Q}{4\pi\epsilon_0 R_1}$$

$$\Rightarrow V_3 = V_4 = \frac{-Q}{4\pi\epsilon_0 R_2}$$

$$R_1 = \sqrt{\left(x - \frac{a}{2}\right)^2 + \left(\frac{a}{2}\right)^2}$$

$$R_2 = \sqrt{\left(x + \frac{a}{2}\right)^2 + \left(\frac{a}{2}\right)^2}$$

$$V = V_1 + V_2 + V_3 + V_4 = 2V_1 + 2V_3$$

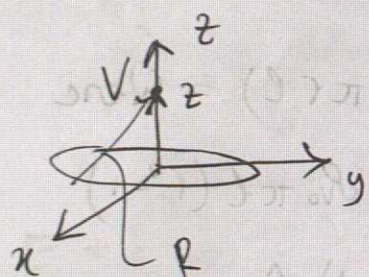
$$= \frac{Q}{2\pi\epsilon_0 R_1} - \frac{Q}{2\pi\epsilon_0 R_2} = \frac{Q}{2\pi\epsilon_0} \left[\frac{1}{\sqrt{(x - a/2)^2 + a^2/4}} - \frac{1}{\sqrt{(x + a/2)^2 + a^2/4}} \right]$$

What V @ $x = a/2$?

$$V = \frac{Q}{2\pi\epsilon_0} \left[\frac{1}{\sqrt{\frac{a^2}{4}}} - \frac{1}{\sqrt{a^2 + \frac{a^2}{4}}} \right]$$

$$= \frac{Q}{2\pi\epsilon_0 a} \left[2 - \frac{2}{\sqrt{5}} \right] = \frac{0.55Q}{2\pi\epsilon_0 a} = V\left(\frac{a}{2}\right)$$

4.32:



$$V = \frac{1}{4\pi\epsilon_0} \int \frac{dQ'}{R}$$

$$dQ = \sigma_c d\ell$$

$$R = \sqrt{z^2 + a^2}$$

$$V = \frac{1}{4\pi\epsilon_0} \int_0^{2\pi a} \frac{\sigma_c d\ell}{\sqrt{z^2 + a^2}} \Rightarrow V = \frac{\sigma_c a}{2\epsilon_0 \sqrt{z^2 + a^2}}$$

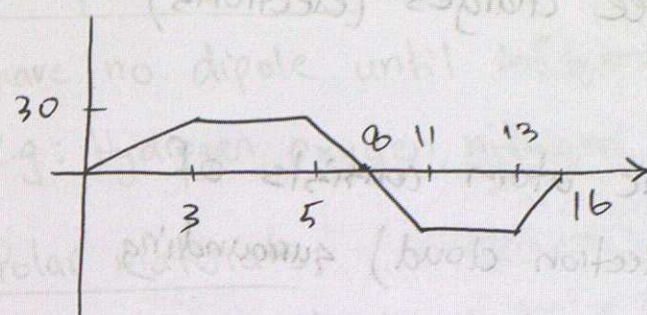
$$\vec{E} = -\nabla V = \frac{\partial V}{\partial z} \hat{z} \leftarrow \text{since only } z\text{-comp exists}$$

$$= -\hat{z} \frac{\sigma_c a}{2\epsilon_0} \frac{\partial}{\partial z} \left[\frac{1}{\sqrt{z^2 + a^2}} \right]$$

$$= -\hat{z} \frac{\sigma_c a}{2\epsilon_0} \left(-\frac{1}{z} \right) \left(\frac{z}{(z^2 + a^2)^{3/2}} \right)$$

$$\vec{E} = \frac{\sigma_c a z}{2\epsilon_0 (z^2 + a^2)^{3/2}} \hat{z}$$

4.36: $\vec{E} = -\nabla V = -\hat{x} \frac{\partial V}{\partial x} \leftarrow \text{since graphs show } V \text{ as a function of } x \text{ only}$

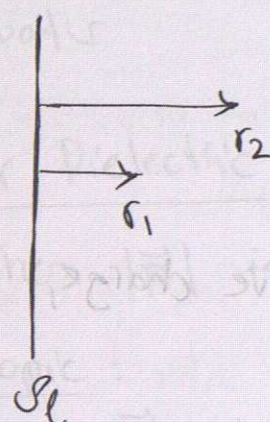


b) $V(x) = 44 \sin\left(\frac{\pi}{3} x\right)$

c) $V(x) = -44 \sin\left(\frac{\pi}{6} x\right)$

$$\vec{E} = -x \frac{\partial V}{\partial x}$$

4.33:

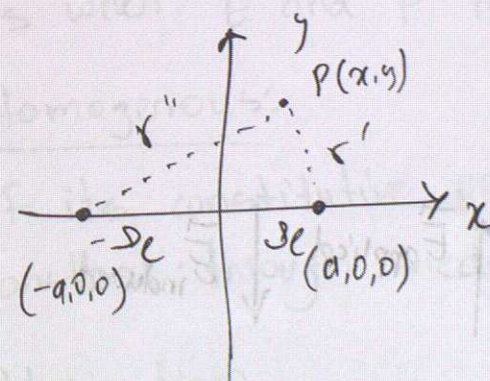


$$V_{12} = -\int \vec{E} \cdot d\vec{\ell} \quad \text{and} \quad \vec{E} = -\nabla V$$

$$V_{12} = -\int_{r_2}^{r_1} \frac{\sigma_c}{2\pi\epsilon_0 r} \cdot d\ell \quad \uparrow \quad |\vec{E}| = \frac{\sigma_c}{2\pi\epsilon_0 r}$$

$$= -\frac{\sigma_c}{2\pi\epsilon_0} \ln\left(\frac{r_2}{r_1}\right)$$

4.37:



$$V_{12}' = \frac{\sigma_c}{2\pi\epsilon_0} \ln\left(\frac{r_2}{r_1}\right) \quad r_2 = a, \quad r_1 = r'$$

$$r' = \sqrt{(x-a)^2 + y^2}$$

$$\Rightarrow V_{12}' = \frac{\sigma_c}{2\pi\epsilon_0} \ln\left[\frac{a}{\sqrt{(x-a)^2 + y^2}}\right]$$

$$V_{12}'' = -\frac{\sigma_c}{2\pi\epsilon_0} \ln\left[\frac{a}{\sqrt{(x+a)^2 + y^2}}\right]$$

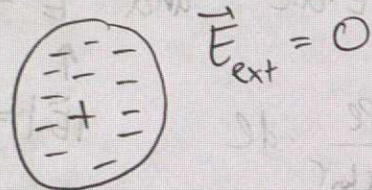
$$\therefore V_{12} = V_{12}' + V_{12}''$$

$$= \frac{\sigma_c}{4\pi\epsilon_0} \ln\left[\frac{(x+a)^2 + y^2}{(x-a)^2 + y^2}\right]$$

$$V_{12} = \frac{\sigma_c}{2\pi\epsilon_0} \left\{ \ln\left[\frac{a}{\sqrt{(x-a)^2 + y^2}}\right] - \ln\left[\frac{a}{\sqrt{(x+a)^2 + y^2}}\right] \right\}$$

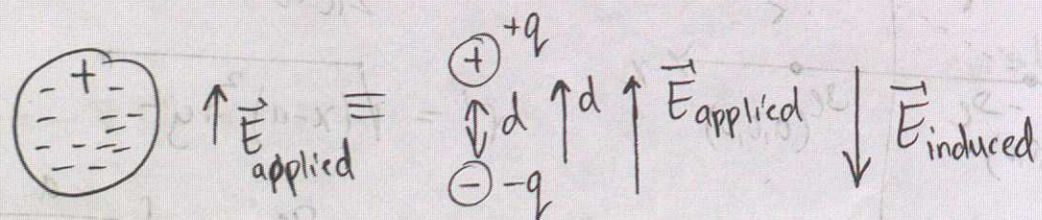
4.7 Dielectrics

- have very few, if any, free charges (electrons) available for conduction
- at atomic level, a dielectric atom consists of a negative charge $-q$ (electron cloud) surrounding a positive charge $+q$ (nucleus)



- since equal amount of (+)ve and (-)ve charge, then atom is electrically neutral.

→ Applying $\vec{E}$



- causes the electron cloud to shift such that dipoles are formed that are aligned in the direction of $\vec{E}_{\text{applied}}$
- in fact, the presence of $\vec{E}_{\text{applied}}$ induces a local electric dipole moment ($\vec{P}$) and the dielectric is said to be polarized.

$$\vec{P} = q\vec{d}$$

Two types: nonpolar materials, polar materials

- 1) Nonpolar materials:
 - have no dipole until influenced by $\vec{E}$, then become polarized
 - e.g: Hydrogen, oxygen, nitrogen, rare gases
- 2) Polar materials:
 - have built-in dipole that are randomly oriented
 - e.g: water

→ Linear Dielectric Medium

- is when $|\vec{P}|$ is proportional to $|\vec{E}|$

→ Isotropic:

- is when $\vec{E}$ and $\vec{P}$ have the same direction

→ Homogenous:

- if its constitutive parameters (ϵ, μ, σ) are constant through medium

Polarization

- shows the density of electric dipole moment per unit volume and is given by

$$\vec{P} = \chi_e \epsilon_0 \vec{E} \quad \text{where } \vec{P} \text{ is proportional to } \vec{E}$$

$\uparrow$
 "chi"

$\rightarrow$ susceptibility, a scalar if isotropic
 (for linear, isotropic, homogenous)

Q: $\vec{P}$ is electric dipole moment and also polarization?

* χ_e shows how receptive a material is to polarization.

* note that presence of dipoles change electric flux density ($\vec{D}$) and extends D to

$$\vec{D} = \epsilon_0 \vec{E} + \vec{P} \quad \epsilon_0 \rightarrow \text{vacuum}$$

$$\vec{D} = \epsilon_0 \vec{E} + \chi_e \epsilon_0 \vec{E} \quad \vec{D} = \epsilon_r \epsilon_0 \vec{E} \rightarrow \text{other stuff}$$

$$\vec{D} = (1 + \chi_e) \epsilon_0 \vec{E}$$

ϵ_r epsilon r (relative permittivity) (dielectric constant)

a convenient to show ϵ relative to free space ϵ_0

$$\epsilon = \epsilon_0 \epsilon_r \Rightarrow \epsilon_r = \frac{\epsilon}{\epsilon_0} \quad \text{get from tables}$$

Dielectric Breakdown

* is when dielectric becomes conducting

* the minimum $\vec{E}$ at which dielectric breakdown occurs is called dielectric strength (E_{ds})

* occurs when electrons detach from molecules and accelerate in the material conduction current, causing sparks and ^{as} damaging the dielectric.

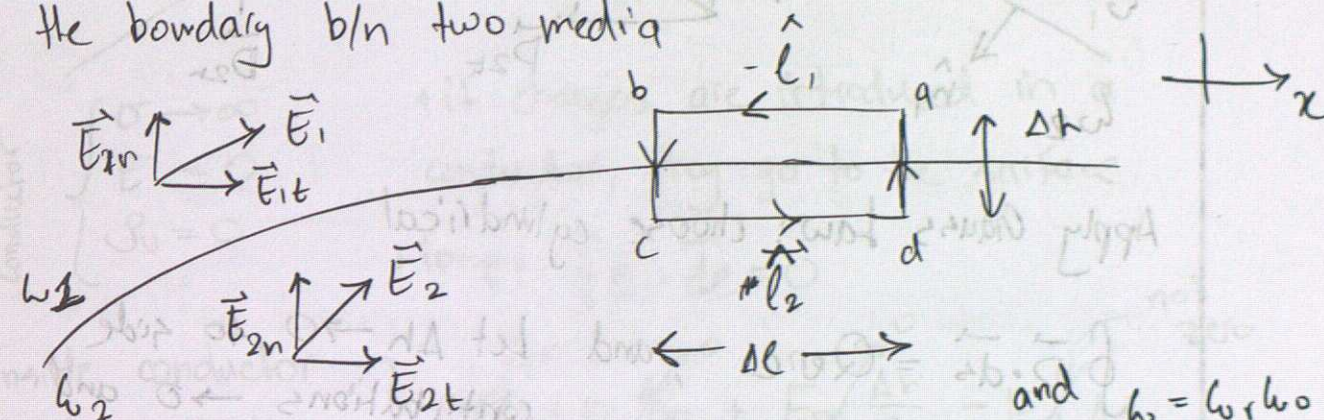
Ex-4-12

material	air	glass	quartz
ϵ_r	1.0006 ± 1	$4.5 - 10$	$3.5 - 8$
$E_{ds} [\frac{MV}{m}]$	≈ 3	$\approx 25 - 40$	≈ 30

★ 4.8 Electric Boundary Conditions

* $\vec{E}$ may be continuous inside media, but can be discontinuous at the boundary

* provide information on how $\vec{E}$ (E_t and E_n) behave at the boundary b/n two media



Find $\vec{E}$ at boundary $\rightarrow$ path a b c d

Knowledge: $\oint \vec{E} \cdot d\vec{l} = 0$ and let $\Delta h \Rightarrow 0$

$$\Rightarrow \int_a^b \vec{E}_1 \cdot \hat{l}_1 dl + \int_c^d \vec{E}_2 \cdot \hat{l}_2 dl = 0 \quad \text{and} \quad \hat{l}_1 = -\hat{l}_2$$

$$\Rightarrow [(\vec{E}_1 \cdot \hat{l}_1) + (\vec{E}_2 \cdot (-\hat{l}_2))] \Delta l = 0 \quad \vec{E}_1 = \vec{E}_{1t} + \vec{E}_{1n} \quad \vec{E}_2 = \vec{E}_{2t} + \vec{E}_{2n}$$

$$(\vec{E}_1 - \vec{E}_2) \cdot \hat{l}_1 = 0 \quad \leftarrow \text{sub}$$

$$\Rightarrow (E_{1t} - E_{2t}) \underbrace{\hat{x} \cdot \hat{x}}_{=1} + (E_{1n} - E_{2n}) \underbrace{\hat{z} \cdot \hat{x}}_{=0} = 0$$

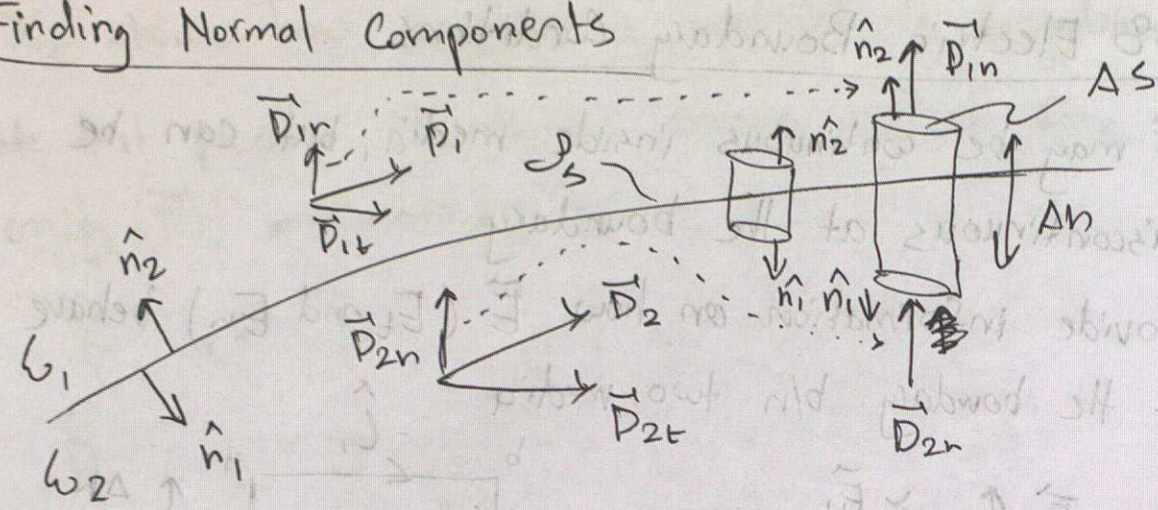
$$\boxed{E_{1t} = E_{2t}}$$

Find $\vec{D} \left\{ \begin{array}{l} \vec{D}_{1t} = \epsilon_1 \vec{E}_{1t} \\ \vec{D}_{2t} = \epsilon_2 \vec{E}_{2t} \end{array} \right.$

$$\frac{\vec{D}_{1t}}{\epsilon_1} = \frac{\vec{D}_{2t}}{\epsilon_2}$$

divide the 2
 $\frac{\vec{D}_{1t}}{\epsilon_1} = \frac{\epsilon_1 \vec{E}_{1t}}{\epsilon_2 \vec{E}_{2t}}$

Finding Normal Components



Apply Gauss Law: choose cylindrical

$\oint \vec{D} \cdot d\vec{s} = Q_{enc}$ and let $\Delta h \rightarrow 0$ so side contributions $\rightarrow 0$ and only top/bottom remains
and $Q_{enc} = \rho_s \Delta s$

$$\Rightarrow \oint \vec{D} \cdot d\vec{s} = \int_{top} \vec{D}_1 \cdot \hat{n}_1 d\vec{s} + \int_{bottom} \vec{D}_2 \cdot \hat{n}_2 d\vec{s} = Q_{enc}$$

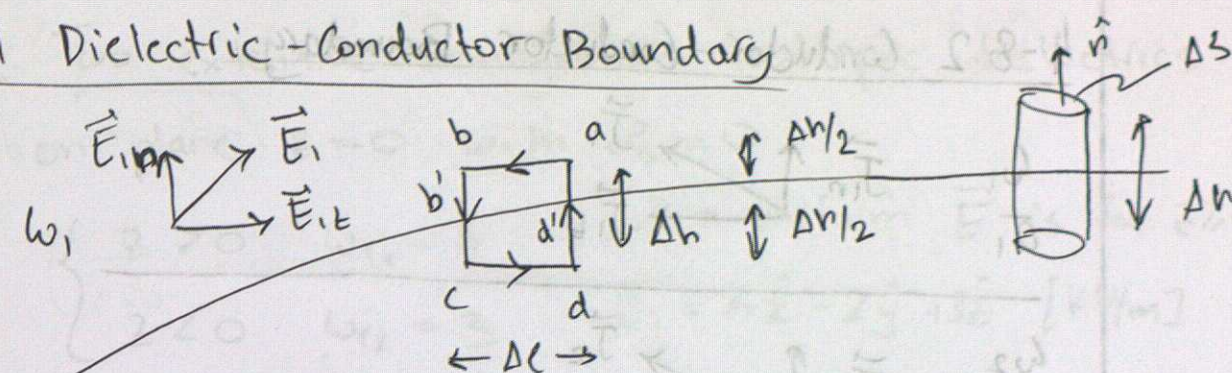
and $\hat{n}_1 = -\hat{n}_2$

$$(\underbrace{\vec{D}_{1n} \hat{z} \cdot \hat{z}}_{=1} + \underbrace{\vec{D}_{2n} \hat{z} \cdot (-\hat{z})}_{=-1}) \Delta s = \rho_s \Delta s$$

$$|\vec{D}_{1n} - \vec{D}_{2n} = \rho_s| \quad |(\vec{D}_1 - \vec{D}_2) \cdot \hat{n} = \rho_s|$$

$$|\epsilon_1 E_{1n} - \epsilon_2 E_{2n} = \rho_s|$$

4-8.1 Dielectric-Conductor Boundary



if charges are introduced in a conductor, they go to the surface
loop: $\oint \vec{E} \cdot d\vec{e} = 0$

inside conductor: $\vec{E} = 0$
outside conductor: $\oint \vec{E} \cdot d\vec{e} = 0$

$$0 \cdot \Delta l + 0 \cdot \frac{\Delta h}{2} + E_{1n} \frac{\Delta h}{2} - E_{2n} \frac{\Delta h}{2} = 0$$

not zero

$$\Rightarrow -E_{1t} \Delta l = 0$$

$$\therefore E_{1t} = 0$$

Apply Gauss Law: $\oint \vec{D} \cdot d\vec{s} = Q_{enc}$ and let $\Delta h \rightarrow 0$

inside conductor: $\vec{D} = \epsilon \vec{E} = 0$

inside dielectric: $\oint \vec{D} \cdot \hat{n} = \rho_s \Delta s$

Summary: $[C/m^2] \rightarrow \boxed{D_{1n} = \rho_s}$

note that perfect conductor, $E = 0, \rho = 0$

then $\begin{cases} E_{1t} = D_{1t} = 0 \\ D_{1n} = \epsilon_1 E_{1n} = \rho_s \end{cases}$ (Table 4-3, pg 202)

4-8.2 Conductor-Conductor Boundary

$$\begin{matrix} \epsilon_1 \\ \sigma_1 \end{matrix} \quad \begin{matrix} \vec{J}_{1n} \\ \vec{J}_{1t} \end{matrix}$$

$$\begin{matrix} \epsilon_2 \\ \sigma_2 \end{matrix} \quad \begin{matrix} \vec{J}_{2n} \\ \vec{J}_{2t} \end{matrix}$$

Already know $\vec{E}_{1t} = \vec{E}_{2t}$ and $\epsilon_1 E_{1n} - \epsilon_2 E_{2n} = \rho_s$

Since conductor, then applying $\vec{E}$, a current will flow

Recall $\vec{J} = \sigma \vec{E} \Rightarrow \vec{E} = \frac{\vec{J}}{\sigma}$

$$\left\{ \begin{matrix} \vec{J}_{1t} = \sigma_1 \vec{E}_{1t} \\ \vec{J}_{2t} = \sigma_2 \vec{E}_{2t} \end{matrix} \right\} \text{ divide } \Rightarrow \frac{\vec{J}_{1t}}{\vec{J}_{2t}} = \frac{\sigma_1 \vec{E}_{1t}}{\sigma_2 \vec{E}_{2t}} \quad \begin{matrix} \text{since} \\ \text{same} \\ \vec{E} \text{ applied} \end{matrix}$$

$$\therefore \frac{\vec{J}_{1t}}{\sigma_1} = \frac{\vec{J}_{2t}}{\sigma_2}$$

$$\left\{ \begin{matrix} \vec{J}_{1n} = \sigma_1 \vec{E}_{1n} \Rightarrow \vec{E}_{1n} = \frac{\vec{J}_{1n}}{\sigma_1} \\ \vec{J}_{2n} = \sigma_2 \vec{E}_{2n} \Rightarrow \vec{E}_{2n} = \frac{\vec{J}_{2n}}{\sigma_2} \end{matrix} \right. \text{ plug in eq ①}$$

$$\therefore \epsilon_1 \frac{\vec{J}_{1n}}{\sigma_1} - \epsilon_2 \frac{\vec{J}_{2n}}{\sigma_2} = \rho_s$$

$$\vec{J}_{1n} \left(\frac{\epsilon_1}{\sigma_1} - \frac{\epsilon_2}{\sigma_2} \right) = \rho_s$$

if $J_{1n} \neq J_{2n}$
 ρ_s or ϵ or $\sigma \neq \rho_s$ leaves
 conclude $\vec{J}_{1n} = \vec{J}_{2n}$

Week 4: Lecture 3

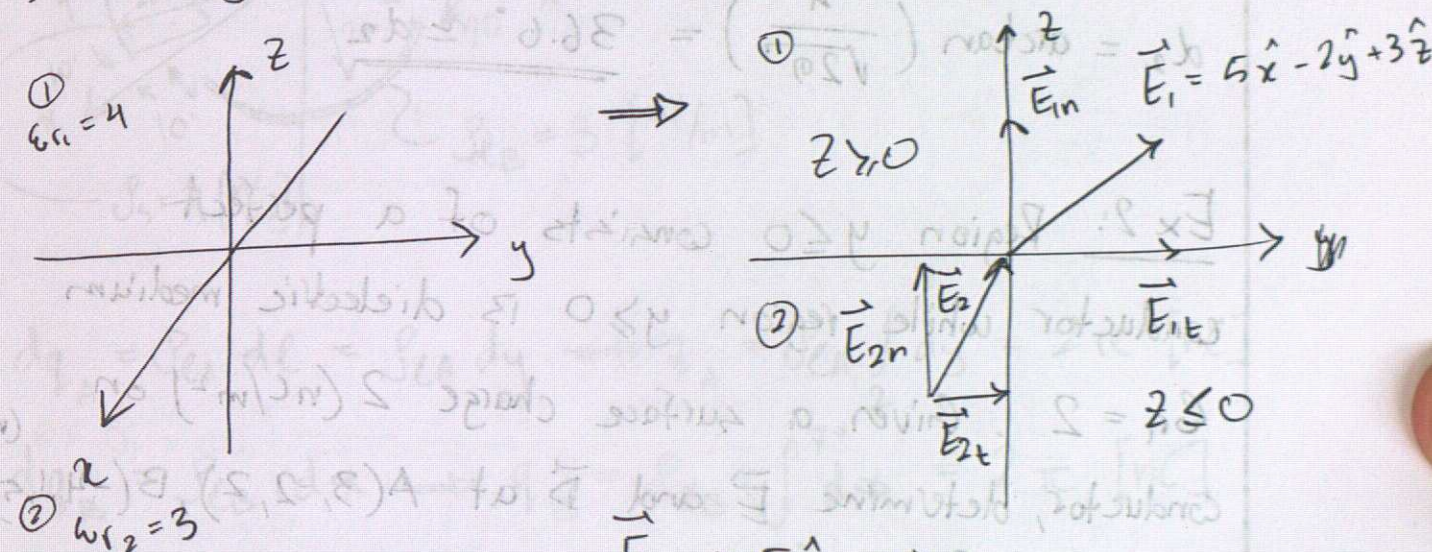
Ex 1: Two extensive homogenous isotropic dielectrics meet on plane $z=0$ with $\rho_s = 0$

for $\begin{cases} z > 0 & \epsilon_1 = 4 \\ z < 0 & \epsilon_2 = 3 \end{cases}$

and a uniform $\vec{E}$ is for $z > 0$
 $\vec{E}_1 = 5\hat{x} - 2\hat{y} + 3\hat{z} \text{ [kV/m]}$

a) $\vec{E}_2$ for $z \leq 0$

b) The angles $\vec{E}_1$ and $\vec{E}_2$ make with interface



$$\vec{E}_1 = 5\hat{x} - 2\hat{y} + 3\hat{z} \quad \left\{ \begin{matrix} \vec{E}_{1t} = 5\hat{x} - 2\hat{y} \\ \vec{E}_{1n} = 3\hat{z} \end{matrix} \right. \Rightarrow \vec{E}_{2t} = 5\hat{x} - 2\hat{y}$$

Knowing $D_{1n} = D_{2n} = \rho_s \Rightarrow \rho_s = 0, D_{1n} = D_{2n}$

and $\epsilon_1 E_{1n} = \epsilon_2 E_{2n} \Rightarrow \vec{E}_{2n} = \frac{\epsilon_1}{\epsilon_2} E_{1n} = \frac{4}{3} (3\hat{z}) = 4\hat{z}$

$$\therefore \vec{E}_2 = \vec{E}_{2t} + \vec{E}_{2n} = 5\hat{x} - 2\hat{y} + 4\hat{z}$$

b) $\uparrow +z$

$$|\vec{E}_{1n}| = 3$$

$$|\vec{E}_{1t}| = \sqrt{3^2 + 2^2} = \sqrt{29}$$

$$d_1 = \arctan\left(\frac{3}{\sqrt{29}}\right)$$

$$d_1 \approx 29.1^\circ$$

$$|\vec{E}_{2t}| = |\vec{E}_{1t}| = \sqrt{29}, \quad |\vec{E}_{2n}| = 4$$

$$d_2 = \arctan\left(\frac{4}{\sqrt{29}}\right) = 36.6^\circ \approx d_2$$

Ex 2: Region $y \leq 0$ consists of a perfect conductor while region $y \geq 0$ is dielectric medium $\epsilon_{r1} = 2$. Given a surface charge $2 \text{ (nC/m}^2\text{)}$ on conductor, determine $\vec{E}$ and $\vec{D}$ at $A(3, -2, 2), B(-4, 1, 5)$ (m)

$y \leq 0$ conductor $\textcircled{2}$ $y \geq 0, \epsilon_{r1} = 2$ $\textcircled{1}$

a) Find $\vec{E} = ?$ in conductor

$$\vec{E} = 0 \quad \vec{D} = 0 \quad (\text{point A})$$

b) Find $\vec{E}$ inside dielectric (Point B)

knowing $D_{1n} - D_{2n} = \rho_s \Rightarrow D_{1n} = \rho_s = 2 \text{ [nC/m}^2\text{]}$

$$\vec{E}_{1t} = \vec{E}_{2t} = 0$$

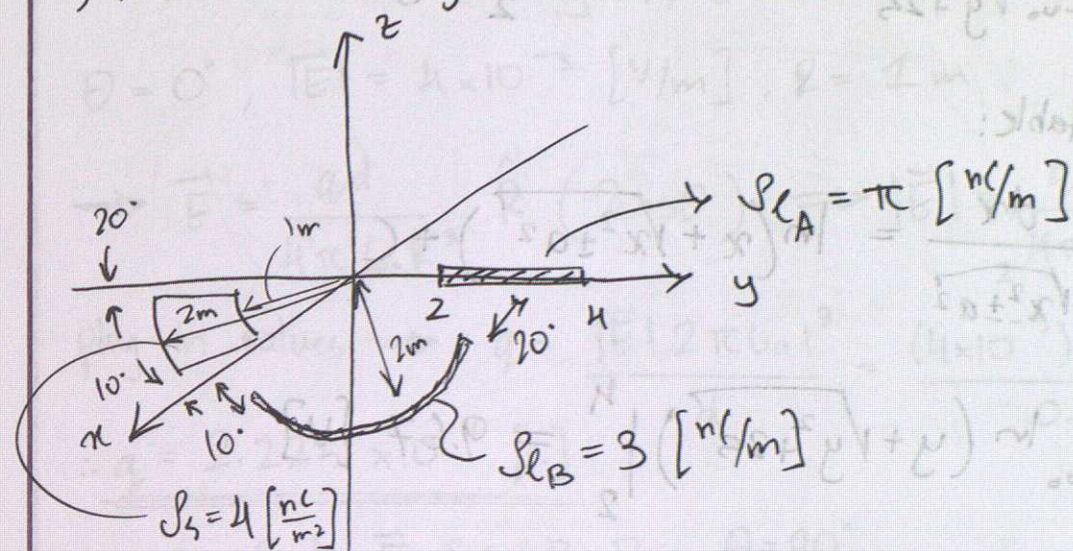
$$\therefore \vec{E}_1 = 36\pi \hat{y} \text{ [V/m]}$$

$$E_{1n} = \frac{D_{1n}}{\epsilon_{r1}} = \frac{2 \text{ [nC/m}^2\text{]}}{2 \epsilon_0} = 36\pi$$

$\uparrow 8.854 \times 10^{-12}$

Ex 3: Consider 3 separate charge distributions in free space.

a) find total charge for each distribution



$$dq_A = \rho_{LA} dl = \rho_{LA} dy \Rightarrow q_A = \rho_{LA} \int_2^4 dy = 2\pi \text{ [nC]}$$

$$dq_B = \rho_{LB} r d\phi \Rightarrow q_B = \rho_{LB} r \int_{10^\circ}^{70^\circ} d\phi = 2\pi \text{ [nC]}$$

$$dq_S = \rho_S dS = \rho_S r d\phi dr \Rightarrow q_S = \rho_S \int_0^2 r dr \int_{10^\circ}^{70^\circ} d\phi = 2\pi \text{ [nC]}$$

b) Find potential at $P(0, 0, 5) \text{ [m]}$ caused by each of these three distributions acting alone

$$dV = \frac{dq}{4\pi\epsilon_0 |\vec{r} - \vec{r}_i|}$$

$$r = \sqrt{5^2 + y^2} = \sqrt{y^2 + 25}$$

$\vec{r} = 5\hat{z}$
 $\vec{r}_i = y\hat{y}$

→ straight line:

$$dV = \frac{\rho_e dy}{4\pi\epsilon_0 \sqrt{y^2 + 25}} \Rightarrow V = \frac{\rho_e A}{4\pi\epsilon_0} \int_2^4 \frac{dy}{\sqrt{y^2 + 25}}$$

integral table:

$$\int \frac{dx}{\sqrt{x^2 + a^2}} = \ln(x + \sqrt{x^2 + a^2}) + C$$

$$V = \frac{\pi}{4\pi\epsilon_0} \ln(y + \sqrt{y^2 + 25}) \Big|_2^4 = 9.67 \text{ [V]}$$

→ arc: $|\vec{r} - \vec{r}_i| = |5\hat{z} - 2\hat{r}|$

$$V_{\text{arc}} = \frac{\rho_e B}{4\pi\epsilon_0} \int_{10^\circ}^{70^\circ} \frac{r d\phi}{\sqrt{5^2 + r^2}} = \frac{3(2)}{4\pi\epsilon_0} \frac{1}{\sqrt{29}} \int_0^{\pi/3} d\phi = 10.49 \text{ [V]}$$

→ surface: $|\vec{r} - \vec{r}_i| = |5\hat{z} - r\hat{r}|$, $dq_s = \rho_s r dr d\phi$

$$V = \frac{\rho_s}{4\pi\epsilon_0} \int_{10^\circ}^{70^\circ} \int_1^2 \frac{r dr d\phi}{\sqrt{r^2 + 25}} = \frac{1}{\pi\epsilon_0} \left(\frac{\pi}{3} \right) \int_1^2 \frac{r dr}{\sqrt{r^2 + 25}} = 10.77 \text{ [V]}$$

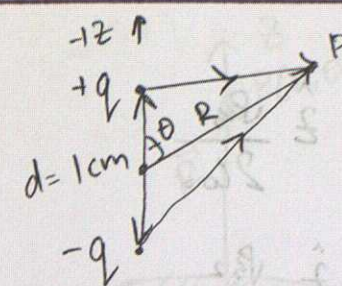
c) Find total voltage:

$$V = V_e + V_{\text{arc}} + V_s = 30.9 \text{ [V]}$$

Week 5 Tutorial 4

Feb 3, 2025

4.35:



$$\vec{E} = \frac{qd}{4\pi\epsilon_0 R^3} [\hat{R} 2\cos\theta + \hat{\theta} \sin\theta] \quad \text{eq. 4.56}$$

• for any ϕ , E is same (in this configuration)

$$\theta = 0^\circ, |\vec{E}| = 4 \times 10^{-3} \text{ [V/m]}, R = 1 \text{ m}$$

$$\Rightarrow \vec{E} = \frac{qd}{4\pi\epsilon_0 R^3} \hat{R} (2\cos\theta) \Rightarrow |\vec{E}| = \frac{qd}{2\pi\epsilon_0 R^3} (2\cos\theta)$$

$$\text{plug in values} \Rightarrow q = \frac{|\vec{E}| 2\pi\epsilon_0 R^3}{d} = \frac{(4 \times 10^{-3})(2\pi\epsilon_0)}{0.01} \\ \therefore q = 2.225 \times 10^{-11} \text{ [C]}$$

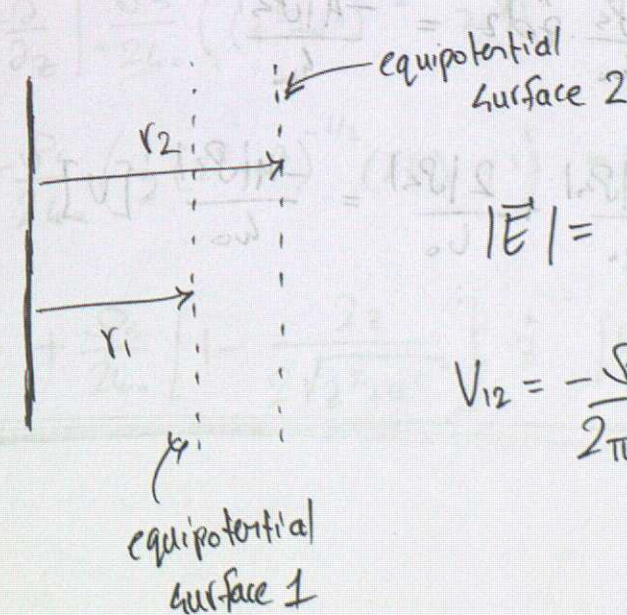
$$\Rightarrow \text{now find } \vec{E} \text{ for } R = 2 \text{ m}, \theta = 90^\circ$$

$$|\vec{E}| \Rightarrow \frac{qd}{4\pi\epsilon_0 R^3} [\hat{R} 2\cos\theta + \hat{\theta} \sin\theta] = \vec{E}$$

$\cos 90^\circ = 0$

$$|\vec{E}| = \frac{(2.225 \times 10^{-11})(0.01)}{4\pi(8.854 \times 10^{-12})(2)^3} = 2.5 \times 10^{-4} \text{ [V/m]} = |\vec{E}|$$

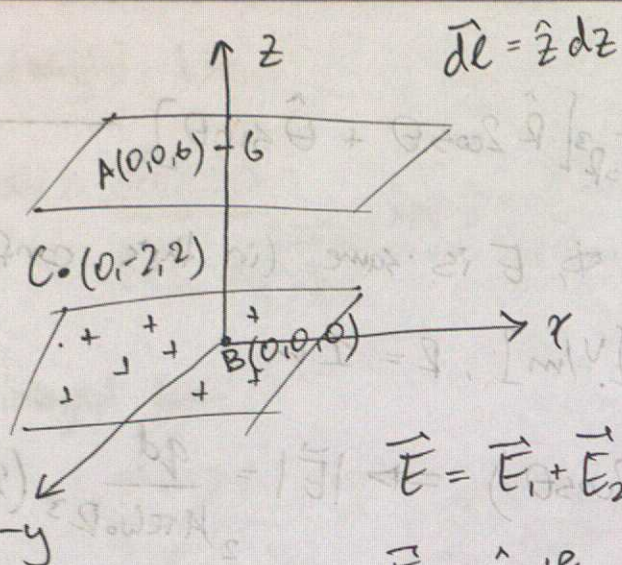
4.33
(review)



$$|\vec{E}| = \frac{V_e}{2\pi\epsilon_0 r}, \quad V_{12} = - \int_{r_2}^{r_1} \vec{E} \cdot d\vec{r}$$

$$V_{12} = - \frac{\rho_e}{2\pi\epsilon_0} \int_{r_2}^{r_1} \frac{dx}{x} = \frac{\rho_e}{2\pi\epsilon_0} \ln\left[\frac{r_2}{r_1}\right]$$

4.40



$$d\vec{l} = \hat{z} dz$$

$$\vec{E}_1 = \hat{z} \frac{\rho_{s1}}{2\epsilon_0}$$

$$\vec{E}_2 = \hat{z} \frac{\rho_{s2}}{2\epsilon_0}$$

$$\vec{E} = \vec{E}_1 + \vec{E}_2 = \hat{z} \frac{1}{2\epsilon_0} (\rho_{s1} + \rho_{s2})$$

$$\vec{E} = \hat{z} \frac{\rho_s}{\epsilon_0}$$

$$V_{AB} = - \int_B^A \vec{E} \cdot d\vec{l} = V_A - V_B$$

$$= - \int_0^6 \hat{z} \frac{\rho_s}{\epsilon_0} \cdot \hat{z} dz = - \frac{\rho_s}{\epsilon_0} \int_0^6 dz = - \frac{6|\rho_s|}{\epsilon_0}$$

$$V_{BC} = - \int_C^B \vec{E} \cdot d\vec{l} = - \int_2^0 \hat{z} \frac{\rho_s}{\epsilon_0} \cdot \hat{z} dz = + \frac{2|\rho_s|}{\epsilon_0}$$

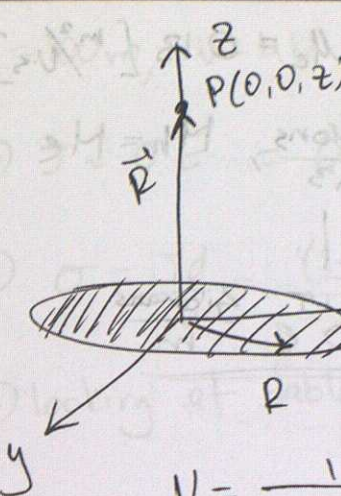
$$V_{AC} = - \int_C^A \vec{E} \cdot d\vec{l} = - \int_2^6 \hat{z} \frac{\rho_s}{\epsilon_0} \cdot \hat{z} dz = - \frac{4|\rho_s|}{\epsilon_0}$$

or

$$V_{AC} = V_{AB} + V_{BC} = \frac{-6|\rho_s|}{\epsilon_0} + \frac{2|\rho_s|}{\epsilon_0} = \frac{-4|\rho_s|}{\epsilon_0} [V]$$

4.31

a)



$$ds = r dr d\phi$$

$$dq = \rho_s ds = \rho_s r dr d\phi$$

$$dV = \frac{1}{4\pi\epsilon_0} \frac{dq}{r} \quad \vec{r} = \vec{R} - \vec{R}'$$

$$r = \sqrt{r^2 + z^2}$$

$$V = \frac{1}{4\pi\epsilon_0} \int_0^a \int_0^{2\pi} \frac{\rho_s r}{\sqrt{r^2 + z^2}} dr d\phi$$

$$V = \frac{\rho_s}{2\epsilon_0} \int_0^a \frac{r}{\sqrt{r^2 + z^2}} dr \rightarrow u = r^2 + z^2 \quad du = 2r dr \quad dr = \frac{1}{2r} du$$

$$= \frac{\rho_s}{2\epsilon_0} \int_{z^2}^{a^2 + z^2} \frac{1}{\sqrt{u}} \cdot \frac{1}{2} du = \frac{\rho_s}{4\epsilon_0} \int_{z^2}^{a^2 + z^2} (u)^{-1/2} du \Rightarrow \text{integral}$$

$$V = \frac{\rho_s}{2\epsilon_0} \left[\sqrt{z^2 + a^2} - z \right]$$

$$b) \vec{E} = -\nabla V = - \left(\hat{x} \frac{\partial}{\partial x} + \hat{y} \frac{\partial}{\partial y} + \hat{z} \frac{\partial}{\partial z} \right) V = - \frac{\partial V}{\partial z} \hat{z}$$

$$= - \frac{\partial}{\partial z} \left[\frac{\rho_s}{2\epsilon_0} \left((z^2 + a^2)^{1/2} - z \right) \right]$$

$$= - \frac{\rho_s}{2\epsilon_0} \left(\frac{1}{2} (z^2 + a^2)^{-1/2} (2z) - 1 \right) = - \frac{\rho_s}{2\epsilon_0} \left[\frac{z}{\sqrt{z^2 + a^2}} - 1 \right] = E$$

$$\vec{E} = + \frac{\rho_s}{2\epsilon_0} \left[1 - \frac{z}{\sqrt{z^2 + a^2}} \right] \hat{z} [V/m]$$

4.41 a) radius = 1mm, length = 8cm, $V_{app} = 5V$, $\mu_e = 0.13 [m^2/V.s]$

$\mu_h = 0.05 [m^2/V.s]$, $N_e = 1.5 \times 10^{16} \frac{\text{electrons}}{m^3}$, $N_h = N_e$

eq. 4.65 — $\sigma = (N_e \mu_e + N_h \mu_h) e$

$\sigma = (1.5 \times 10^{16}) (0.13 + 0.05) e = 2.7 \times 10^{15} \frac{e}{m} \xrightarrow{\text{Siemens}}$

$\sigma = 4.32 \times 10^{-4} S/m$

b) $I = JA = \sigma EA$, but $Ed = V \Rightarrow E = \frac{V}{d}$

$I = \frac{\sigma VA}{d} = \frac{(4.32 \times 10^{-4}) (5) (\pi (4 \times 10^{-3})^2)}{(0.08) (0.08)} = 1.36 \times 10^{-6} A$

c) $u_e = -\mu_e E = \frac{-\mu_e V}{d} = \frac{-(0.13)(5)}{0.08} = -8.125 m/s \hat{E}$

$u_h = +\mu_h E = \frac{-(0.05)(5)}{0.08} = 3.125 m/s \hat{E}$

d) $R = \frac{V}{I} = \frac{5}{1.36 \mu A} = 3.68 M\Omega$

e) $P = IV = (5)(1.36 \mu A) = 6.8 \mu W$

4.42

a) $2.3 S/m$

b) $I = 7.225 mA$

c) $u_e = -25 m/s \hat{E}$ $u_h = 12.5 m/s \hat{E}$

d) $R = 0.69 k\Omega$

e) $P = 36.125 mW$

repeat Q4.41 for Germanium (μ_e)

4.43

$\ell = 100m$, $V = 4V$, $J = 1.4 \times 10^6 [A/m^2]$ — what material?

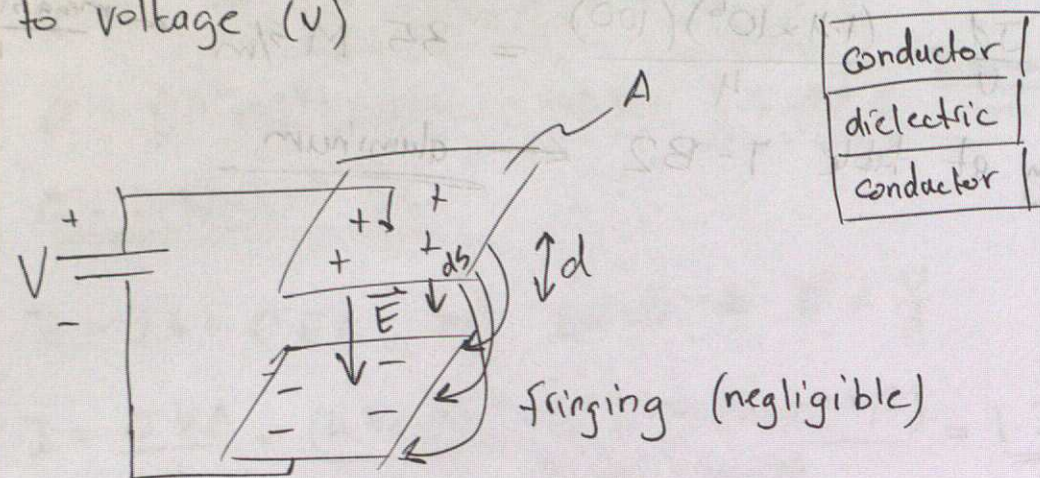
① $J = \sigma E = \sigma \frac{V}{d}$

② $\sigma = \frac{Jd}{V} = \frac{(1.4 \times 10^6)(100)}{4} = 35 MS/m \leftarrow \text{megasiemens}$

③ looking at table T-B2 $\leftarrow$ aluminum

4.9 Capacitance

- two conductors (any shape/geometry) connected to voltage (V)



→ Define Capacitance:

$$C \triangleq \frac{Q}{V} \text{ [C/V] or [F]}$$

conductor - dielectric:

$$\begin{cases} E_t = 0 \\ D_n = \rho_s \end{cases}$$

- Tangential $\vec{E}$ (E_t) vanishes at the surface and $\vec{E}$ is always $\perp$ to the surface

$$\Rightarrow \vec{E} \cdot \hat{n} = E_n = \frac{\rho_s}{\epsilon_0} \Rightarrow \rho_s = \epsilon_0 \vec{E} \cdot \hat{n}$$

$$Q = \int \rho_s dS$$

$$= \int \epsilon_0 \vec{E} \cdot \hat{n} dS = \epsilon_0 \int \vec{E} \cdot d\vec{s}$$

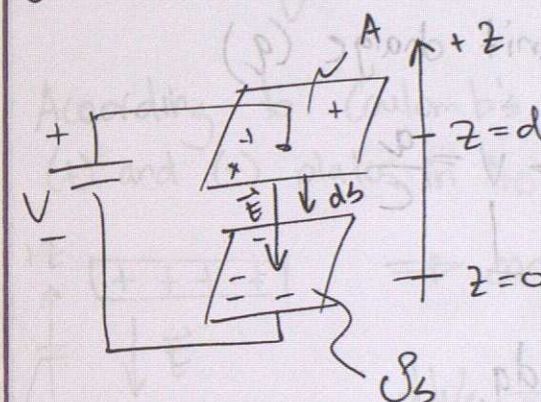
Knowing that $V = -\int \vec{E} \cdot d\vec{e} \Rightarrow C = \frac{\int \epsilon_0 \vec{E} \cdot d\vec{s}}{-\int \vec{E} \cdot d\vec{e}} \text{ [F]}$

Recall: $\vec{E} = -\frac{\nabla V}{\epsilon_0} \Rightarrow P = \frac{-\int \epsilon_0 \vec{E} \cdot d\vec{e}}{\int \epsilon_0 \vec{E} \cdot d\vec{s}}$

$$\Rightarrow PC = \frac{-\int \epsilon_0 \vec{E} \cdot d\vec{e}}{\int \epsilon_0 \vec{E} \cdot d\vec{s}} \cdot \int \epsilon_0 \vec{E} \cdot d\vec{s} \Rightarrow PC = \frac{\epsilon_0}{\sigma} = \tau \text{ [s]}$$

(time constant)

- Consider Parallel Plates: find C from geometry



Knowing: $C = \frac{Q}{V}$

$$C = \frac{\int \epsilon_0 \vec{E} \cdot d\vec{s}}{-\int \vec{E} \cdot d\vec{e}}$$

$$Q = \int \epsilon_0 \vec{E} \cdot d\vec{s} = \int \epsilon_0 E(-\hat{z}) \cdot (-\hat{z}) dS = \epsilon_0 E \int dS = \epsilon_0 EA$$

$$\therefore Q = \epsilon_0 EA$$

$$V = -\int \vec{E} \cdot d\vec{e} = -\int E(-\hat{z}) \cdot \hat{z} dz = Ed \Rightarrow V = Ed$$

$$C = \frac{Q}{V} = \frac{\epsilon_0 EA}{Ed} \Rightarrow C = \frac{\epsilon_0 A}{d} \text{ [F]}$$

4.10: Electrostatic Energy

- consider ideal capacitor with no ohmic losses
- $\sigma \rightarrow \infty$ plates (conductor)
- $\sigma \rightarrow \infty$ dielectric

then, in charging a capacitor, the energy is stored as electrostatic potential energy

electric potential energy per unit charge (q)

$$V = \frac{dW_e}{dq}, \text{ knowing } C = \frac{q}{V} \Rightarrow V = \frac{q}{C}$$

$$\Rightarrow \frac{q}{C} = \frac{dW_e}{dq} \Rightarrow dW_e = \frac{q}{C} dq$$

- if charging from 0 to Q $q = CV$

$$W_e = \int_0^Q \frac{q}{C} dq = \frac{1}{2} \frac{Q^2}{C}$$

$$\boxed{W_e = \frac{1}{2} CV^2 \text{ [J]}}$$

- so far, we know $C = \frac{\epsilon_0 A}{d}$, $V = Ed \Rightarrow E = \frac{V}{d}$ [V/m]
- and $W_e = \frac{1}{2} CV^2 = \frac{1}{2} \frac{\epsilon_0 A}{d} (Ed)^2 = \frac{1}{2} \epsilon_0 E^2 Ad$
 $Ad = \text{Volume } V$
- or $\boxed{W_e = \frac{1}{2} \int_V \epsilon_0 E^2 dV}$ $W_e = \frac{1}{2} \int$

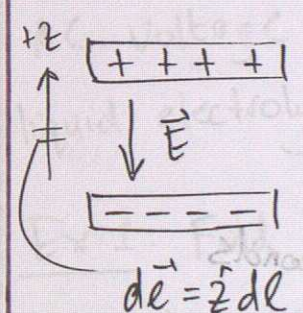
- connecting E and W and others:

$$\boxed{W_e = \frac{1}{2} \int_V \epsilon_0 E^2 dV \text{ [J]}} \quad \boxed{W_e = \frac{1}{2} \int_V \frac{D^2}{\epsilon_0} dV \text{ [J]}}$$

- Electrostatic Energy density (W_e)
 $\rightarrow$ is defined as energy W_e per unit volume

$$W_e = \frac{W_e}{V} \Rightarrow w_e = \frac{W_e}{V} \Rightarrow \boxed{w_e = \frac{1}{2} \epsilon_0 E^2 \text{ [J/m}^3\text{]}}$$

- According to Coulomb's Law, there is a force b/w (+) and (-) plates in the same direction of $\vec{E}$


 $\Rightarrow$ can write $\vec{F}_e = -F_e \hat{z}$

$$dW_e = \vec{F}_e \cdot d\vec{e}$$

$$= -F_e \hat{z} \cdot \hat{z} dz = -F_e dz$$

$$F_e = -\frac{dW_e}{dz}$$

- note: we can generalize dz (de) along any direction

$$\Rightarrow \boxed{\vec{F}_e = -\nabla W_e} \leftarrow \text{similar to } \vec{E} = -\nabla V$$

- recall $W_e = \frac{1}{2} \frac{\epsilon_0 AV^2}{d} \xrightarrow{\text{can write}} dW_e = \frac{1}{2} \epsilon_0 AV^2 \left(-\frac{1}{d^2} dz\right)$
 $(d=z)$

$$dW_e = -\frac{1}{2} \frac{\epsilon_0 A}{d^2} V^2 dz \leftarrow \text{sub in } F_e = -\frac{dW_e}{dz}$$

$$F_e = -\frac{1}{dz} \left(-\frac{1}{2} \frac{\omega A V^2}{z^2} dz \right)$$

$$\vec{F}_e = \frac{1}{2} \frac{\omega A V^2}{z^2} \hat{z} \quad \text{---} \quad z=d$$

$$\boxed{\vec{F}_e = \frac{1}{2} \omega A \frac{V^2}{d^2} \hat{z}} \quad [N]$$

* supercapacitor

* suppose 1 Farad, $d = 1 \text{ mm}$
 $\epsilon_r = 4$

$$C = \frac{\epsilon_0 \epsilon_r A}{d} \Rightarrow A = 28.3 \times 10^6 \text{ [m}^2\text{]}$$

* suppose 25 V, $C = 1 \text{ F}$

$$W = \frac{1}{2} C V^2 = \frac{1}{2} (1) (25)^2 = 312.5 \text{ J}$$

means can have 100 W light bulb ≈ 3 seconds

2W LED for 2.6 min

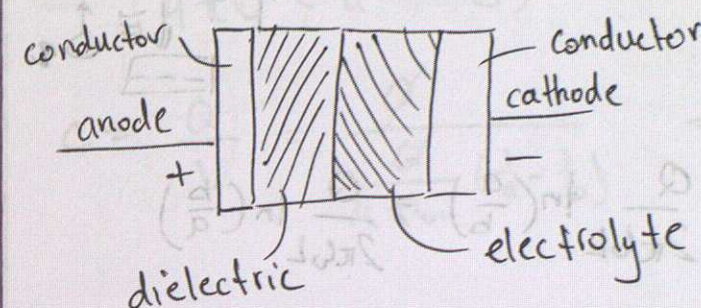
Amazon: 20 x 3000 F @ 2.7 [V] \$1540
\$1659

Week 5: Lecture 2

Feb 5, 2025

Electrolytic Capacitor

* has an asymmetrical construction, hence, has positive (anode) and negative (cathode) polarities



- * has high capacitance
- * good for low frequency filtering and smoothing rectified AC voltage
- * liquid electrolyte can dry out over time

Ex 1: Find capacitance of coaxial capacitor filled with dielectric ϵ_r and charge $+Q$ and $-Q$ where $L \gg b$

Knowing $C = \frac{Q}{V}$

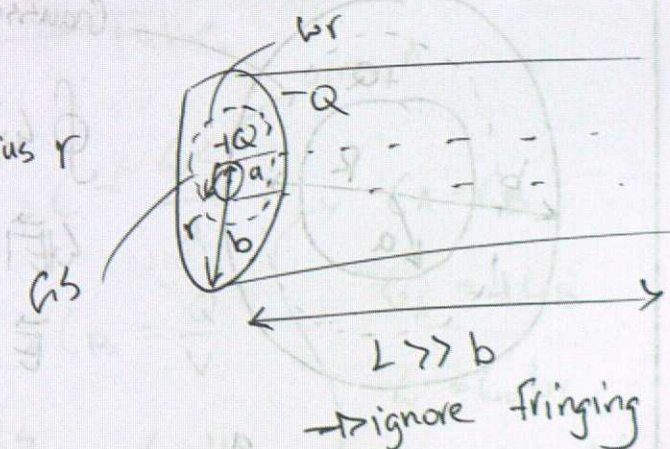
Use cylinder G.S. with radius r

Apply Gauss Law

$$\oint \vec{E} \cdot d\vec{s} = Q_{enc} = Q$$

$$E 2\pi r L = Q$$

$$\vec{E} = \frac{Q}{2\pi \epsilon_0 L r} \hat{r}$$

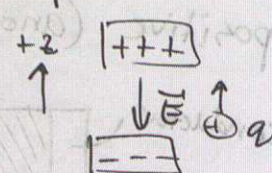


→ coaxial shape maybe on mid.

Q: what Q do we take? →

$$V = - \int_L \vec{E} \cdot d\vec{r} = - \int_b^a \frac{Q}{2\pi\epsilon_0 L r} \hat{r} \cdot \hat{r} dr$$

go against the field as per def:

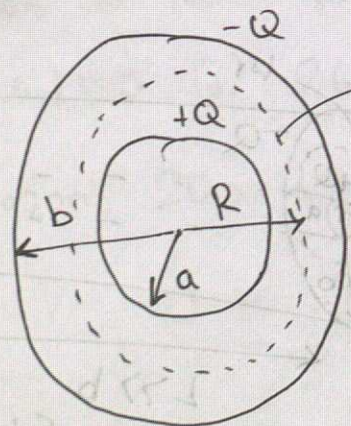


$$= \frac{-Q}{2\pi\epsilon_0 L} \int_b^a \frac{1}{r} dr$$

$$= \frac{-Q}{2\pi\epsilon_0 L} (\ln r)_b^a = -\frac{Q}{2\pi\epsilon_0 L} \ln\left(\frac{a}{b}\right) = \frac{Q}{2\pi\epsilon_0 L} \ln\left(\frac{b}{a}\right)$$

$$C = \frac{Q}{V} = \frac{Q}{\frac{Q}{2\pi\epsilon_0 L} \ln(b/a)} = \frac{2\pi\epsilon_0 L}{\ln(b/a)} [F]$$

Ex 2: Find capacitance of spherical capacitor: two concentric spherical conductors separated by dielectric with ϵ_0 and having charges $+Q$ and $-Q$



Gaussian surface

$$\oint \epsilon_0 \vec{E} \cdot d\vec{s} = Q_{enc}$$

$$\epsilon_0 E 4\pi R^2 = Q$$

$$\vec{E} = \frac{Q}{4\pi\epsilon_0 R^2} \hat{r}$$

$$V = - \int_b^a \vec{E} \cdot d\vec{r} = - \int_b^a \frac{Q}{4\pi\epsilon_0 R^2} \hat{r} \cdot \hat{r} dR$$

$$V = - \frac{Q}{4\pi\epsilon_0} \int_b^a \frac{dR}{R^2} = \frac{-Q}{4\pi\epsilon_0} \left(\frac{-1}{R} \right)_b^a$$

$$= \frac{Q}{4\pi\epsilon_0} \left(\frac{1}{a} - \frac{1}{b} \right)$$

$$C = \frac{Q}{V} = \frac{Q}{\frac{Q}{4\pi\epsilon_0} \left(\frac{1}{a} - \frac{1}{b} \right)} = \frac{4\pi\epsilon_0}{\frac{1}{a} - \frac{1}{b}} [F]$$

Ex 3: Capacitor

	Area	Spacing	charge	Voltage
Cap A	S	d	Q	V
Cap B	2S	d/2	Q	V

Is it true that cap B have has a dielectric more easily polarized? → False

$$\chi_e = \epsilon_r + 1, q = CV, C = \frac{\epsilon S}{d}$$

$$C = \frac{Q}{V} \Rightarrow C_A = \frac{Q}{V}, C_B = \frac{Q}{V}$$

$$C_A = \frac{\epsilon_A S}{d}, C_B = \frac{\epsilon_B 2S}{d/2} = \frac{\epsilon_B 4S}{d}$$

area A

$$C_A = C_B$$

$$\epsilon_A = 4\epsilon_B$$

$$\epsilon = \epsilon_0 \epsilon_r$$

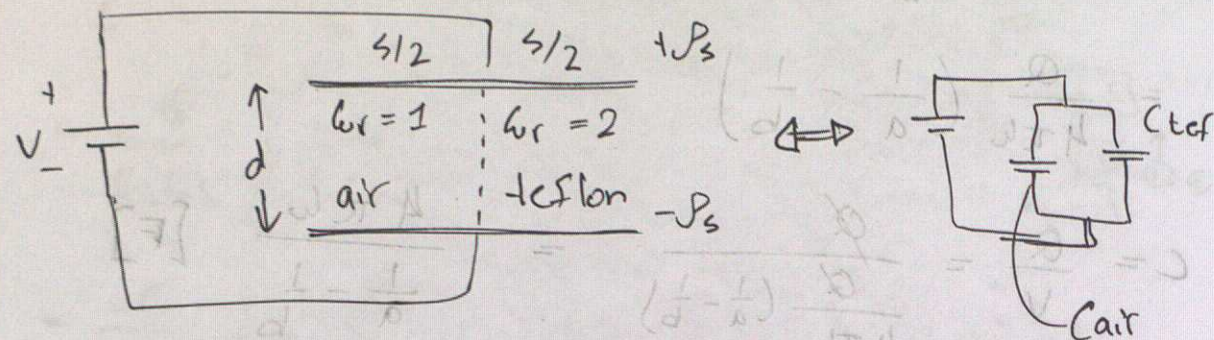
$$\Rightarrow \epsilon_{rA} = 4\epsilon_{rB}$$

$$\Rightarrow \chi_{eA} = \epsilon_{rA} + 1 \gg \chi_{eB} = \frac{1}{4}\epsilon_{rA} + 1$$

∴ Cap A more receptive than Cap B ... ∴ False

★ go on
back
and
do for
exam

Ex 4: Compare surface charge densities $\rho_{s,air}$ and $\rho_{s,tef}$



$$d_{air} = d_{tef}$$

$$V_{air} = V_{tef} \rightarrow E_{air} = E_{tef}$$

$$D_{air} = \epsilon_0 \epsilon_r E$$

$$D_{tef} = \epsilon_0 \epsilon_r E$$

$$D_{air} = \epsilon_0 \epsilon_r E = \epsilon_0 E = \rho_{s,air}$$

$$D_{tef} = \epsilon_0 \epsilon_r E = 2\epsilon_0 E = \rho_{s,tef}$$

$$\therefore \rho_{s,tef} > \rho_{s,air}$$

$$\rho_{s,tef} = 2\rho_{s,air}$$

Compare total charge Q_{air} and Q_{tef}

$$C = \frac{\epsilon_0 \epsilon_r S}{d}, C_{air} = \frac{\epsilon_0 \epsilon/2}{d}, C_{tef} = \frac{2\epsilon_0 \epsilon/2}{d}$$

$$C_{tef} = 2C_{air}, Q = CV \rightarrow Q_{air} = C_{air} V$$

$$Q_{tef} = C_{tef} V = 2C_{air} V$$

$$\rightarrow Q_{tef} = 2Q_{air}$$

Week 5 lecture 3

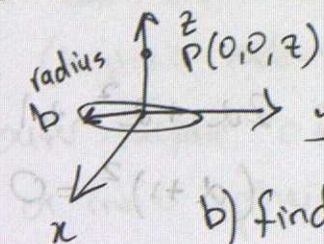
Midterm 2014

Q3

Consider a ring on xy-plane: a) sketch variation of ρ_ℓ

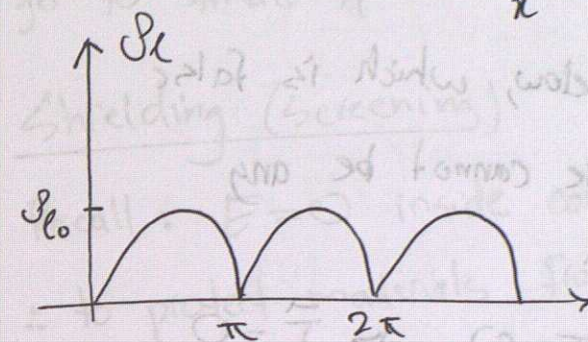
$$\rho_\ell = \rho_{\ell 0} |\sin \phi|$$

positive constant



b) find $\vec{D}$ and $\vec{V}$ at $P(0,0,z)$

a)



$$dl = b d\phi \rightarrow dq = \rho_\ell b d\phi$$

$$V = \int \frac{dq}{4\pi\epsilon_0 |\vec{r} - \vec{r}_i|}$$

b)

$$V = \int_0^{2\pi} \frac{\rho_{\ell 0} |\sin \phi| b d\phi}{4\pi\epsilon_0 \sqrt{b^2 + z^2}} d\phi = 2 \int_0^\pi \frac{\rho_{\ell 0} \sin \phi b d\phi}{4\pi\epsilon_0 \sqrt{b^2 + z^2}}$$

$$= \frac{\rho_{\ell 0} b}{2\pi\epsilon_0 \sqrt{b^2 + z^2}} \int_0^\pi \sin \phi d\phi = \frac{\rho_{\ell 0} b}{2\pi\epsilon_0 \sqrt{b^2 + z^2}} (-\cos \pi + \cos 0)$$

$$= \frac{\rho_{\ell 0} b}{\pi\epsilon_0 \sqrt{b^2 + z^2}} [V] \rightarrow \text{to find } D, \text{ knowing } \vec{E} = -\nabla V$$

$$\vec{D} = \epsilon_0 \vec{E} \Rightarrow \vec{D} = \epsilon_0 (-\nabla V)$$

$$\Rightarrow \vec{D} = \epsilon_0 \left(\frac{\partial}{\partial z} [V] \right) = \epsilon_0 \frac{\partial}{\partial z} \left[\frac{\rho_{\ell 0} b}{\pi\epsilon_0 \sqrt{b^2 + z^2}} \right] \hat{z}$$

$$\vec{D} = -\frac{\rho_{\ell 0} b}{\pi} \hat{z} \left(-\frac{1}{2} (b^2 + z^2)^{-3/2} (2z) \right)$$

$$\vec{D} = \frac{\rho_{\ell 0} b}{\pi} \frac{z}{(b^2 + z^2)^{3/2}} \hat{z} \quad [C/m^2]$$

Ex 2: Given that $\vec{A} = 2\alpha \hat{x} + \hat{y} + \hat{z}$ and $\vec{B} = \hat{x} + \alpha^2 \hat{y} + \hat{z}$. If $\vec{A}$ and $\vec{B}$ are normal to each other, then what is α ?

$$\vec{A} \cdot \vec{B} = 0 \Rightarrow 2\alpha + \alpha^2 + 1 = 0$$

$$(\alpha + 1)^2 = 0 \Rightarrow \underline{\underline{\alpha = -1}}$$

Ex 3: From the statements below, which is false

(A) In a perfect dielectric, there cannot be any current or any electric field

$$\vec{J} = \sigma \vec{E} \text{ dielectric} \Rightarrow \sigma = 0 \Rightarrow \vec{J} = 0$$

but $E \neq 0$

T B) A perfectly conducting material requires no applied field for current to flow inside it.

$$\vec{J} = \sigma \vec{E} \Rightarrow \sigma \rightarrow \infty \Rightarrow \vec{J} \rightarrow \infty$$

no E required

$$E = \frac{J}{\sigma} = \frac{0}{\sigma} = 0 \rightarrow E = \frac{J}{\sigma} = \frac{\text{something}}{\infty} = 0$$

T c) A perfect dielectric always has a zero current inside it

T d) A perfect conductor always has a zero electric field inside it

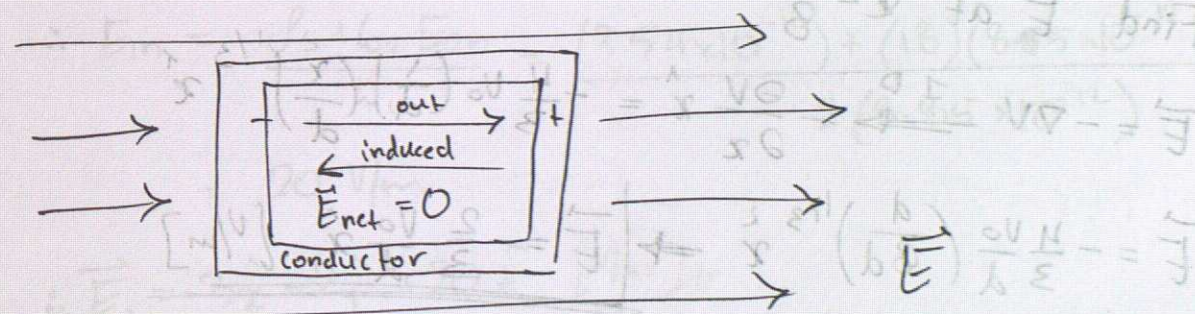
Ex 4:

- the charges are same sign, they don't like each other and want to be as far away from each other as possible $\rightarrow$ only on outer surface of shell (highest radius, surface)
- charge $\therefore$ stays on outer surface of hollow sphere, doesn't go to small sphere or inner sphere

Shielding (Screening)

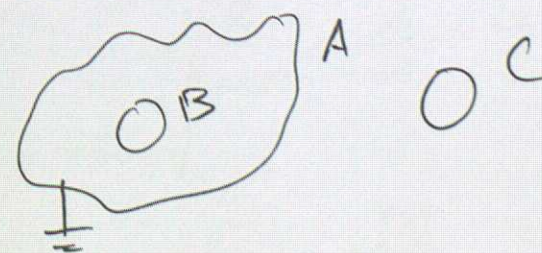
Recall: $E = 0$ inside conductor

$\therefore$ to protect materials from external $\vec{E}$, then ~~by~~ hollow surround them by hollow conductors



$\vec{E}_{\text{external}}$ causes charges to rearrange, then the resulting E_{net} becomes zero

Ex 5: Consider hollow A conductor at potential zero then A screens B from outside and C from B

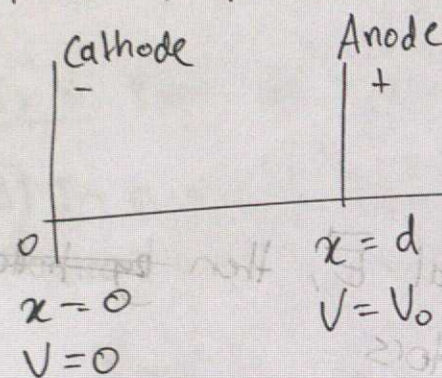


Ex 4: Consider a 2-plate cap with

$$V = V_0 \left(\frac{x}{d} \right)^{4/3} [V] \text{ where } V_0 \text{ is constant and}$$

d is spacing with $0 \leq x \leq d$

a) Find $V = ?$ @ $x = \frac{d}{8}$



$$V = V_0 \left(\frac{d}{8d} \right)^{4/3} = V_0 \left(\frac{1}{8} \right)^{4/3} = \frac{V_0}{4} [V]$$

b) Find E at $x = \frac{d}{8}$

$$\vec{E} = -\nabla V \xrightarrow{1D} -\frac{\partial V}{\partial x} \hat{x} = -\frac{4}{3} V_0 \left(\frac{1}{d} \right) \left(\frac{x}{d} \right)^{1/3} \hat{x}$$

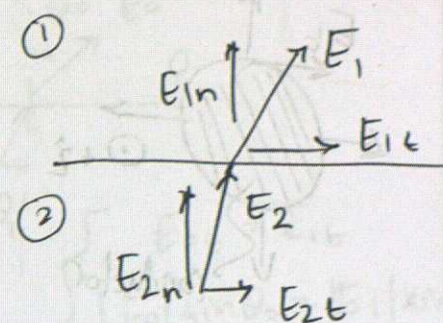
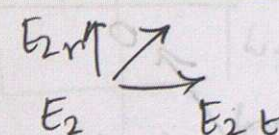
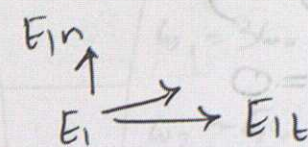
$$\vec{E} = -\frac{4}{3} \frac{V_0}{d} \left(\frac{d}{8d} \right)^{1/3} \hat{x} \Rightarrow \vec{E} = -\frac{2}{3} \frac{V_0}{d} \hat{x} [V/m]$$

↑
plus x

4.118:

$$\vec{E}_2 = 3\hat{x} - 2\hat{y} + 2\hat{z} [V/m]$$

a)



$$E_{2t} = 3\hat{x} - 2\hat{y} \text{ and } \boxed{E_{1t} = E_{2t}} = 3\hat{x} - 2\hat{y}$$

$$E_{2n} = 2\hat{z} = E_{2z} \quad \left[(\vec{D}_1 - \vec{D}_2) \cdot \hat{n} = \rho_s \right]$$

$$\hat{z} (\epsilon_1 E_{1n} \hat{z} - \epsilon_2 E_{2n} \hat{z}) = \rho_s$$

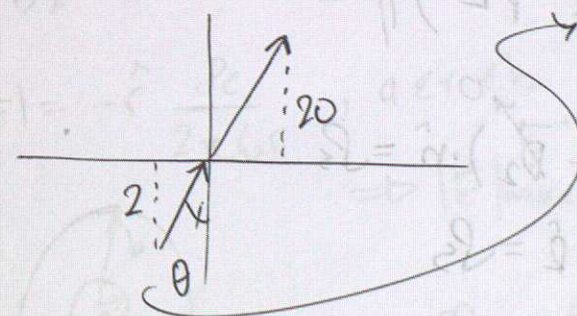
$$\epsilon_1 E_{1n} - \epsilon_2 E_{2n} = \rho_s$$

$$\therefore E_{1n} = \frac{\rho_s + \epsilon_2 E_{2n}}{\epsilon_1} = \frac{(3.54 \times 10^{-11}) + (18)(8.85 \times 10^{-12})(2)}{2(8.85 \times 10^{-12})}$$

$$= 20 V/m$$

$$\therefore \vec{E}_1 = 3\hat{x} - 2\hat{y} + 20\hat{z} [V/m]$$

b)

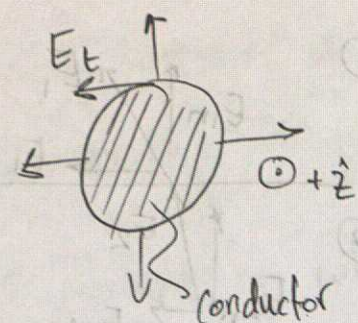


$$|\vec{E}_1| \cos \theta = E_{1z} = 20$$

$$\theta = \arccos \left(\frac{2}{\sqrt{3^2 + 2^2 + 20^2}} \right)$$

$$\theta \approx 61^\circ$$

4.49:



$$\vec{E} = \hat{r} E_r + \hat{\phi} E_\phi$$

$$\text{and } \nabla \cdot \vec{D} = 0$$

$$\vec{D} = \epsilon_0 \vec{E}$$

$$\nabla \cdot \vec{E} = \frac{1}{r} \frac{\partial}{\partial r} (r E_r) + \frac{1}{r} \frac{\partial}{\partial \phi} (E_\phi) + \frac{\partial}{\partial z} (E_z)$$

$$\Rightarrow \frac{1}{r} \frac{\partial}{\partial r} (r E_r) + \frac{1}{r} \frac{\partial}{\partial \phi} (E_\phi) = 0$$

$$\frac{\partial}{\partial r} (r E_r) + \frac{1}{r^2} (+\sin \phi) = 0 \quad \rightarrow \quad E_r = \frac{\sin \phi}{r^2}$$

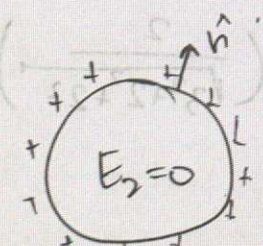
$$\frac{\partial}{\partial r} (r E_r) = -\frac{1}{r^2} \sin \phi$$

$$\int \partial r E_r = \int -\frac{1}{r^2} \sin \phi \cdot dr$$

$$r E_r = -\sin \phi \int \frac{1}{r^2} dr = -\sin \phi \left(-\frac{1}{r} \right)$$

$$\therefore \vec{E} = \hat{r} \left(\frac{\sin \phi}{r^2} \right) - \hat{\phi} \left(\frac{\cos \phi}{r^2} \right)$$

4.50:



$E_1 \neq 0$

$$(\vec{D}_1 - \vec{D}_2) \cdot \hat{n} = \rho_s$$

$$\vec{D}_1 \cdot \hat{n} = \rho_s$$

$$\epsilon_0 E_{1n} = \rho_s$$

$$E_{1n} = \frac{\rho_s}{\epsilon_0} = \frac{Q}{4\pi\epsilon_0 R^2}$$

$$Q = \int \rho_s dS$$

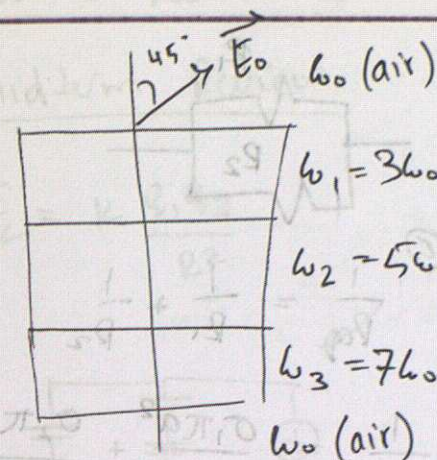
$$\rho_s = \frac{Q}{4\pi R^2}$$

$$\therefore Q = (150)(4\pi\epsilon_0)(0.05)^2$$

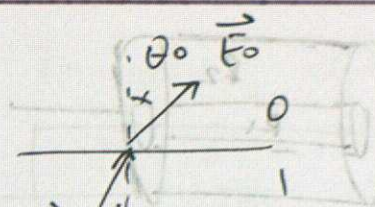
$$Q = 4.2 \times 10^{-11} \text{ [C]}$$

$$R = 5 \text{ cm}$$

4.51:



(A)



$$\begin{cases} E_{0t} = E_{1t} \\ |E_0| \sin \theta_0 = |E_1| \sin \theta_1 \end{cases} \quad \text{--- (1)}$$

$$D_{0n} - D_{1n} = 0$$

$$\Rightarrow D_{0n} = D_{1n}$$

$$\epsilon_0 E_{0n} = \epsilon_1 E_{1n}$$

$$\epsilon_0 |E_0| \cos \theta_0 = \epsilon_1 |E_1| \cos \theta_1 \quad \text{--- (2)}$$

since no charges on surface:

divide (1) ÷ (2)

$$\frac{\tan \theta_0}{\epsilon_0} = \frac{\tan \theta_1}{\epsilon_1}$$

$$\theta_1 = \arctan \left(\frac{\epsilon_1}{\epsilon_0} \tan \theta_0 \right) \quad \leftarrow \text{use this for every part}$$

$$\theta_2 = \arctan \left(\frac{\epsilon_2}{\epsilon_1} \tan \theta_1 \right) \quad \leftarrow \text{and work your way backwards}$$

$$\theta_3 = \arctan \left(\frac{\epsilon_3}{\epsilon_2} \tan \theta_2 \right)$$

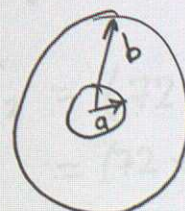
$$\theta_1 = \arctan \left(3 \arctan \left(\frac{\pi}{4} \right) \right) = 1.249 \text{ rad}$$

$$\theta_2 = \arctan \left(\frac{\pi}{3} \arctan(\dots) \right) \dots \dots$$

4.53:

$$|E| = -\hat{r} \frac{\rho_c}{2\pi b r}, \quad a \leq r \leq b \quad \text{and max } |E| \text{ at } r=a$$

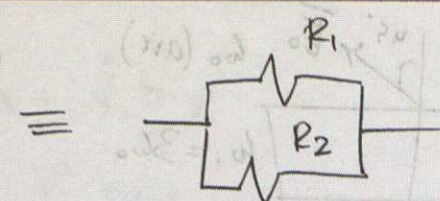
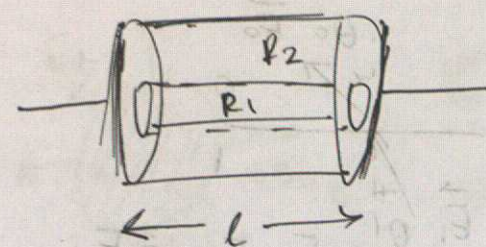
$$\Rightarrow |E|_{\max} = \frac{\rho_c}{2\pi b a} \quad \text{200 MV} \quad \text{from data table}$$



$$\rho_c = (200 \times 10^6)(2\pi)(8.85 \times 10^{-12})(0.01)(6) = 667.6 \times 10^{-6} \text{ C/m}$$

$$V_{ab} = \frac{\rho_c}{2\pi\epsilon_0\epsilon_r} \ln \left(\frac{b}{a} \right) = \frac{(667.6 \times 10^{-6})}{2\pi(6)(8.85 \times 10^{-12})} \ln \left(\frac{2}{1} \right) = 1.39 \times 10^6 \text{ [V]}$$

4.44



$$\text{inner: } \pi a^2 = A_1 \quad (1)$$

$$\text{outer: } \pi(b^2 - a^2) = A_2 \quad (2)$$

$$R_1 = \frac{l_1}{\sigma_1 A_1} \quad \text{and} \quad R_2 = \frac{l_1}{\sigma_2 A_2}$$

$$(3) \quad \frac{l_1}{\sigma_1 \pi a^2} \quad (4) \quad \frac{l_1}{\sigma_2 \pi(b^2 - a^2)}$$

$$\therefore R_{eq} = \frac{l}{\pi[\sigma_1 a^2 + \sigma_2(b^2 - a^2)]}$$

$$4.54.a) \quad \frac{V}{d} = E = 1.6 \times 10^{-16} \text{ H}$$

$$b) \quad F_{net} = ma \Rightarrow a = 1.76 \times 10^{-14} \text{ m/s}^2$$

$$c) \quad d = v_0 t + \frac{1}{2} a t^2 \Rightarrow t = \sqrt{\frac{2d}{a}} \Rightarrow 10.7 \times 10^{-9} \text{ s}$$

$$4.55: \quad W_c = \frac{1}{2} \int_0^3 \int_0^2 \int_{-1}^1 \epsilon [(x^2 + 2z)^2 + x^4 + (y + z)^2] dx dy dz$$

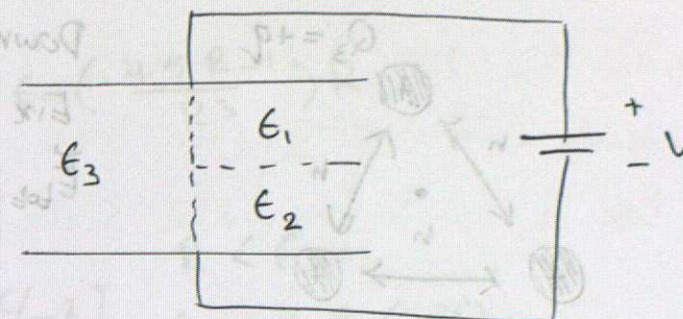
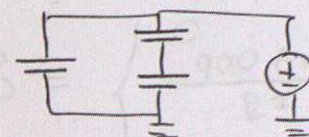
$$4.57.a) \quad C = C_1 + C_2 = \frac{\epsilon_1 A_1}{d} + \frac{\epsilon_2 A_2}{d}$$

Week 6: Lecture 1

Feb 11, 2025

Midterm Review

$$\vec{E} = k \frac{q_1 q_2}{r^2}$$

Ex 1: Find $\vec{E}$ @ $P(2\text{cm}, 0, 0)$

Apply superposition

$$\vec{E}_{tot} = \vec{E}_1 + \vec{E}_2$$

$$\vec{E}_1 = k \frac{Q_1}{r_1^2} \hat{x}$$

$$= \frac{(9 \times 10^9)(1 \times 10^{-6})}{(0.03)^2} \hat{x} = 10^7 \hat{x} \text{ [N/C]}$$

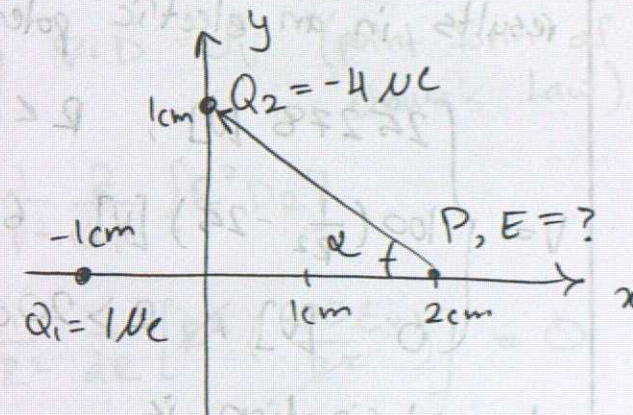
$$E_2 = k \frac{Q_2}{r_2^2} = \frac{(9 \times 10^9)(4 \times 10^{-6})}{(\sqrt{1^2 + 2^2} \times 10^{-2})^2} = 72 \times 10^6 \text{ [N/C]}$$

$$\text{direction } \alpha = \tan^{-1}(\frac{1}{2}) \approx 26.6^\circ$$

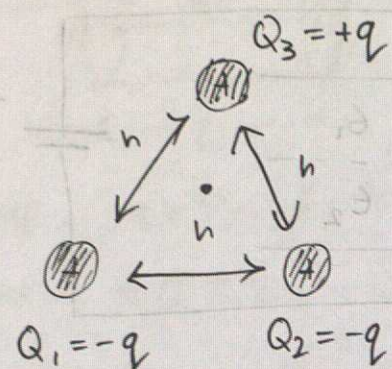
$$\vec{E}_2 = (72 \times 10^6)(-\cos 26.6^\circ \hat{x} + \sin 26.6^\circ \hat{y})$$

$$= (72 \times 10^6)(-0.89 \hat{x} + 0.45 \hat{y})$$

$$\vec{E}_{tot} = -54.4 \times 10^6 \hat{x} + 32.3 \times 10^6 \hat{y} \text{ [N/C]}$$



Ex 2: Find direction of $\vec{E}$ at the center



Downward:

$$E_{1x} = E_{2x} \rightarrow \text{cancel}$$

$$\vec{E}_{\text{tot}} = \vec{E}_3 + \vec{E}_{1y} + \vec{E}_{2y}$$

Ex 3: A certain collection of charge distribution results in an electric potential field given by:

$$V = \begin{cases} 25278 \text{ [V]}, & R < 6 \text{ cm} \\ 100 \left(\frac{1}{R^2} - 25 \right) \text{ [V]}, & 6 \text{ cm} \leq R \leq 20 \text{ cm} \\ 0 \text{ [V]}, & R > 20 \text{ cm} \end{cases}$$

also, polarization is

$$\vec{P} = \begin{cases} 0 \text{ [C/m}^2\text{]}, & R < 6 \text{ cm} \\ 200 \epsilon_0 \left(\frac{4.5R-1}{R^3} \right) \hat{R} \text{ [C/m}^2\text{]}, & 6 \text{ cm} \leq R \leq 20 \text{ cm} \\ 0 & R > 20 \text{ cm} \end{cases}$$

a) Find $\vec{E}$: $\vec{E} = -\nabla V$

$$\vec{E} = \begin{cases} 0 & R < 6 \text{ cm} \\ -\frac{d}{dR} \left(100 \left(\frac{1}{R^2} - 25 \right) \right) = -100 \left(-\frac{2}{R^3} \right) R^2 & 6 \text{ cm} \leq R \leq 20 \text{ cm} \\ 0 & R > 20 \text{ cm} \end{cases}$$

$$\vec{E} = \begin{cases} 0 & R < 6 \text{ cm} \\ \frac{200}{R^3} \hat{R} & 6 \text{ cm} \leq R \leq 20 \text{ cm} \\ 0 & R > 20 \text{ cm} \end{cases}$$

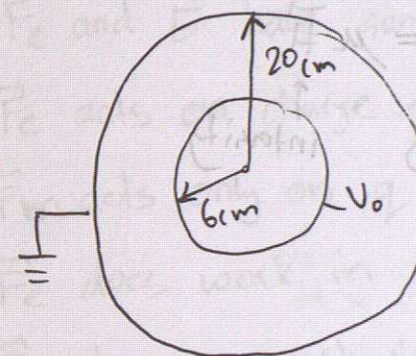
b) Find $\vec{D}$: $\vec{D} = \epsilon_0 \vec{E} + \vec{P}$

$$\vec{D} = \begin{cases} 0 & R < 6 \text{ cm} \\ \frac{200}{R^3} \hat{R} + 200 \epsilon_0 \left(\frac{4.5R-1}{R^3} \right) \hat{R} & 6 \text{ cm} \leq R \leq 20 \text{ cm} \\ 0 & R > 20 \text{ cm} \end{cases}$$

$$\vec{D} = \begin{cases} 0 & R < 6 \text{ cm} \\ \frac{900 \epsilon_0}{R^2} \hat{R} \text{ [C/m}^2\text{]} & 6 \text{ cm} \leq R \leq 20 \text{ cm} \\ 0 & R > 20 \text{ cm} \end{cases}$$

c) Describe charge distribution

Knowing $\nabla \cdot \vec{D} = \rho_V$ (point form of Gauss's Law)



$$\nabla \cdot \vec{D} = \frac{1}{R^2} \frac{\partial}{\partial R} [R^2 D_R]$$

$$= \frac{1}{R^2} \frac{d}{dR} [R^2 \left(\frac{900 \epsilon_0}{R^2} \right)] = 0$$

$\Rightarrow$ since $\nabla \cdot \vec{D} = 0$, $\therefore$ no volume charge

$\therefore$ field must be due to surface charge

Q: why $\rho_s = D$?

$$\rho_s|_{6\text{cm}} = D|_{6\text{cm}} = \frac{900 \epsilon_0}{(6 \times 10^{-2})^2} = 2.21 \times 10^{-6} \text{ [C/m}^2\text{]}$$

$$\rho_s|_{20\text{cm}} = -D|_{20\text{cm}} = \frac{-900 \epsilon_0}{(20 \times 10^{-2})^2} = -0.199 \times 10^{-6} \text{ [C/m}^2\text{]}$$

d) Find C and Energy:

$$C = \frac{Q}{V} = \frac{\rho_s|_{6\text{cm}} 4\pi R^2}{25278} = \frac{(2.21 \times 10^{-6})(4\pi)(6 \times 10^{-2})^2}{25278} = 3.96 \text{ pF}$$

$$W_c = \frac{1}{2} CV^2 = \frac{1}{2} (3.96 \text{ pF})(25278)^2 = 1.26 \text{ mJ}$$

Chapter 5: Magnetostatics

- stationary charge (Q) $\rightarrow \vec{E}$ (static electric field)
- steady (non-varying) (non-time varying) current (I)
 $\rightarrow \vec{H}$ (static magnetic field)

Electrostatic

$$\nabla \cdot \vec{D} = \rho_v$$

$$\nabla \times \vec{E} = 0$$

$$\vec{D} = \epsilon \vec{E}$$

↑ density ↑ intensity

Magnetostatic

$$\nabla \cdot \vec{B} = 0$$

$$\nabla \times \vec{H} = \vec{J}$$

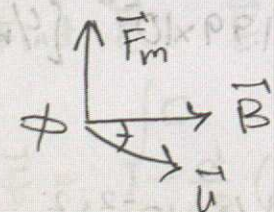
$$\vec{B} = \mu \vec{H}$$

↑ density ↑ intensity

5.1: Magnetic Force & Torque

→ define magnetic flux density ($\vec{B}$)

- give a test charge ($+q$) with velocity $\vec{u}$ through point P
- if a force $\vec{F}_m$ acts on moving $+q$, then a magnetic field $\vec{B}$ is present at point P such that:



$$\phi = 0 \Rightarrow F_m = 0$$

$$\phi = 90^\circ \Rightarrow F_m \text{ is max}$$

} observation

$$F_m = q u B \sin \phi$$

other unit: (non SI)

Gauss $[G] \Rightarrow T$

$$\vec{F}_m = q \vec{u} \times \vec{B}$$

$$1T = 10^4 G$$

$$[T] \text{ Tesla} = \left[\frac{H}{C \cdot \frac{m}{s}} \right] = \left[\frac{N}{A \cdot m} \right]$$

Notes:

- direction of F_m is given by R.H. rule.
- if both $\vec{E}$ and $\vec{B}$ are present, then electromagnetic force is $\vec{F} = \vec{F}_e + \vec{F}_m$
 $= q\vec{E} + q\vec{u} \times \vec{B}$

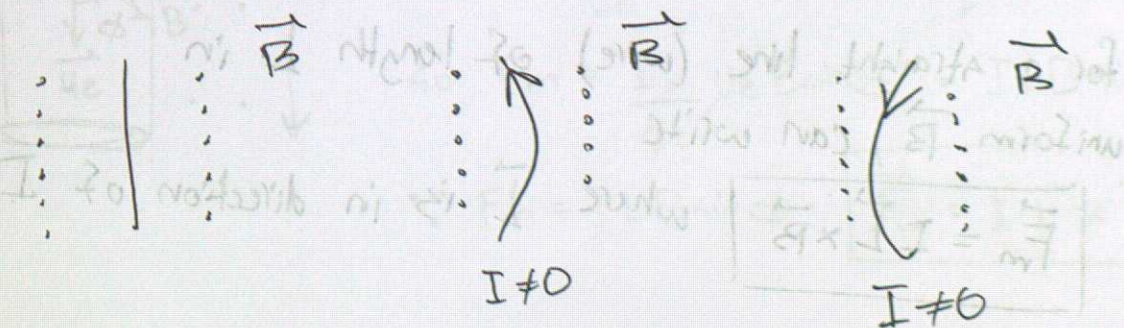
$$\boxed{\vec{F} = q(\vec{E} + \vec{u} \times \vec{B})} \leftarrow \text{Known as Lorentz Force}$$

Differences between F_e and F_m

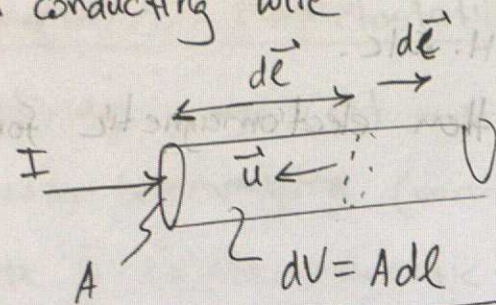
- $\vec{F}_e$ and $\vec{E}$ have same direction, but $\vec{F}_m$ and $\vec{B}$ are $\perp$
- $\vec{F}_e$ acts on charge particle both in motion and stationary
- $\vec{F}_m$ acts only on q in motion ($\vec{u} \neq 0$)
- $\vec{F}_e$ does work in moving q
- $\vec{F}_m$ does no work in moving q ; it only changes direction

5.1-1: Magnetic Force on Current-Carrying Conductor (wire)

- Note: $\vec{B}$ exerts a sideways force on a moving charge
- current (I) is moving charges
 $\Rightarrow \vec{B}$ should also exert a sideways force on the current-carrying conductor.



→ For conducting wire



can write # of carriers per unit volume

$$n_{ve} = -N_e e$$

free electron charge density per unit volume

$$\text{then } dq = n_{ve} A dl$$

$$= -N_e e A dl$$

$$\text{but } d\vec{F}_m = dq \vec{u}_e \times \vec{B}$$

$$= -N_e e A dl \vec{u}_e \times \vec{B}$$

then can write $dl \vec{u}_e = -d\vec{e} u_e$

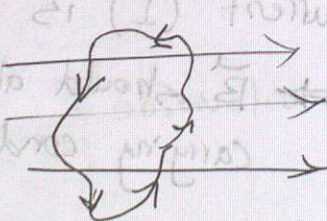
$$\text{sub that: } \Rightarrow d\vec{F}_m = N_e e A u_e d\vec{e} \times \vec{B}$$

$$\therefore d\vec{F}_m = I d\vec{e} \times \vec{B}$$

$$\Rightarrow \boxed{\vec{F}_m = I \oint d\vec{e} \times \vec{B}}$$

Note that vector sum of $d\vec{e}$ over a closed path equals zero

$$\Rightarrow \vec{F}_m = I \oint d\vec{e} \times \vec{B} = 0$$

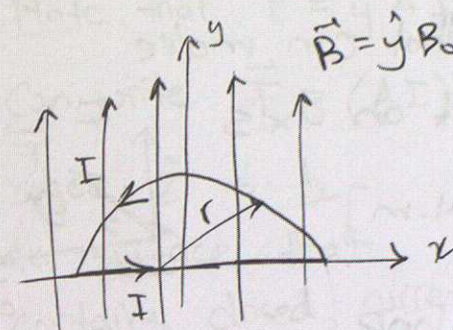


* for a straight line (wire) of length L in uniform $\vec{B}$, can write

$$\boxed{\vec{F}_m = I \vec{L} \times \vec{B}}$$

where $\vec{L}$ is in direction of I

Ex 1: Find force on wire knowing $\vec{F} = I \int d\vec{e} \times \vec{B}$



straight line:

$$\vec{F}_1 = I \int 2r \hat{x} \times \hat{y} B_0$$

$$= I 2r B_0 \hat{z} \Rightarrow \boxed{\vec{F}_1 = 2 I r B_0 \hat{z}}$$

curved half-loop: $\vec{F}_2 = I \int d\vec{e} \times \vec{B}$

$d\vec{e} = r d\phi$, and by RHR, direction is $-\hat{z}$

$$|\vec{F}_2| = I \int d\vec{e} \sin \phi B_0 = I \int_0^\pi r \sin \phi B_0 d\phi = I r B_0 (2)$$

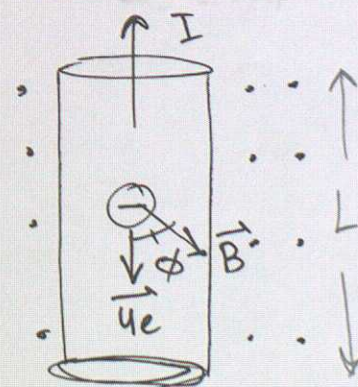
$$\boxed{\vec{F}_2 = 2 r I B_0 (-\hat{z})}$$

take notes

5-1.2: Magnetic Torque on current-carrying loop

Torque: is a measurement of force that can make an object to rotate about an axis

Method 2



time for e to travel distance L is

$$t = \frac{L}{u_e}, \text{ but } I = \frac{dq}{dt} \Rightarrow q = It$$

$$\therefore q = \frac{IL}{u_e}, \text{ but } F_m = q u_e B \sin \phi$$

$$\text{so } F_m = \frac{IL}{u_e} u_e B \sin \phi = IL B \sin \phi$$

$$\therefore F_m = IL B \sin \phi, \boxed{\vec{F}_m = I \vec{L} \times \vec{B}}$$

5-1.2: Magnetic Torque on Current-carrying loop

Torque: Is a measure of force that can make an object to rotate about an axis

$$T = dF \sin \theta \quad \text{or} \quad \vec{T} = \vec{d} \times \vec{F} \quad [\text{N}\cdot\text{m}]$$

→ Magnetic field in the plane of the loop

Knowing: $\vec{F} = I \vec{\ell} \times \vec{B}$

and $\vec{B} = \hat{x} B_0$

$$\vec{F}_1 = I(-\hat{y}b) \times \hat{x} B_0 = \hat{z} I b B_0$$

$$\vec{F}_3 = I(\hat{y}b) \times \hat{x} B_0 = -\hat{z} I b B_0$$

and $\vec{F}_2 = \vec{F}_4 = 0$

Knowing $\vec{T} = d\vec{\ell} \times \vec{F}$

$$\vec{T} = \vec{d}_1 \times \vec{F}_1 + \vec{d}_3 \times \vec{F}_3$$

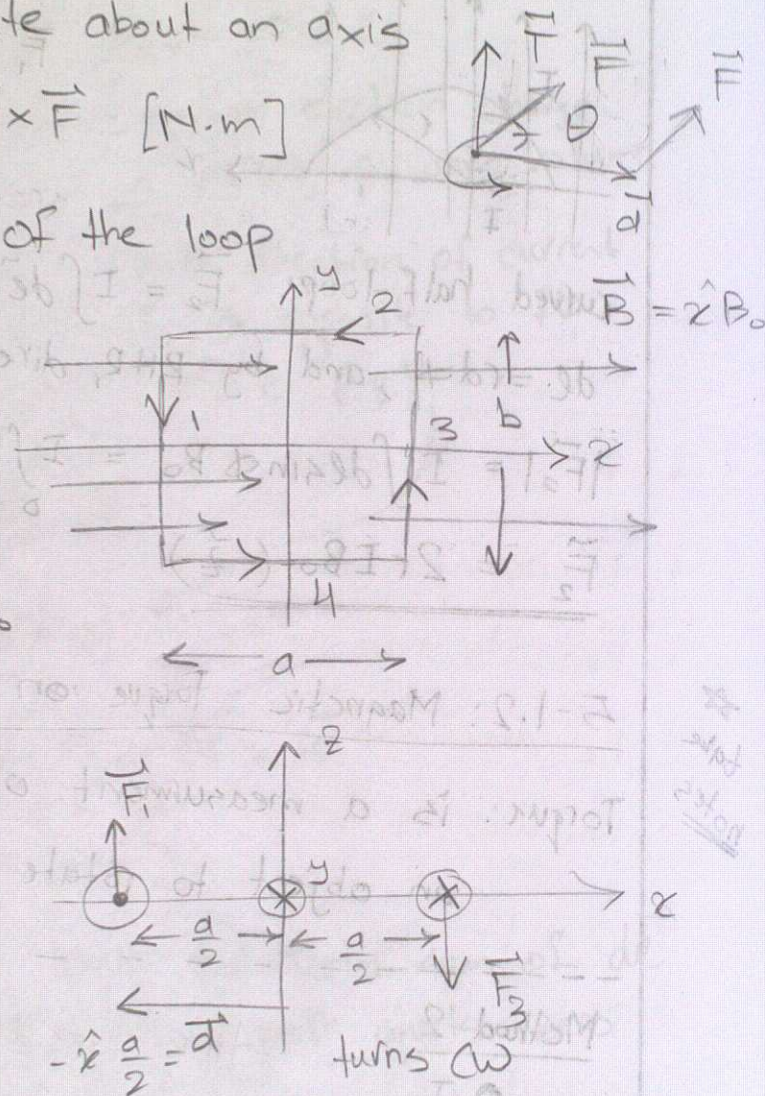
$$= -\hat{x} \frac{a}{2} \times \hat{z} I b B_0$$

$$+ \hat{x} \frac{a}{2} \times -\hat{z} I b B_0$$

$$\vec{T} = \frac{a}{2} I b B_0 (-\hat{x} \times \hat{z} - \hat{x} \times \hat{z})$$

$$= \frac{a}{2} I b B_0 (-2(\hat{x} \times \hat{z}))$$

$$\boxed{\vec{T} = \hat{y} A I B_0}$$



Magnetic Moment ($\vec{m}$)

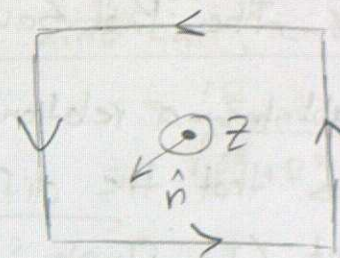
Note that $\vec{T} = \hat{y} A I B_0$

Can write $\vec{T} = (AI) \underbrace{\hat{z} \times \hat{x}}_{\hat{y}} B_0$

where $\hat{z}$ is $\perp$

to surface that

contains closed, current-carrying loop (R.H.R)



⇒ Define magnetic moment as $\vec{m} = AI \hat{z}$

$$\Rightarrow \vec{T} = \vec{m} \times \vec{B}$$

Can also generalize $\vec{m} = AI \hat{z}$ as $\boxed{\vec{m} = AI \hat{n} \text{ [A}\cdot\text{m}^2]}$

where $\hat{n}$ is unit vector normal to surface containing loop.

* if loop has N turns, then

$$\boxed{\vec{m} = N A I \hat{n} \text{ [A}\cdot\text{m}^2]}$$

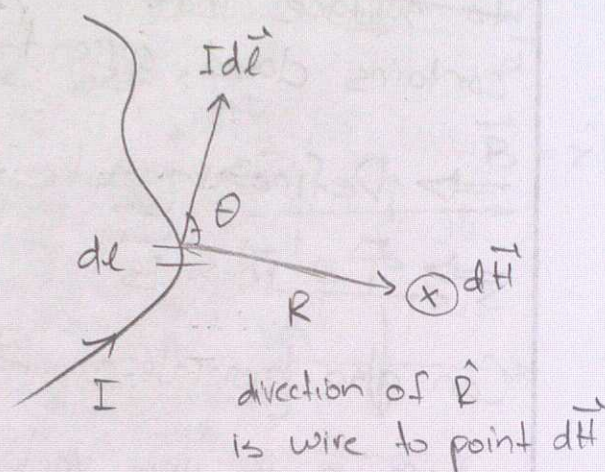
5.2: The Biot-Savart Law (experimental)

- establishes a relationship b/n I and H
- states that the differential $\vec{H}$ ($d\vec{H}$) generated by a steady current (I) flowing through $d\vec{l}$ is:

$$dH = \frac{1}{4\pi} \frac{Idl \sin\theta}{R^2} \quad [A/m]$$

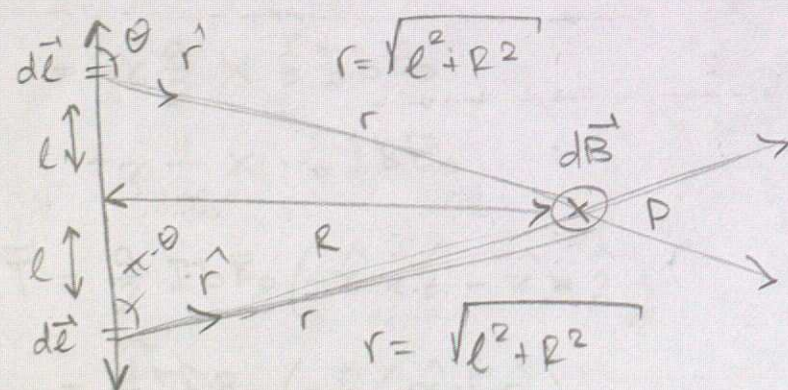
$$d\vec{H} = \frac{I}{4\pi} \frac{d\vec{l} \times \hat{R}}{R^2} \quad [A/m]$$

$$\vec{H} = \frac{I}{4\pi} \int \frac{d\vec{l} \times \hat{R}}{R^2} \quad [A/m]$$



← calculating integral is hard and depends on the path.

Magnetic field due to current in a long straight wire



$$D = \epsilon E$$

$$B = \mu H$$

↑ ↑
density intensity

Apply Biot-Savart Law

$$dB = \frac{\mu_0}{4\pi} \frac{Idl \sin\theta}{r^2}$$

Note Symmetries:

$$\rightarrow B = 2 \int_0^\infty \frac{\mu_0}{4\pi} \frac{Idl \sin\theta}{r^2}$$

$$= \frac{\mu_0 I}{2\pi} \int_0^\infty \frac{\sin\theta dl}{r^2} \quad r = \sqrt{l^2 + R^2}$$

$$= \frac{\mu_0 I}{2\pi} \int_0^\infty \frac{R}{(l^2 + R^2)^{3/2}} dl$$

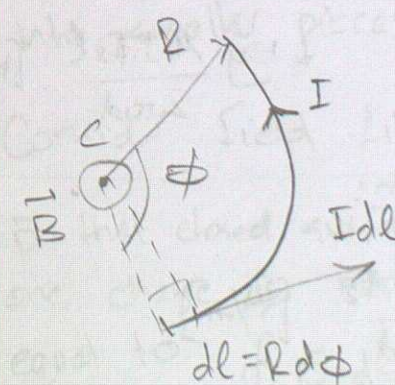
$$= \frac{\mu_0 I}{2\pi} \int_0^\infty \frac{R dl}{(l^2 + R^2)^{3/2}}$$

← solve using tables or substitution

$$B = \frac{\mu_0 I}{2\pi R} \quad [T]$$

magnetic field due to current in a long straight wire (memorize this equation)

Magnetic field due to current in a circular arc of wire. Find $\vec{B}$ at center C due to I



Apply Biot-Savart:

$$d\vec{B} = \frac{\mu_0}{4\pi} \frac{Id\vec{l} \times \hat{r}}{r^2}$$

direction of $\vec{B}$ is outwards

$$dB = \frac{\mu_0}{4\pi} \frac{Idl \sin\theta}{r^2}$$

no matter where dl is, $d\vec{r} \perp \hat{r}$

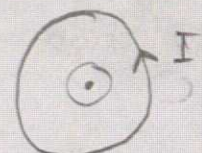
$\Rightarrow \theta = 90^\circ$ and $dl = R d\phi$

$$B = \frac{\mu_0 I}{4\pi} \int \frac{dl}{R^2} = \frac{\mu_0 I}{4\pi} \int_0^\phi \frac{R d\phi}{R^2} = \frac{\mu_0 I}{4\pi R} \int_0^\phi d\phi$$

$$B = \frac{\mu_0 I \phi}{4\pi R} \text{ [T]} \quad \text{magnetic field at center of arc}$$

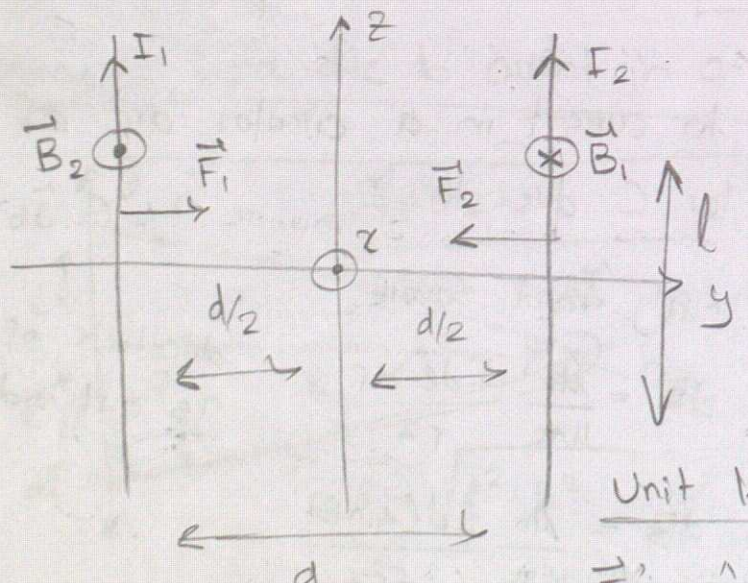
Special Case: Full circle:

Full circle, set $\phi = 2\pi$



$$B = \frac{\mu_0 I}{4\pi R} \int_0^{2\pi} d\phi \rightarrow B = \frac{\mu_0 I}{2R} \text{ [T]} \quad \text{magnetic field at center of a full circle}$$

5-2.3: Magnetic Force between 2 parallel conductors (currents)



parallel attract
opposite repel

$$\vec{B}_1 = -\hat{x} \frac{\mu_0 I_1}{2\pi d}$$

$$\vec{F}_2 = I_2 l \hat{z} \times \vec{B}_1 = -\hat{y} \frac{\mu_0 I_1 I_2 l}{2\pi d} \text{ [N]}$$

Unit length:

$$\vec{F}_2' = -\hat{y} \frac{\mu_0 I_1 I_2}{2\pi d} \text{ [N/m]}$$

$$\vec{F}_1' = \hat{y} \frac{\mu_0 I_1 I_2}{2\pi d} \text{ [N/m]}$$

5.3: Maxwell's Magnetostatic Equations

Recall electrostatic:

Gauss's Law for electricity:

$$\nabla \cdot \vec{D} = \rho_v \quad \longleftrightarrow \quad \oint_{\text{enc}} \vec{D} \cdot d\vec{s} = Q_{\text{enc}}$$

point form integral form

Magnetostatics

The counterpart is:

$$\nabla \cdot \vec{B} = 0 \quad \longleftrightarrow \quad \oint_{\text{enc}} \vec{B} \cdot d\vec{s} = 0$$

Point form integral form

$\rightarrow$ called Gauss's Law for magnetism

note: zero reflects that the magnetic equivalent of electric ρ_v (or Q_{enc}) does not exist

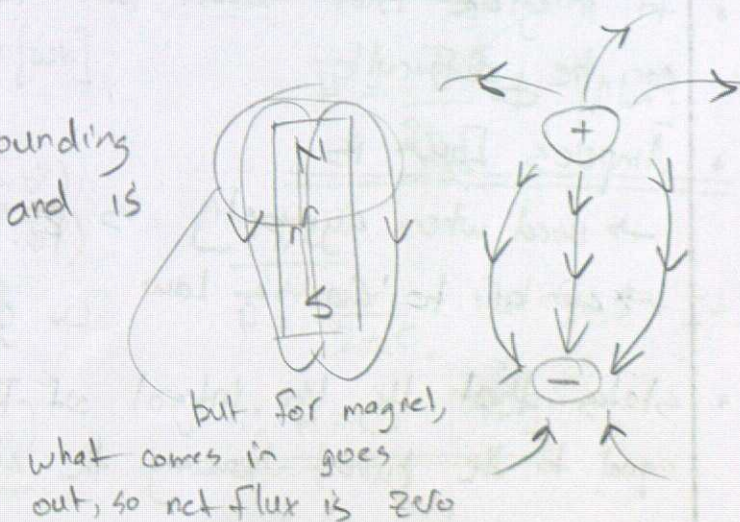
* since no matter how many times a magnet is divided into smaller pieces, still have magnetic dipole

Consider field lines

* $\vec{D}$ thru closed surface surrounding one charge is non-zero and is equal to $\oint \vec{D} \cdot d\vec{s} = Q_{\text{enc}}$

* magnet case

$$\oint_S \vec{B} \cdot d\vec{s} = 0$$



Integration

$$B = \frac{\mu_0 I}{2\pi} \int_0^\infty \frac{R d\ell}{(\ell^2 + R^2)^{3/2}}$$

$$\ell = 0 \Rightarrow \theta = 0$$

$$\ell = \infty \Rightarrow \theta = \pi/2$$

$$B = \frac{\mu_0 I}{2\pi} \int_0^{\pi/2} \frac{R \sec^2 \theta d\theta}{(R^2 \sec^2 \theta)^{3/2}}$$

$$= \frac{\mu_0 I}{2\pi} \frac{R^2}{R^3} \int_0^{\pi/2} \frac{\sec^2 \theta}{\sec^3 \theta} d\theta$$

$$= \frac{\mu_0 I}{2\pi R} \int_0^{\pi/2} \frac{1}{\sec \theta} d\theta = \frac{\mu_0 I}{2\pi R} \int_0^{\pi/2} \cos \theta d\theta$$

$$\Rightarrow B = \frac{\mu_0 I}{2\pi R} [T]$$

5-3.2 Ampere's Law

* to integrate Biot-Savart law to find magnetic field can be difficult

* Ampere's Law is

→ used when symmetry is present

→ similar to Gauss's Law $\Rightarrow \oint \vec{D} \cdot d\vec{A} = Q_{enc}$

* states that the line integral of $\vec{H}$ around a closed path is equal to the current traversing the surface bound by the path

$$\text{Let } \ell = R \tan \theta$$

$$d\ell = R \sec^2 \theta d\theta$$

$$\Rightarrow \ell^2 = R^2 \tan^2 \theta$$

$$\ell^2 + R^2 = R^2 \tan^2 \theta + R^2$$

$$= R^2 (1 + \tan^2 \theta)$$

$$= R^2 \sec^2 \theta$$

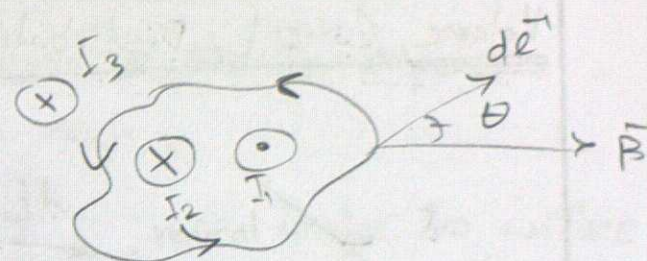
* the closed loop is called Amperian loop

* $d\vec{\ell}$ is along tangent to loop

$$I_{enc} = I_1 - I_2$$

* direction of current is determined by R.H.R.

* contribution of current outside of loop is zero



Ex 1: find magnetic field for coaxial cable everywhere

Apply Ampere's Law

$$\oint \vec{H} \cdot d\vec{\ell} = I_{enc}$$

$$0 < r < a$$

$$H 2\pi r = I_{enc}$$

$$I_{enc} = I \frac{\pi r^2}{\pi a^2}$$

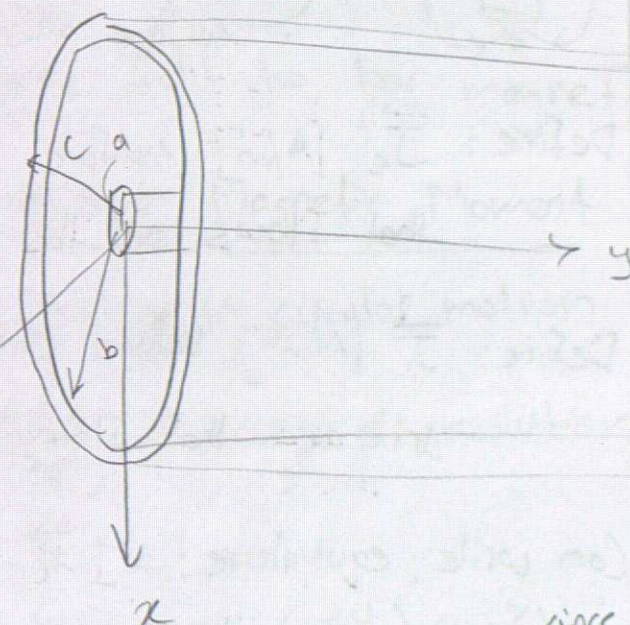
$$= I \frac{r^2}{a^2}$$

$$\therefore \vec{H} = \frac{I}{2\pi a^2} r \hat{\phi} [A/m] \text{ or } [Wb]$$

$$b \leq r \leq c \quad I_{enc} = I - I \frac{\pi(r^2 - b^2)}{\pi(c^2 - b^2)}$$

$$\vec{H} = \frac{I_{enc}}{2\pi r}$$

$$\vec{H} = \frac{I}{2\pi r} \left(1 - \frac{r^2 - b^2}{c^2 - b^2}\right) \hat{\phi} [A/m]$$



Since I_{enc} is I

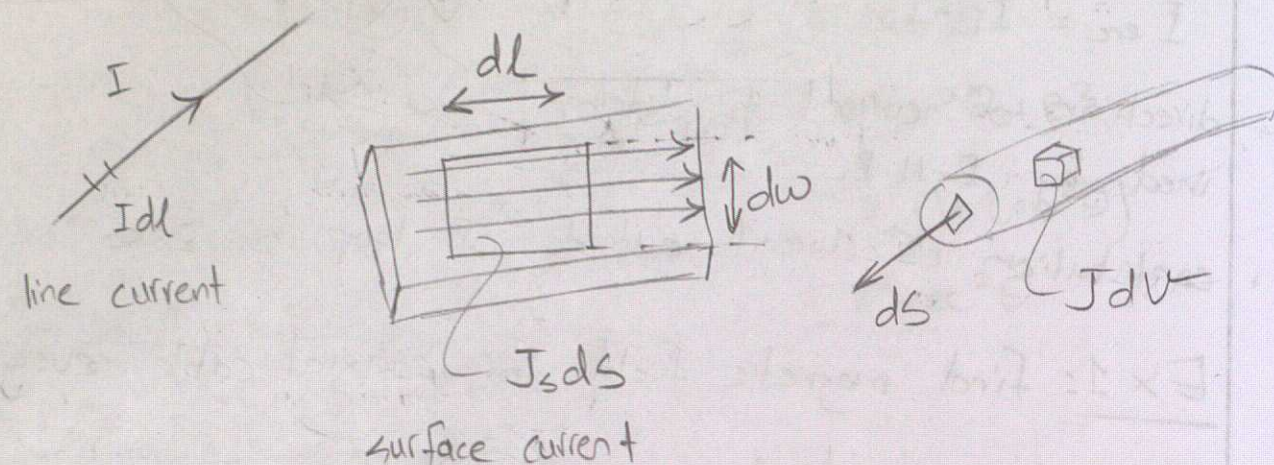
$$\vec{H} = \frac{I}{2\pi r} \hat{\phi} [A/m]$$

$$r > c$$

$$\vec{H} = \frac{I_{enc}}{2\pi r}, \text{ but } I_{enc} = I - I = 0$$

$$\therefore \vec{H} = 0 [A/m]$$

5-2.1: Magnetic Field Due to Surface and Volume Current Distribution



* Define: $\vec{J}_s$ [A/m] surface current density as current that flows on the surface of conductor

* Define: $\vec{J}$ [A/m²] volume current density as current per unit area that flows $\perp$ to surface

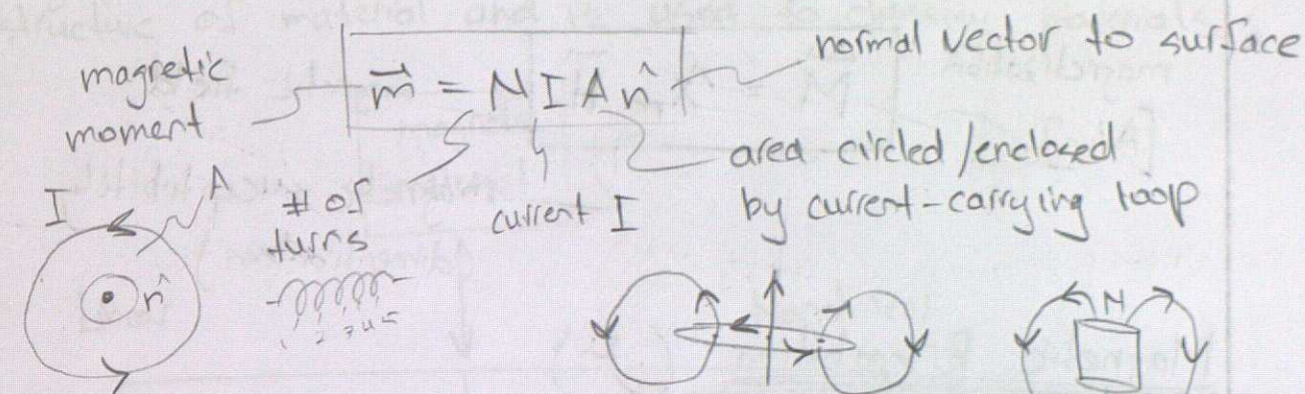
* Can write equivalence: $I d\vec{l} \longleftrightarrow \vec{J}_s d\vec{s} \longleftrightarrow \vec{J} dV$
 $\text{A}\cdot\text{m} \qquad \quad [\frac{\text{A}}{\text{m}}] \cdot [\text{m}^2] \qquad \quad [\frac{\text{A}}{\text{m}^2}] \cdot [\text{m}^3]$
 $\qquad \qquad \qquad = \text{A}\cdot\text{m} \qquad \qquad \qquad = \text{A}\cdot\text{m}$

* Biot-Savart Law can be written:

$$\vec{H} = \int_l \frac{I d\vec{l} \times \hat{r}}{4\pi r^2} \quad \vec{H} = \iint_S \frac{\vec{J}_s d\vec{s} \times \hat{r}}{4\pi r^2} \quad \vec{H} = \iiint_V \frac{\vec{J} dV \times \hat{r}}{4\pi r^2}$$

5-5: Magnetic Properties of Materials

* Recall Magnetic Dipole: analogous to electric dipole and is a current-carrying loop such:



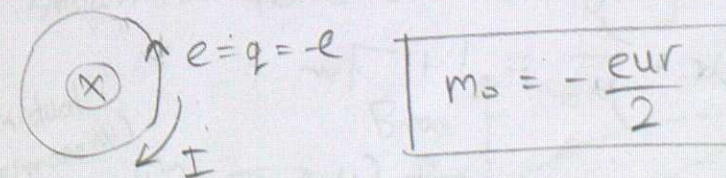
* magnetic dipole similar magnetic field to bar magnet

5-5.1: Electron Orbital and Spin Magnetic Moment

* Consider electron with $q=e$ moving in circular motion with speed $u \Rightarrow T = \frac{2\pi r}{u}$ [seconds] 1 revolution

$$I = \frac{dq}{dt} = \frac{-e}{T} = \frac{-eu}{2\pi r}$$

* orbital magnetic moment: $m_o = IA = \left(\frac{-eu}{2\pi r}\right)(\pi r^2) = -\frac{eur}{2}$



5-5.2 : Magnetic Permeability μ

- * magnetization vector: is a measure of how receptive material is to magnetization and (for some mater.) given by:

$$\text{magnetization } [\text{A/m}] \rightarrow \boxed{\vec{M} = \chi_m \vec{H}} \leftarrow \text{magnetic field}$$

magnetic susceptibility (dimensionless)

Magnetic Permeability (μ)

Recall: $\vec{D} = \epsilon_0 \vec{E} \rightarrow \vec{D} = \epsilon_0 \vec{E} + \vec{P}$

Likewise: $\vec{B} = \mu_0 \vec{H} \rightarrow \vec{B} = \mu_0 \vec{H} + \mu \vec{M}$

$$\Rightarrow \vec{B} = \mu_0 (\vec{H} + \vec{M}) = \mu_0 (\vec{H} + \chi_m \vec{H})$$

$$= \underbrace{\mu_0 (1 + \chi_m)}_{\mu_r} \vec{H}$$

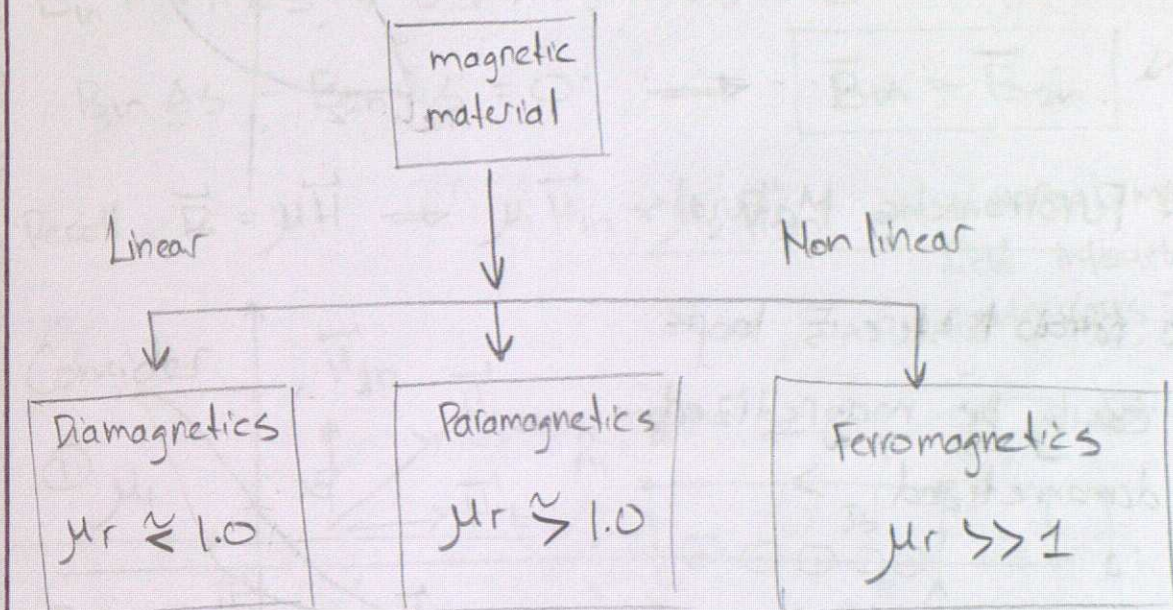
$$\vec{B} = \mu_0 \mu_r \vec{H} = \mu \vec{H}$$

$$\mu_r = \frac{\mu}{\mu_0} = 1 + \chi_m$$

$$\mu_0 = 4\pi \times 10^{-7} [\text{A/m}]$$

Classification of Materials

- * is based on χ_m
- * nature of magnetic behaviour depends on the crystalline structure of material and is used to classify materials

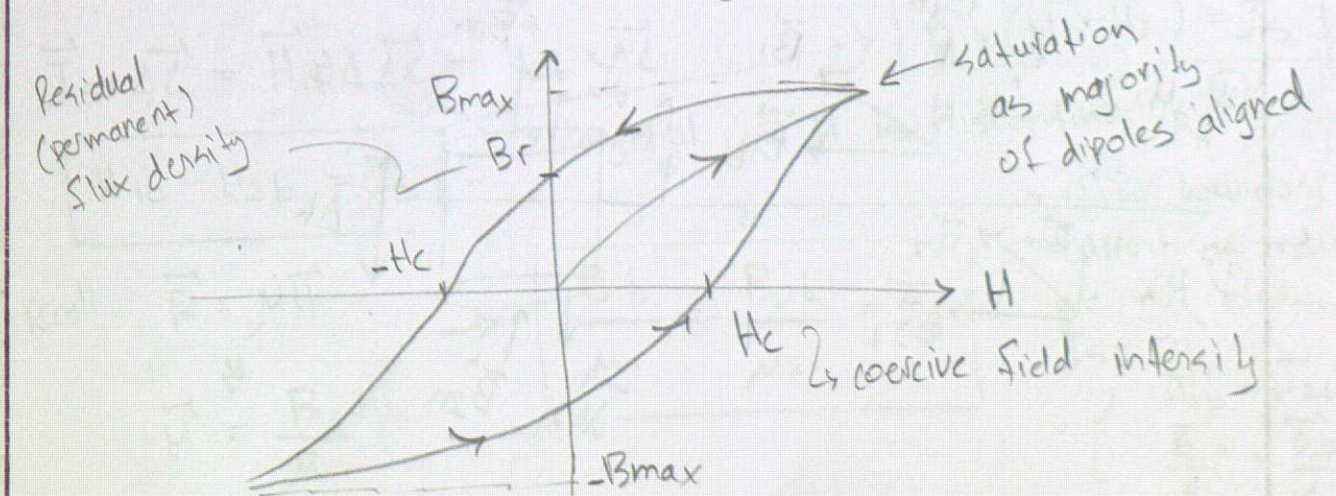


5-5.3 Magnetic Hysteresis of Ferromagnets

- * "hysteresis" means "lag behind" ..

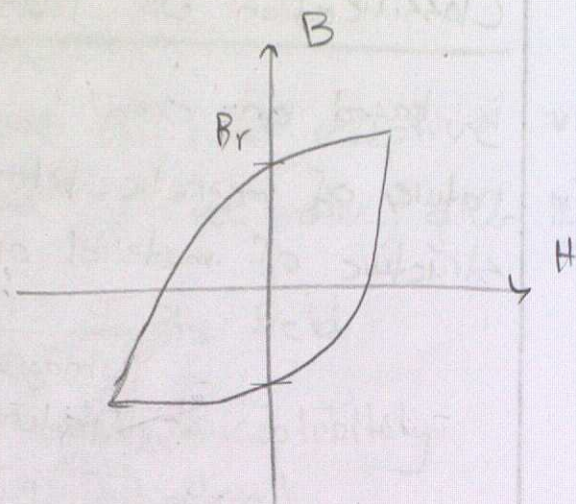
- * eg: iron, nickel, cobalt, alloys

- * is shown in terms of B-H magnetization curve



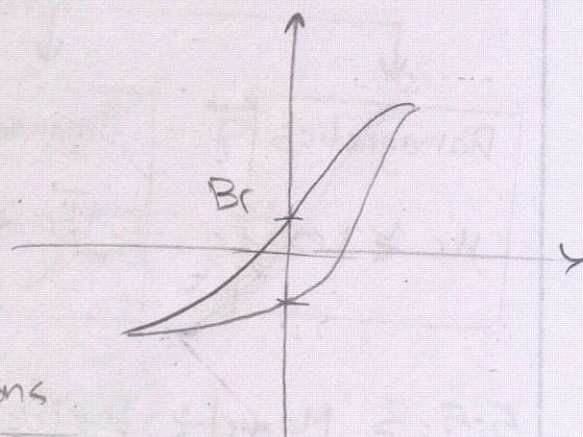
Hard Ferromagnetic Materials

- * have wide hysteresis loops
- * not easily magnetized/demagnetized



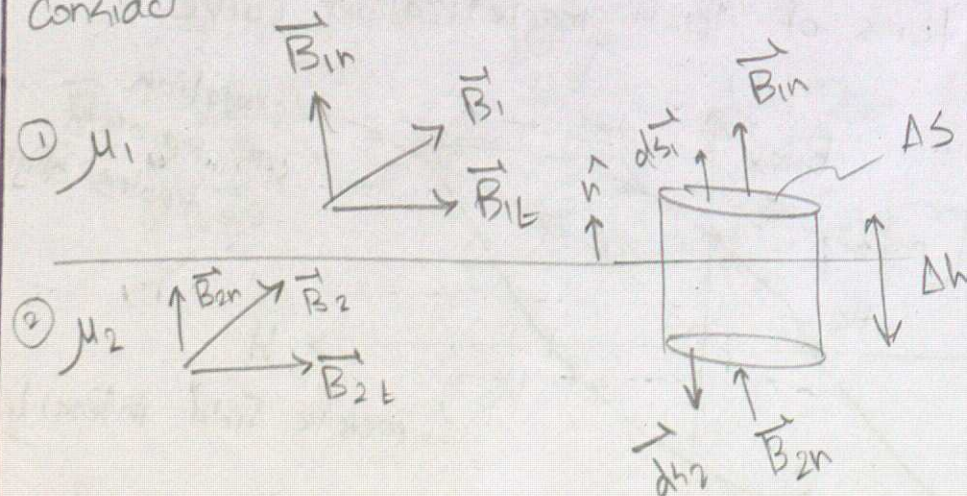
Soft Ferromagnetic Materials

- * have narrow hysteresis loops
- * can easily be magnetized or demagnetized



5-6 Magnetic Boundary Conditions

- * are the conditions $\vec{H}/\vec{B}$ field must satisfy @ boundary b/n 2 different media
- * Consider



- * Apply Gauss Law for magnetism

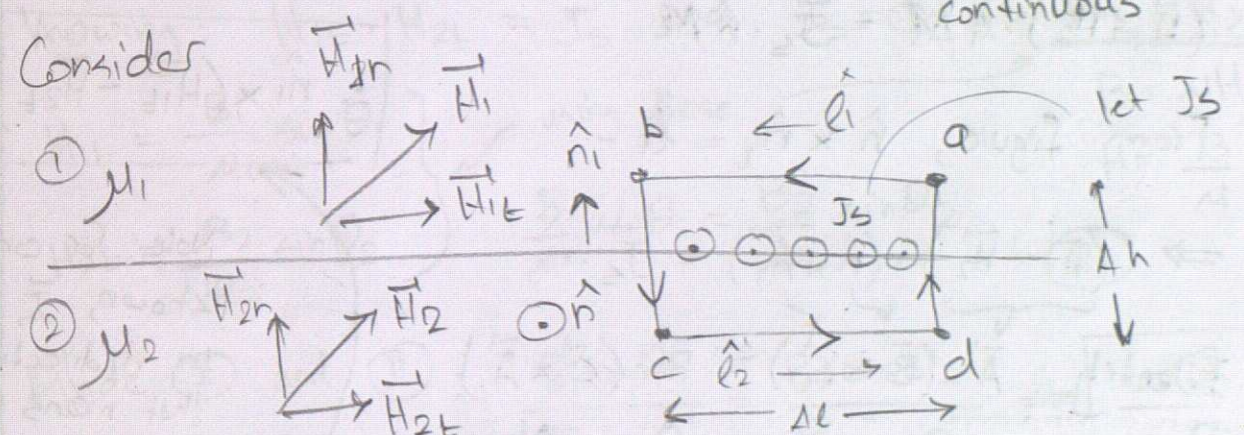
$$\oint_S \vec{B} \cdot d\vec{S} = 0 \text{ and let } \Delta h \rightarrow 0 \text{ (side contribution goes to zero)}$$

from top & bottom remain

$$B_{1n} \hat{n} \cdot \hat{n} \Delta S + B_{2n} \hat{n} \cdot (-\hat{n}) \Delta S = 0$$

$$B_{1n} \Delta S - B_{2n} \Delta S = 0 \Rightarrow \boxed{\vec{B}_{1n} = \vec{B}_{2n}} \quad \leftarrow \begin{array}{l} \therefore \text{normal } B \\ \text{is cont @} \\ \text{boundary} \end{array}$$

- * Recall $\vec{B} = \mu \vec{H} \Rightarrow \mu_1 \vec{H}_{1n} = \mu_2 \vec{H}_{2n} \Rightarrow \therefore$ normal magnetic field intensity is not continuous



- * Apply Ampere's Law: $\oint \vec{H} \cdot d\vec{l} = I_{enc}$
- * and $I = \vec{J}_s \cdot \Delta \vec{l}$

- * Let J_s be surface current also $\Delta h \rightarrow 0$

$$\vec{J}_s \cdot \Delta \vec{l} = \vec{H}_{1t} \cdot \Delta \vec{l} - \vec{H}_{2t} \cdot \Delta \vec{l} \Rightarrow \boxed{\hat{n}_1 \times (\vec{H}_{1t} - \vec{H}_{2t}) = \vec{J}_s}$$

$$\boxed{H_{1t} - H_{2t} = J_s} \rightarrow \text{tangential of } H \text{ is discontinuous}$$

Recall $\vec{B} = \mu \vec{H}$

$$\vec{H} = \frac{\vec{B}}{\mu}$$

$$\rightarrow \boxed{\frac{B_{1t}}{\mu_1} - \frac{B_{2t}}{\mu_2} = J_s}$$

if no boundary current or media are not conductors, $J_s = 0$

$$\begin{cases} \vec{H}_{1t} = \vec{H}_{2t} \\ \frac{\vec{B}_{1t}}{\mu_1} = \frac{\vec{B}_{2t}}{\mu_2} \end{cases}$$

Another Method

* Apply Ampere's law $\oint \vec{H} \cdot d\vec{l} = I_{enc}$ and let $\Delta l \rightarrow 0$

$$\oint \vec{H} \cdot d\vec{l} = \int_a^b \vec{H}_1 \cdot \hat{l}_1 dl + \int_c^d \vec{H}_2 \cdot \hat{l}_2 dl$$

* Can write $\vec{H}_1 \cdot \hat{l}_1 \Delta l + \vec{H}_2 \cdot \hat{l}_2 \Delta l = I$ for Δl
 * Also, $\hat{l}_2 = -\hat{l}_1 \Rightarrow (\vec{H}_1 - \vec{H}_2) \cdot \hat{l}_1 \Delta l = I$ $I = \vec{J}_s \cdot \vec{A} \hat{l}$
 $= \vec{J}_s \cdot \hat{n} \Delta l$

$$(\vec{H}_1 - \vec{H}_2) \cdot \hat{l}_1 \Delta l = \vec{J}_s \cdot \hat{n} \Delta l$$

* From figure, $\hat{n} \times \hat{n}_1 = \hat{l}_1$

$$\Rightarrow (\vec{H}_1 - \vec{H}_2) \cdot (\hat{n} \times \hat{n}_1) = \vec{J}_s \cdot \hat{n}$$

* Identity: $\vec{A} \cdot (\vec{B} \times \vec{C}) = \vec{B} \cdot (\vec{C} \times \vec{A})$

$$\Rightarrow \hat{n} \cdot (\hat{n}_1 \times (\vec{H}_1 - \vec{H}_2)) = \vec{J}_s \cdot \hat{n}$$

* Identity: $\vec{v} \cdot \vec{w} = \vec{w} \cdot \vec{v}$

$$\Rightarrow (\hat{n}_1 \times (\vec{H}_1 - \vec{H}_2)) \cdot \hat{n} = \vec{J}_s \cdot \hat{n}$$

$$\hat{n}_1 \times (\vec{H}_1 - \vec{H}_2) = \vec{J}_s \quad \leftarrow \text{but } \begin{matrix} \vec{H}_1 = \vec{H}_{1n} + \vec{H}_{1t} \\ \vec{H}_2 = \vec{H}_{2n} + \vec{H}_{2t} \end{matrix}$$

$$\Rightarrow \hat{n}_1 \times (\vec{H}_{1n} + \vec{H}_{1t} - (\vec{H}_{2n} + \vec{H}_{2t})) = \vec{J}_s$$

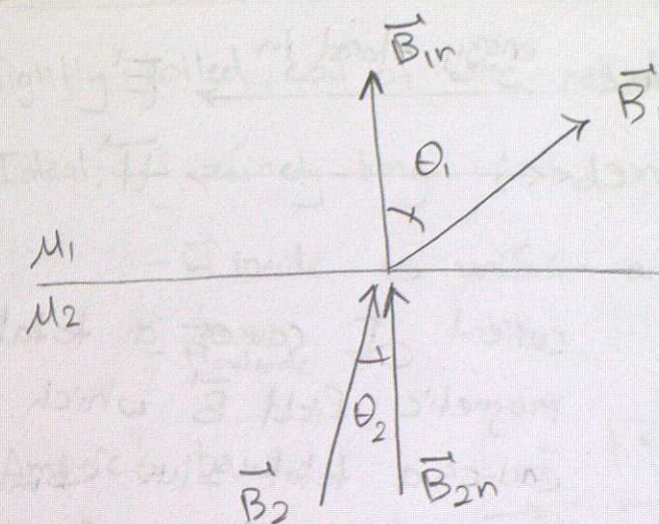
note $\hat{n}_1 \times \vec{H}_{1n} = 0$ and $\hat{n}_1 \times \vec{H}_{2n} = 0$

$$\therefore \hat{n}_1 \times (\vec{H}_{1t} - \vec{H}_{2t}) = \vec{J}_s$$

Note: for config shown, $\vec{J}_s$ is in $\hat{n}$ direction, that means $H_{1t} < H_{2t}$

if $H_{1t} < H_{2t} \Rightarrow \hat{n}$
 $H_{1t} > H_{2t} \Rightarrow -\hat{n}$
 $H_{1t} = H_{2t} \Rightarrow \vec{J}_s = 0$

Ex: Find relation b/n μ_1 and μ_2 given figure:



* We know $\vec{B}_{1n} = \vec{B}_{2n}$

can write:

$$\begin{cases} B_{1n} = B_1 \cos \theta_1 \\ B_{2n} = B_2 \cos \theta_2 \end{cases}$$

$$\therefore B_1 \cos \theta_1 = B_2 \cos \theta_2 \quad \text{--- (I)}$$

* Knowing: $H_{1t} - H_{2t} = J_s$ and $J_s = 0 \Rightarrow H_{1t} = H_{2t}$

$$H_{1t} = \frac{B_1}{\mu_1} \sin \theta_1$$

$$H_{2t} = \frac{B_2}{\mu_2} \sin \theta_2$$

using these

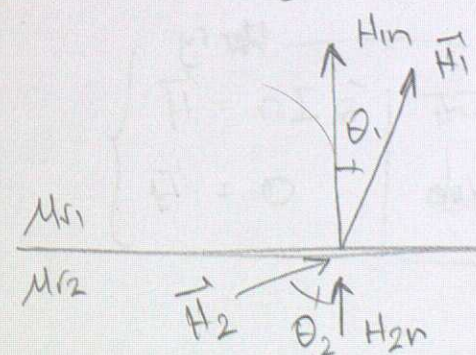
$$\frac{B_1}{\mu_1} \sin \theta_1 = \frac{B_2}{\mu_2} \sin \theta_2 \quad \text{--- (II)}$$

$$B = \mu H$$

$$H = \frac{B}{\mu}$$

Divide (I) and (II): $\frac{B_1 \cos \theta_1}{\frac{B_1}{\mu_1} \sin \theta_1} = \frac{B_2 \cos \theta_2}{\frac{B_2}{\mu_2} \sin \theta_2} \Rightarrow \boxed{\frac{\tan \theta_1}{\tan \theta_2} = \frac{\mu_1}{\mu_2}}$

Ex: For magnetic field shown, how does μ_1 relate to μ_2



$$B_{1n} = B_{2n} \quad B = \mu H$$

$$\mu_1 H_{1n} = \mu_2 H_{2n}$$

$$H_{1n} = \frac{\mu_2}{\mu_1} H_{2n}$$

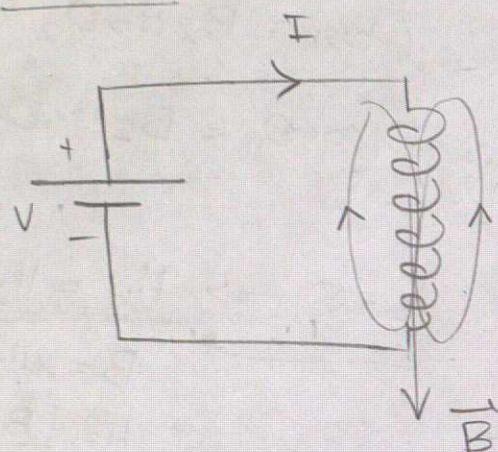
From figure drawn to scale $H_{1n} > H_{2n}$



5-7: Inductance

Capacitor $\xrightarrow{\text{has}}$ capacitance $\xrightarrow{\text{energy stored in}}$ E
 Inductor $\xrightarrow{\text{has}}$ inductance $\xrightarrow{\text{energy stored in}}$ H

* Consider



current I causes a total magnetic field $\vec{B}$ which causes a total flux Φ_m through each turn of the coil given by:

$$\Phi_B = \int_S \vec{B} \cdot d\vec{S}$$

* For N identical and tightly wrapped coils, can define magnetic flux linkage as

$$\Lambda = N \Phi_B \quad [\text{Wb}]$$

capital lambda

* then inductance is defined as the ratio of Λ to current $[I]$

$$L = \frac{\Lambda}{I} = \frac{N\Phi}{I} \quad [H] \text{ or } \left[\frac{\text{Wb}}{\text{A}}\right]$$

5-7.1 Magnetic Field in a Solenoid

* Tightly coiled coil of wire called a "solenoid"

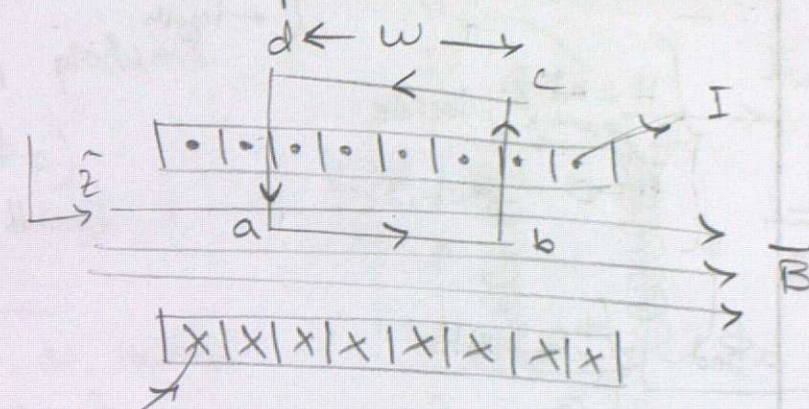
* Ideal: - infinitely long $l \gg d$

- $\vec{H}$ inside is uniform and parallel to solenoid axis

- $\vec{H}_{\text{outside}} = 0$

* Ampere's Law:

$$\oint \vec{H} \cdot d\vec{l} = I_{\text{enc}}$$



$$\oint \vec{H} \cdot d\vec{l} = \int_a^b \vec{H} \cdot d\vec{l} + \int_b^c \vec{H} \cdot d\vec{l} + \int_c^d \vec{H} \cdot d\vec{l} + \int_d^a \vec{H} \cdot d\vec{l}$$

$\theta = 0 \quad \theta = 90^\circ \quad \text{outside} \quad \theta = 90^\circ$
 $\therefore \neq 0 \quad \therefore = 0 \quad \therefore = 0 \quad \therefore = 0$

$$\oint \vec{H} \cdot d\vec{l} = Hw + 0 + 0 + 0 = I_{\text{enc}}$$

$$Hw = In \quad \rightarrow \text{\# of turns per length}$$

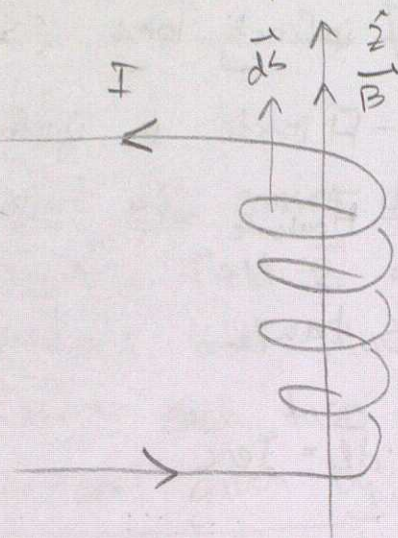
$$\begin{cases} \vec{H} = nI \hat{z} & \text{inside} \\ \vec{H} = 0 & \text{outside} \end{cases} \quad \vec{B} = \mu \vec{H}$$

5-7.2: Self Inductance of a Solenoid

- Self Inductance: is when the inductance is produced by the inductor itself

Consider: $n = \frac{N}{l}$
total # of turns
length

$$\begin{cases} H = nI\hat{z} & \text{inside} \\ \vec{H} = 0 & \text{outside} \end{cases}$$



and $\begin{cases} B = \mu H \\ \Phi_m = \int_S \vec{B} \cdot d\vec{S} \end{cases} \Rightarrow \Phi = \int_S \hat{z} \left(\frac{N}{l} \mu \right) \cdot \hat{z} dS$

$$\Rightarrow \Phi_m = \mu \frac{N}{l} I S \quad \rightarrow S \text{ is cross-sectional area}$$

- Can write in terms of magnetic flux linkage

$$\Lambda = N \Phi_m = N \left(\mu \frac{N}{l} I S \right) = \frac{\mu N^2}{l} I S \quad [\text{wb}]$$

$$\text{Self inductance } L = \frac{\Lambda}{I} = \frac{\mu N^2 S}{l} = \frac{\mu N^2 \epsilon_0 \epsilon_r d}{l}$$

$$\boxed{\therefore L = \frac{\mu N^2 S}{l} \quad [\text{H}]}$$

$$\longleftrightarrow C = \frac{\epsilon A}{d} \rightarrow S \quad [\text{F}]$$

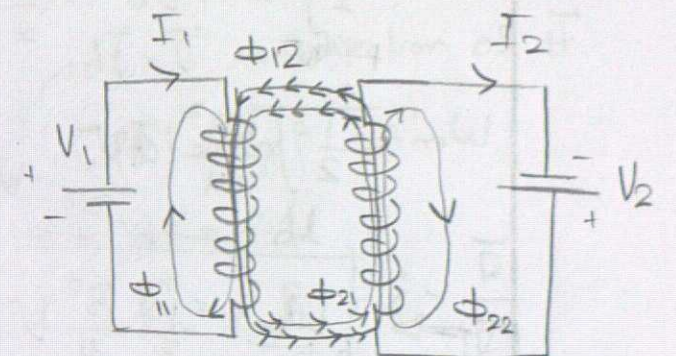
5-7.4: Mutual Inductance

- magnetic coupling b/n two conducting structures is called / or described as mutual inductance

- consider a pair of coils with currents I_1 and I_2

- then $\Phi_{11}, \Phi_{12}, \Phi_{22}, \Phi_{21}$ produced

- some of the flux (Φ_{12}) produced by I_1 links through coil 2



- This flux is common or mutual to both coils

$$\Rightarrow M_{12} = \frac{\Lambda_{12}}{I_1} = \frac{N_2 \Phi_{12}}{I_1} = \frac{N_2}{I_1} \int \vec{B}_1 \cdot d\vec{S}_2$$

Note self inductance is $L_1 = \frac{\Lambda_{11}}{I_1} = \frac{N_1 \Phi_{11}}{I_1}$ Φ_1

Similarly $M_{21} = \frac{\Lambda_{21}}{I_2} = \frac{N_1 \Phi_{21}}{I_2}$

$$L_2 = \frac{\Lambda_{22}}{I_2} = \frac{N_2 \Phi_{22}}{I_2}$$

5-8: Magnetic Energy in Inductor

Recall Cap: $W_e = \frac{1}{2} CV^2$

likewise L: $W_m = \frac{1}{2} LI^2$

$$W_m = \frac{1}{2} \int_V \vec{B} \cdot \vec{H} dV = \frac{1}{2} \int_V \mu H^2 dV \quad \text{since } B = \mu H$$

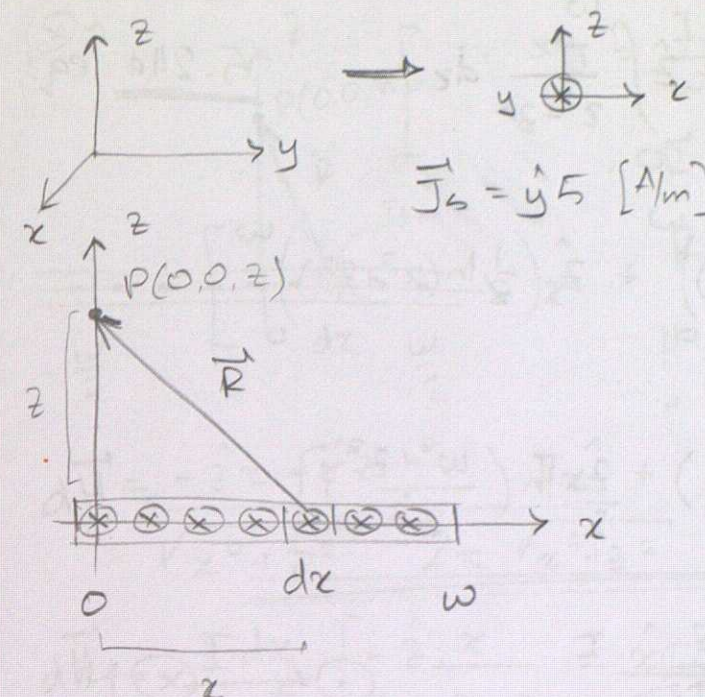
$$W_m = \frac{1}{2} \int_V \frac{B^2}{\mu} dV \quad V: \text{volume}$$

$$\Rightarrow W_m = \frac{1}{2} \frac{B^2}{\mu} V, \quad W_m = \frac{1}{2} \mu H^2 V \quad [J]$$

Week 10: Tutorial 8

Mar 10, 2025

5.10



rotate so $\hat{y}$ into page

$$\vec{H} = \frac{I}{2\pi d} \hat{\phi}$$

Biot-Savart: $d\vec{l} \times \vec{R} = dl(\vec{a} \times \vec{R})$

$$\vec{R} = -x\hat{x} + z\hat{z}$$

$d\vec{l} \times \vec{R}$ ← direction of $\vec{H}$

$$|\vec{R}| = \sqrt{x^2 + z^2}$$

$$d\vec{l} = \hat{a} dl$$

$$\vec{R} = \hat{r} R \quad \hat{r} = \frac{\vec{R}}{|\vec{R}|}$$

$$d\vec{l} \times \vec{R} = dl R (\vec{a} \times \hat{r}) = dl R (\hat{y} \times \frac{-x\hat{x} + z\hat{z}}{\sqrt{x^2 + z^2}})$$

$$\hat{\phi} = \hat{y} \times \frac{-x\hat{x} + z\hat{z}}{\sqrt{x^2 + z^2}} = \frac{\hat{z}x + \hat{x}z}{\sqrt{x^2 + z^2}}$$

$$\therefore d\vec{H} = \frac{\hat{z}x + \hat{x}z}{\sqrt{x^2 + z^2}} \cdot \frac{I}{2\pi R}$$

R found

$$d\vec{H} = \frac{\hat{z}x + \hat{x}z}{\sqrt{x^2 + z^2}} \cdot \frac{I}{2\pi \sqrt{x^2 + z^2}} = \frac{I}{2\pi} \left[\hat{z} \frac{x}{x^2 + z^2} + \hat{x} \frac{z}{x^2 + z^2} \right]$$

and $I = |J_s| dx = 5 dx$

$$d\vec{H} = \frac{5 dx}{2\pi} \left[\hat{z} \frac{x}{x^2 + z^2} + \hat{x} \frac{z}{x^2 + z^2} \right]$$

$$\vec{H} = \int_0^w \frac{5 dx}{2\pi} \left[\hat{z} \frac{x}{x^2 + z^2} + \hat{x} \frac{z}{x^2 + z^2} \right]$$

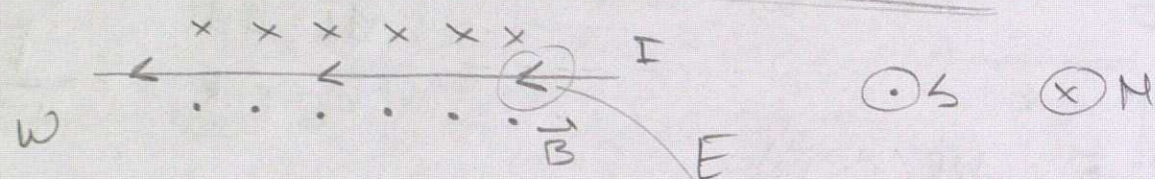
★ Why $\vec{H}$ vs $\vec{B}$?
What about
Biot Savart

$$\vec{H} = \frac{|\vec{J}_s|}{2\pi} \left[\hat{x} \int_0^w \frac{z}{x^2+z^2} dx + \hat{z} \int_0^w \frac{x}{x^2+z^2} dz \right] \quad \underline{5.24a \text{ eq:}}$$

$$= \frac{|\vec{J}_s|}{2\pi} \left[\hat{x} \left(\frac{1}{2} \arctan\left(\frac{x}{z}\right) \right)_0^w + \hat{z} \left(\frac{1}{2} \ln(x^2+z^2) \right)_0^w \right]$$

$$= \frac{|\vec{J}_s|}{2\pi} \left[\frac{\hat{x}}{2} \arctan\left(\frac{w}{z}\right) + \frac{\hat{z}}{2} \ln\left(\frac{w^2+z^2}{z^2}\right) \right]$$

5.13



$$B = (20-15) \mu T$$

$$B = \frac{\mu_0 I}{2\pi d}$$

$$\therefore I = \frac{2\pi dB}{\mu_0} = \frac{2\pi(8)(5)}{\mu_0}$$

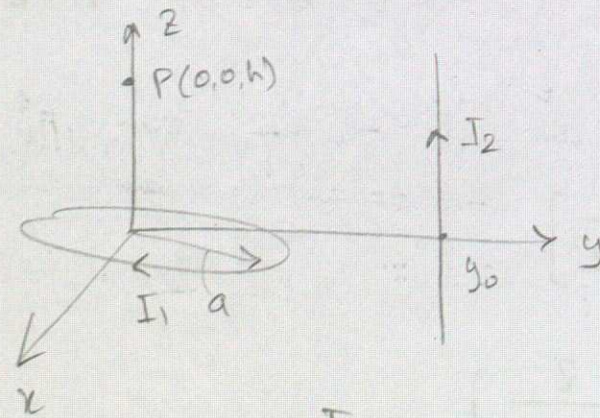
= 200 A current

direction not relevant

5.15

a)

eq. 5.34



$$\vec{H}_2 = \hat{x} \frac{I_2}{2\pi y_0}$$

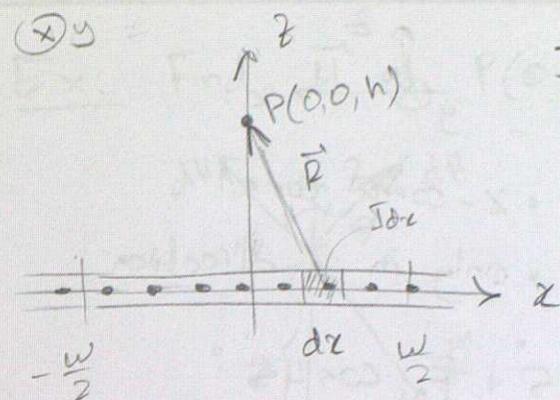
$$\therefore \vec{H}(0,0,h) = \vec{H}_1 + \vec{H}_2$$

$$\underline{5.34} \quad \vec{H} = \hat{z} \frac{I a^2}{2(a^2+z^2)^{3/2}}$$

$$\therefore \vec{H}_1 = -\hat{z} \frac{I_1 a^2}{2(a^2+h^2)^{3/2}}$$

5.18

a)



$$J = \frac{I}{w} \Rightarrow I_x = J dx = \frac{I}{w} dx$$

$$\vec{R} = -x\hat{x} + z\hat{z}$$

$$R = \sqrt{x^2+z^2}$$

$$H = \frac{I}{2\pi R}$$

$$\hat{a} \times \hat{R} = -\hat{y} \times \frac{\vec{R}}{|\vec{R}|}$$

$$= -\hat{y} \times \frac{-x\hat{x} + z\hat{z}}{\sqrt{x^2+z^2}}$$

$$= \frac{-\hat{z}x - \hat{x}z}{\sqrt{x^2+z^2}}$$

$$d\vec{H} = \frac{-\hat{z}x - \hat{x}z}{\sqrt{x^2+z^2}} \cdot \frac{I_x}{2\pi \sqrt{x^2+z^2}}$$

$$d\vec{H} = \frac{I dx}{2\pi w} \left[-\frac{\hat{z}x}{x^2+z^2} - \frac{\hat{x}z}{z^2+z^2} \right]$$

$$\vec{H} = \frac{-I}{2\pi w} \left[\hat{z} \int_{-w/2}^{w/2} \frac{x}{x^2+z^2} dx + \hat{x} \int_{-w/2}^{w/2} \frac{1}{x^2+z^2} dx \right]$$

$$= \frac{-I}{2\pi w} \left[\hat{z} z \left(\frac{1}{2} \arctan\left(\frac{x}{z}\right) \right)_{-w/2}^{w/2} + \hat{x} \frac{1}{2} \ln(x^2+z^2)_{-w/2}^{w/2} \right]$$

$$= \frac{-I}{2\pi w} \left[\hat{z} \left(\arctan\frac{w}{2z} + \arctan\frac{w}{2z} \right) + \hat{x} \left(\dots \right) \right]$$

$$\vec{H} = -\hat{z} \frac{I}{\pi w} \arctan\left(\frac{w}{2z}\right) \xrightarrow{\text{plus } z=h} \vec{H} = -\hat{z} \frac{I}{\pi w} \arctan\left(\frac{w}{2h}\right)$$

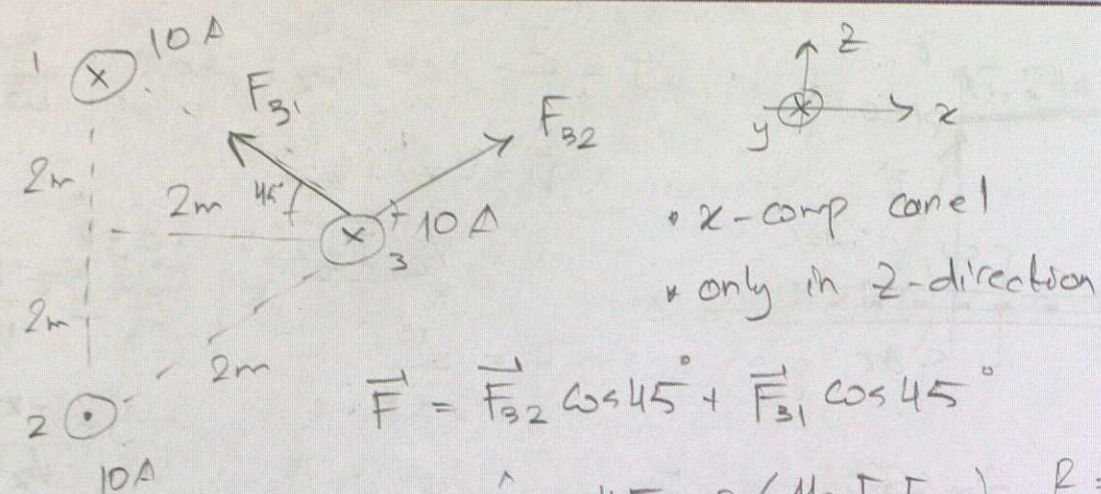
b)

$$\vec{B} = -\hat{z} \frac{\mu_0 I}{\pi w} \arctan\left(\frac{w}{2h}\right), \quad \vec{F} = I \vec{l} \times \vec{B}, \quad \frac{d\vec{F}}{dl} \Rightarrow d\vec{F} = I d\vec{l} \times \vec{B}$$

$$d\vec{l} = -\hat{y} dl, \quad d\vec{F} = I dl (-\hat{y}) \times \vec{B}$$

$$\frac{d\vec{F}}{dl} = -I (\hat{y} \times \vec{B}) = -I \left[\hat{y} \times -\hat{z} \frac{\mu_0 I}{\pi w} \arctan\left(\frac{w}{2h}\right) \right] = -\hat{z} \frac{\mu_0 I^2}{\pi w} \arctan\left(\frac{w}{2h}\right)$$

5.19:



* x-comp cancel
* only in z-direction

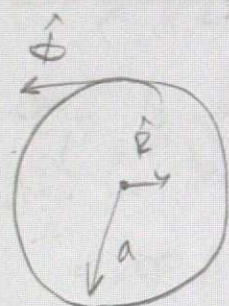
$$\vec{F} = \vec{F}_{32} \cos 45^\circ + \vec{F}_{31} \cos 45^\circ$$

$$= \hat{z} \cos 45^\circ \times 2 \left(\frac{\mu_0 I I_3}{2\pi R} \right), \quad R = R_1 = R_2, \quad I = I_1 = I_2 = 10$$

$$\vec{F} = \hat{z} \cos 45^\circ \left(\frac{\mu_0 I^2}{2\pi R} + \frac{\mu_0 I^2}{2\pi R} \right)$$

$$= \frac{\hat{z} \cos 45^\circ \mu_0 I^2}{\pi R} = \underline{\underline{\hat{z} (10)^{-5} \text{ [N/m]}}}$$

5.25



$$\oint \vec{H} \cdot d\vec{l} = I_{enc}$$

$$d\vec{l} = a d\phi \hat{\phi}$$

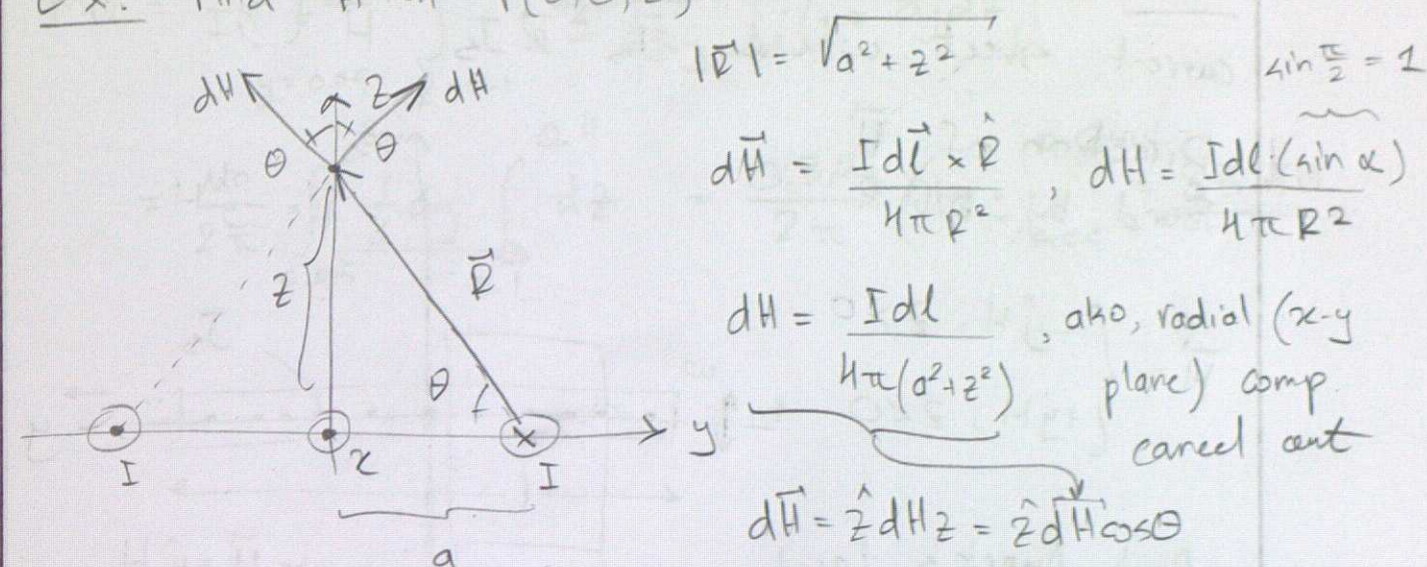
$$I_{enc} = \int_0^{2\pi} \hat{\phi} \cdot \frac{2}{r} [1 - (4r+1)e^{-4r}] \cdot \hat{\phi} a d\phi$$

$$= \frac{4\pi a}{r} [1 - (4r+1)e^{-4r}] \quad \text{for } r = 0.05$$

$$I = 4\pi (1 - (4 \times 0.05 + 1)e^{-4(0.05)}) = 0.22A$$

Week 9: Lecture 1

Mar 11, 2025

Ex: Find $\vec{H}$ at $P(0,0,z)$ 

$$|\vec{R}| = \sqrt{a^2 + z^2}$$

$$\sin \frac{\pi}{2} = 1$$

$$d\vec{H} = \frac{I d\vec{l} \times \hat{R}}{4\pi R^2}, \quad dH = \frac{I dl (\sin \alpha)}{4\pi R^2}$$

$$dH = \frac{I dl}{4\pi (a^2 + z^2)}, \quad \text{also, radial (x-y plane) comp. cancel out}$$

$$d\vec{H} = \hat{z} dH_z = \hat{z} dH \cos \theta$$

$$d\vec{H} = \hat{z} \frac{I \cos \theta}{4\pi (a^2 + z^2)} dl \leftarrow dl = a d\phi$$

$$\vec{H} = \hat{z} \int \frac{I \cos \theta}{4\pi (a^2 + z^2)} dl = \hat{z} \frac{I \cos \theta}{4\pi (a^2 + z^2)} \int_0^{2\pi} a d\phi$$

$$= \hat{z} \frac{I a}{2(a^2 + z^2)} \cos \theta, \quad \text{but } \cos \theta = \frac{a}{\sqrt{a^2 + z^2}} = \frac{a}{R}$$

$$= \hat{z} \frac{I a^2}{2(a^2 + z^2)^{3/2}} \text{ [A/m] @ } P(0,0,z)$$

$$\text{@ } (0,0,0): \vec{H} = \hat{z} \frac{I}{2a} \text{ [A/m]}$$

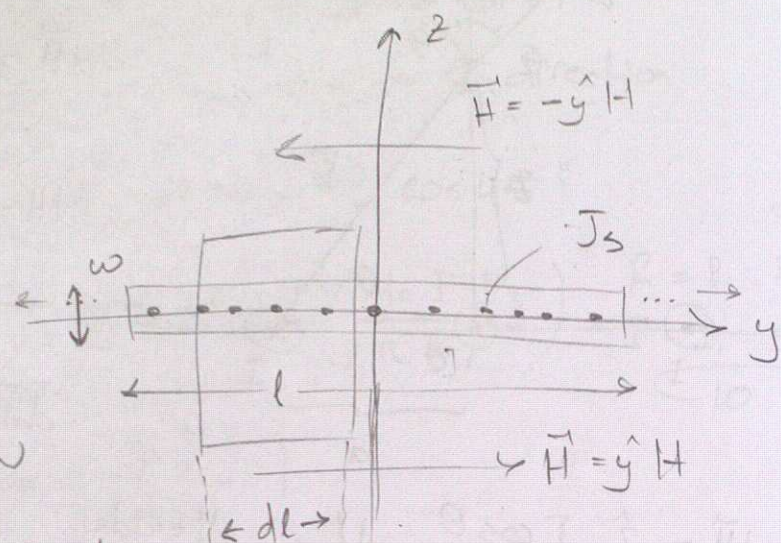
@ $z^2 \gg a^2$ (ie very far)

$$\vec{H} = \hat{z} \frac{I a^2}{2|z|^3} \text{ [A/m]}$$

Ex: Find magnetic field of infinite current sheet where $\vec{J}_s = \hat{x} J_s$, $\vec{H} = ?$

Direction of $\vec{H}$
found by R.H.R

$$\vec{H} = \begin{cases} -\hat{y} H, & z > 0 \\ +\hat{y} H, & z < 0 \end{cases}$$



Apply Amper's Law

$$\oint \vec{H} \cdot d\vec{l} = I_{enc} = J_s l$$

$$H(2l) = J_s l \Rightarrow \vec{H} = \begin{cases} -\hat{y} \frac{J_s}{2}, & z > 0 \\ +\hat{y} \frac{J_s}{2}, & z < 0 \end{cases}$$

Ex: Find mutual inductance b/n wire & loop

Let ① be wire
② be loop

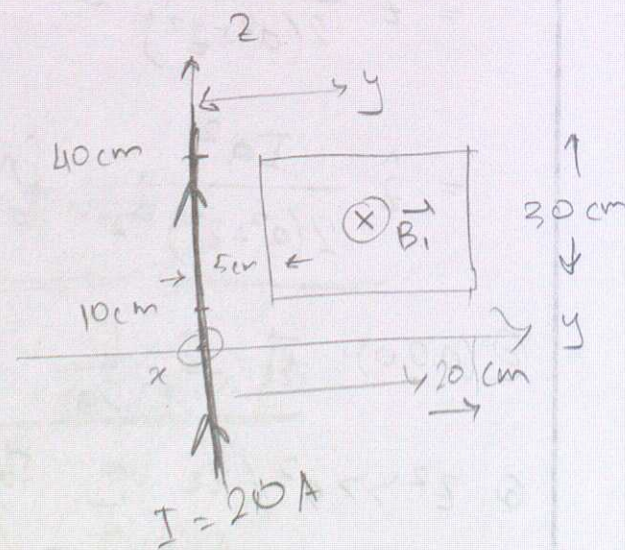
$$M_{12} = \frac{N_2}{I_1} \int_{S_2} \vec{B}_1 \cdot d\vec{S}_2$$

$$\vec{B}_1 = -\hat{x} \frac{\mu_0 I_1}{2\pi y}$$

$$d\vec{S}_2 = -\hat{x} dy dz$$

$$N_2 = 1$$

$$I_1 = I = 20A$$



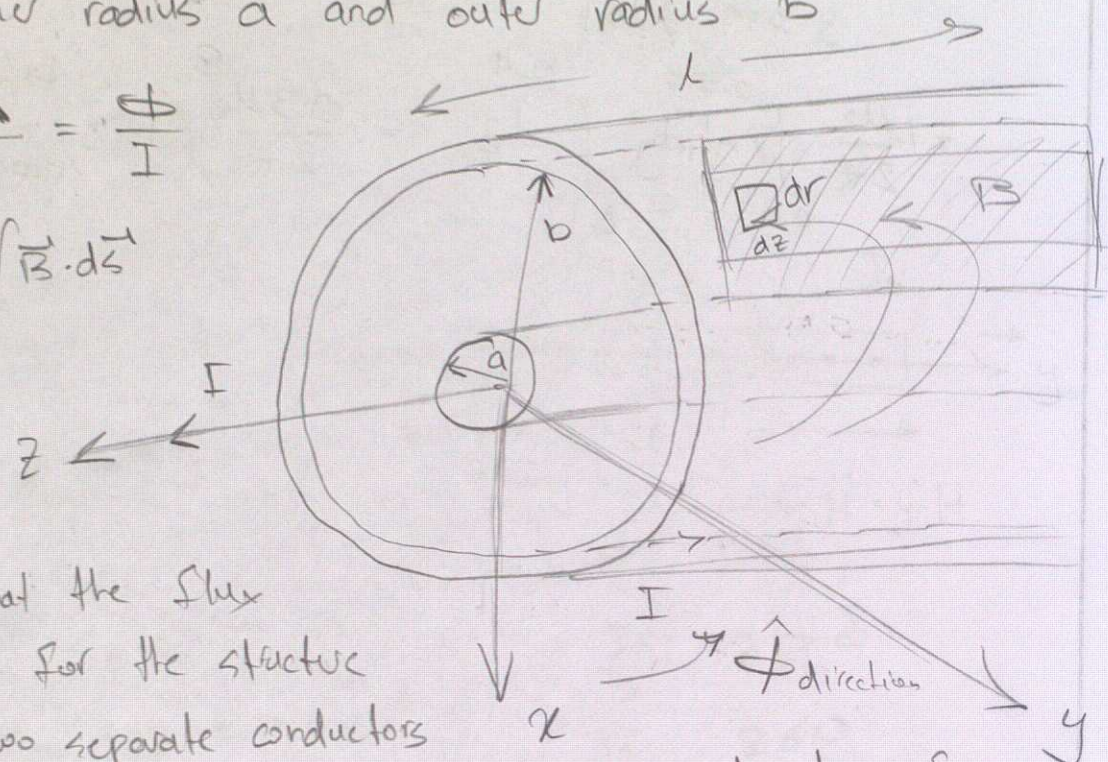
$$M_{12} = \frac{1}{I_1} \int_{y=0.05}^{0.20} \int_{z=0.1}^{0.4} \left(-\hat{x} \frac{\mu_0 I_1}{2\pi y} \right) \cdot (-\hat{x} dy dz)$$

$$= \frac{\mu_0}{2\pi} \int_{0.05}^{0.2} \frac{1}{y} dy \int_{0.1}^{0.4} dz = \frac{0.3\mu_0}{2\pi} (\ln y)_{0.05}^{0.2} = \underline{83 \text{ nH}}$$

Ex: Determine self-inductance of a coaxial cable of inner radius a and outer radius b

$$L = \frac{\Lambda}{I} = \frac{\Phi}{I}$$

$$\Phi = \int \vec{B} \cdot d\vec{s}$$



Note that the flux linkage for the structure with two separate conductors relates to the flux Φ_m through a closed surface between 2 conductors

① Apply Ampere's Law

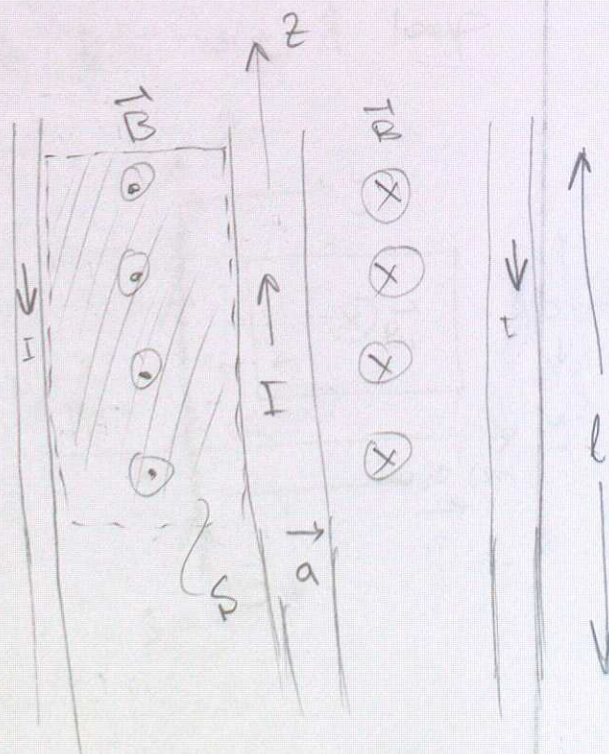
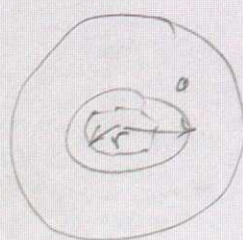
$$\oint \vec{H} \cdot d\vec{l} = I_{enc}$$

For $0 \leq r \leq a$:

$$I_{enc} = I \frac{\pi r^2}{\pi a^2} = I \frac{r^2}{a^2}$$

$$\vec{H} = \frac{I r^2}{a^2} \frac{1}{2\pi r} = \frac{I}{2\pi a^2} r \hat{\phi}$$

$$\therefore \vec{B}_1 = \frac{\mu I}{2\pi a^2} r \hat{\phi} [T]$$



$$d\Phi_1 = B_1 ds = B_1 dr dz$$

$$= \frac{\mu I}{2\pi a^2} r dr dz$$

$$d\Lambda_1 = d\Phi_1 \frac{I_{enc}}{I}$$

$$= d\Phi_1 \frac{r^2}{\pi a^2}$$

$$= \frac{\mu I}{2\pi a^2} r dr dz \frac{r^2}{a^2}$$

$$\Lambda_1 = \int_{r=0}^a \int_{z=0}^l \frac{\mu I}{2\pi a^4} r^3 dr dz = \frac{\mu I}{2\pi a^4} \left[\frac{1}{4} a^4 l \right] = \frac{\mu I l}{8\pi} [wb]$$

$$L_{in} = \frac{\Lambda_1}{I} = \frac{\mu l}{8\pi} [H]$$

$$* a \leq r \leq b: \oint \vec{H} \cdot d\vec{l} = I_{enc} \Rightarrow H(2\pi r) = I \Rightarrow \vec{H} = \frac{I}{2\pi r} \hat{\phi} [A/m]$$

$$\therefore \vec{B}_2 = \frac{\mu I}{2\pi r} \hat{\phi} [T]$$

$$d\Phi_2 = B_2 ds = \frac{\mu I}{2\pi r} dr dz$$

$$d\Lambda_2 = \frac{\mu I}{2\pi r} dr dz \Rightarrow \Lambda_2 = \int_{r=a}^b \int_{z=0}^l \frac{\mu I}{2\pi r} dr dz = \frac{\mu I l}{2\pi} \ln\left(\frac{b}{a}\right)$$

$$L_{ext} = \frac{\Lambda_2}{I} = \frac{\mu l}{2\pi} \ln\left(\frac{b}{a}\right) [H]$$

* Flux linkage is $d\Phi_1$ multiplied by the ratio of the area within the path enclosing the flux to the total area

$$\therefore \text{total } L = L_{in} + L_{ext}$$

$$L = \frac{\mu l}{2\pi} \left[\frac{1}{4} + \ln\left(\frac{b}{a}\right) \right] [H]$$

Method 2

Knowing: $W_m = \frac{1}{2} L I^2 = \frac{1}{2} \int \vec{B} \cdot \vec{H} dV = \frac{1}{2} \int \frac{B^2}{\mu} dV$

$$L_{in} = \frac{2W_m}{I^2} = \frac{2}{I^2} \cdot \frac{1}{2} \int \frac{B_1^2}{\mu} dV$$

$$= \frac{1}{I^2 \mu} \int_0^l \int_0^{2\pi} \int_0^a \left(\frac{\mu I r}{2\pi a^2} \right)^2 r dr d\phi dz$$

$$= \frac{\mu l}{8\pi} [H]$$

$$L_{ext} = \frac{2}{I^2} \int \frac{B_2^2}{2\mu} dV = \frac{1}{4I^2} \int_0^l \int_0^{2\pi} \int_a^b \left(\frac{\mu I}{2\pi r} \right)^2 r dr d\phi dz$$

$$L_{ext} = \frac{\mu}{4\pi^2} (l)(2\pi) \ln(b/a) = \frac{\mu l}{2\pi} \ln(b/a)$$

$$L = \frac{\mu l}{2\pi} \left(\frac{1}{4} + \ln(b/a) \right) [H]$$

if $a \ll b$, so
ln term dominates
and we usually
ignore contribution
of inner

Ch. 6: Dynamic Fields

so far, concentrated on static EM fields where
electrostatic fields ($\vec{E}$) and magnetostatic fields
($\vec{H}$) are independent of each other

$$\begin{array}{l} Q \rightarrow \vec{E} \\ I \rightarrow \vec{H} \end{array} \quad \text{if} \quad \frac{dQ}{dt} \quad \frac{dI}{dt} \Rightarrow \begin{cases} E \text{ changes} \\ H \text{ changes} \end{cases} \Rightarrow \text{then they couple together and travel as electromagnetic waves}$$

Maxwell's Equations

Point Form	Integral Form
Gauss's Law: $\nabla \cdot \vec{D} = \rho_v$	$\oint \vec{D} \cdot d\vec{s} = Q_{enc}$
Gauss's Law for mag: $\nabla \cdot \vec{B} = 0$	$\oint \vec{B} \cdot d\vec{s} = 0$
Faraday's Law: $\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$	$\oint \vec{E} \cdot d\vec{l} = -\frac{\partial}{\partial t} \int \vec{B} \cdot d\vec{s}$
Ampere's Law: $\nabla \times \vec{H} = \vec{J}_c + \frac{\partial \vec{D}}{\partial t}$	$\oint \vec{H} \cdot d\vec{l} = \int_S \left(\vec{J} + \frac{\partial \vec{D}}{\partial t} \right) \cdot d\vec{s}$

Lorentz Force Equation: $\vec{F} = q(\vec{E} + \vec{u} \times \vec{B})$

Constitutive Relations: $\begin{cases} \vec{D} = \epsilon \vec{E} \\ \vec{B} = \mu \vec{H} \\ \vec{J} = \sigma \vec{E} \end{cases}$

- * stationary charges $\rightarrow$ electrostatic field
- * steady current $\rightarrow$ magnetostatic field
- * time varying currents $\rightarrow$ electromagnetic fields

2 Major Concepts

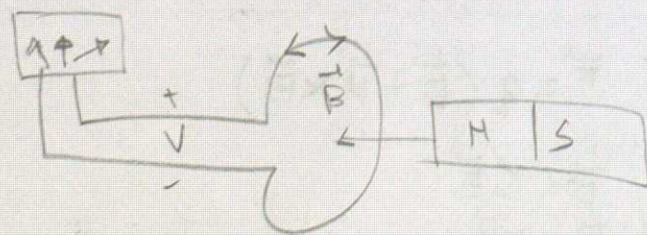
- 1) Electromotive force (emf) based on Faraday's experiments
- 2) Displacement current that resulted from Maxwell's hypothesis

6-1: Faraday's Law

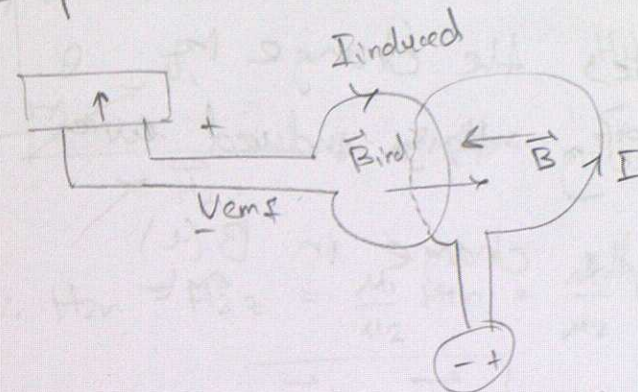
- * Orsted established connection b/n electr. and magn.
- * Faraday hypothesized that if I produces B , then B should produce I called I_{induced}

Experiment

- * magnetic field can produce I in a closed loop only if B changes, i.e.: $\frac{\partial B}{\partial t}$



- * A voltage is detected called electromotive force (emf)
- * the process is called electromagnetic induction



- * a time-varying magnetic field produces an induced voltage called emf in a closed circuit that causes a current I_{induced} to flow

$$V_{\text{emf}} = -N \frac{\partial \Phi}{\partial t} = -N \frac{\partial}{\partial t} \int \vec{B} \cdot d\vec{s} \quad [V]$$

- * negative sign shows the resulting emf opposes the generating magnetic field (comes from Lenz's law)
- * Variation of flux with time may be achieved in 3 ways:

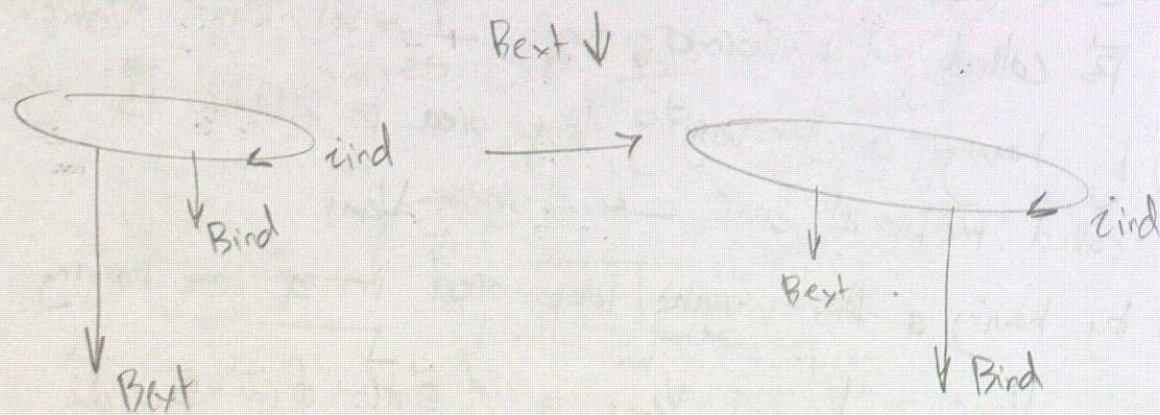
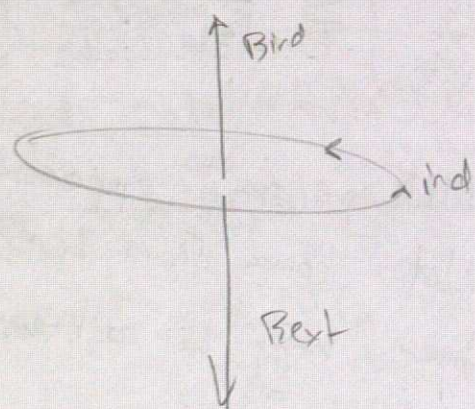
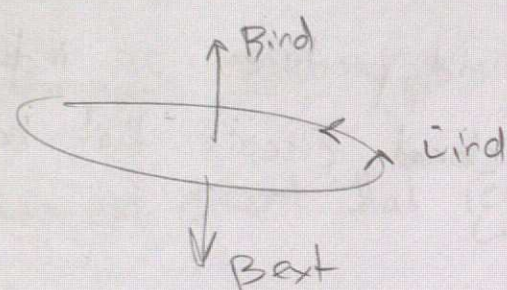
- 1) by having a stationary loop in a time-varying $\vec{B}$ called transformer emf $\rightarrow$ shown $V_{\text{emf}}^{\text{tr}}$
- 2) by having a time-varying loop area in static $\vec{B}$ called motional emf $\rightarrow$ shown $V_{\text{emf}}^{\text{m}}$

- 3) by having a time-varying loop area in a time varying $\vec{B}$

$$V_{\text{emf}} = V_{\text{emf}}^{\text{tr}} + V_{\text{emf}}^{\text{m}} = \oint_C \vec{E} \cdot d\vec{l} + \oint_C (\vec{u} \times \vec{B}) \cdot d\vec{l}$$

Lenz's Law

- induced current direction is set its magnetic field opposes the change in magnetic flux inducing this induced current
- Note: B_{ind} opposed the change in B_{ext}



Problem 5.32

a)

z-comp.

$\vec{H}_1$

$\vec{H}_2$

xy-plane

$$\vec{H}_{1n} = H_{1z} \hat{z} \Rightarrow H_{1n} = H_{1z}$$

$$H_{1t} = H_{1x} \hat{x} + H_{1y} \hat{y} \Rightarrow H_{1t} = \sqrt{H_{1x}^2 + H_{1y}^2}$$

from theory: $\vec{B}_{1n} = \vec{B}_{2n}$

$$\mu_1 \vec{H}_{1n} = \mu_2 \vec{H}_{2n}$$

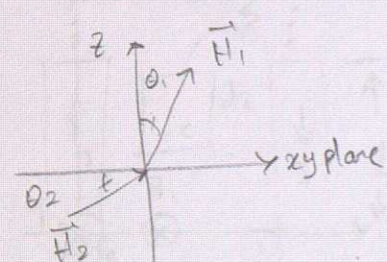
$$\therefore H_{2n} = H_{2z} = \frac{\mu_1}{\mu_2} H_{1n} = \frac{\mu_1}{\mu_2} H_{1z} //$$

from theory: $\vec{H}_{1t} = \vec{H}_{2t}$ since no J_s

$$\therefore \hat{x} H_{1x} + \hat{y} H_{1y} = \hat{x} H_{2x} + \hat{y} H_{2y} \Rightarrow H_{2x} = H_{1x}, H_{2y} = H_{1y} //$$

$$\therefore \vec{H}_2 = \hat{x} H_{1x} + \hat{y} H_{1y} + \hat{z} \frac{\mu_1}{\mu_2} H_{1z}$$

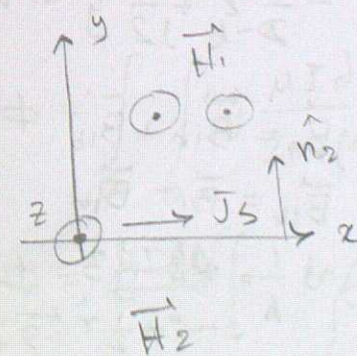
b)



$$\tan \theta_1 = \frac{|\vec{H}_{1t}|}{|\vec{H}_{1n}|} = \frac{\sqrt{H_{1x}^2 + H_{1y}^2}}{H_{1z}}$$

$$\tan \theta_2 = \frac{|\vec{H}_{2t}|}{|\vec{H}_{2n}|} = \frac{\sqrt{H_{1x}^2 + H_{1y}^2}}{\frac{\mu_1}{\mu_2} H_{1z}}$$

Problem 5.33



from theory: $\hat{n}_2 \times (\vec{H}_1 - \vec{H}_2) = \vec{J}_s$

$\hat{n}_2 = \hat{y}$

$$\vec{J}_s = \hat{x} 8$$

$$\Rightarrow \hat{y} \times (\hat{z} 11 - \vec{H}_2) = \hat{x} 8$$

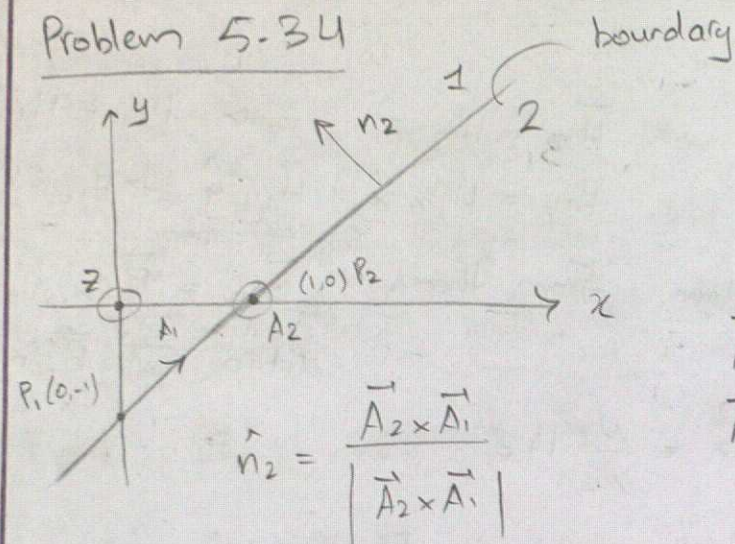
$$\hat{z} 11 - \hat{y} \times \vec{H}_2 = \hat{x} 8 \quad \therefore \vec{H}_2 = \hat{z} 3$$

$$\hat{x} 3 = \hat{x} H_{2x} - \hat{z} H_{2z}$$

$$\therefore H_{2z} = 3$$

$$= \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ 0 & 1 & 0 \\ H_{2x} & H_{2y} & H_{2z} \end{vmatrix} = \hat{x} H_{2z} - \hat{z} H_{2x}$$

Problem 5.34



$$P_1(0, -1, 0)$$

$$P_2(1, 0, 0)$$

$$P_3(1, 0, 1)$$

$$\vec{A}_1 = 1\hat{x} + 1\hat{y}$$

$$\vec{A}_2 = 1\hat{z}$$

$$\vec{A}_2 \times \vec{A}_1 = \vec{n}_2$$

$$\hat{n}_2 = \frac{\vec{A}_2 \times \vec{A}_1}{|\vec{A}_2 \times \vec{A}_1|}$$

$$\vec{A}_2 \times \vec{A}_1 = \hat{z} \times (\hat{x} + \hat{y}) = \hat{y} - \hat{x} \Rightarrow \hat{n}_2 = -\frac{1}{\sqrt{2}}\hat{x} + \frac{1}{\sqrt{2}}\hat{y} //$$

$$|\vec{A}_2 \times \vec{A}_1| = \frac{1}{\sqrt{2}}$$

$$\text{from theory: } \vec{B}_{1n} = \vec{B}_{2n} \quad \text{no } \int$$

$$\Rightarrow \vec{B}_{1n} = \vec{B}_{2n}$$

dot with dir. to get that comp. of $\vec{B}_1$

$$\vec{H}_{1t} = \vec{H}_{2t}$$

$$B_{1n} = \hat{n}_2 \cdot \vec{B}_1 = B_{2n}$$

$$= \left(-\frac{1}{\sqrt{2}}\hat{x} + \frac{1}{\sqrt{2}}\hat{y}\right) \cdot (\hat{x}2 + \hat{y}3)$$

$$= -\frac{2}{\sqrt{2}} + \frac{3}{\sqrt{2}} = \frac{1}{\sqrt{2}} = B_{2n}$$

$$\text{also, } \hat{n}_2 = \frac{\vec{B}_{2n}}{|\vec{B}_{2n}|} \Rightarrow \vec{B}_{2n} = \hat{n}_2 |\vec{B}_{2n}| = -\frac{1}{2}\hat{x} + \frac{1}{2}\hat{y} = \vec{B}_{2n} //$$

$$\textcircled{2} \vec{H}_{1t} = \vec{H}_{2t} \Rightarrow \vec{B}_{2t} = \frac{\mu_2}{\mu_1} \vec{B}_{1t}, \text{ also, } \vec{B}_1 = \vec{B}_{1n} + \vec{B}_{1t}$$

$$\vec{B}_{1t} = \vec{B}_1 - \vec{B}_{1n}$$

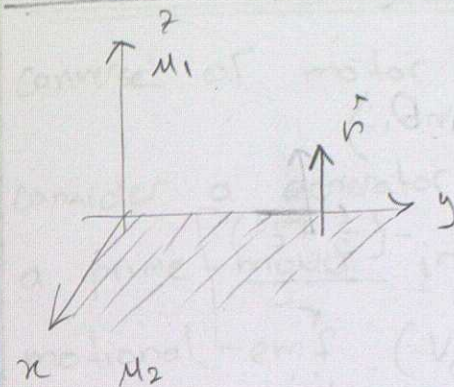
$$= \frac{\mu_2}{\mu_1} (2.5\hat{x} + 2.5\hat{y})$$

$$\vec{B}_{2t} = \frac{1}{2}\hat{x} + \frac{1}{2}\hat{y} //$$

$$= \hat{x}2 + \hat{y}3 - \left(-\frac{1}{2}\hat{x} + \frac{1}{2}\hat{y}\right) = 2.5\hat{x} + 2.5\hat{y}$$

$$\vec{B}_2 = \vec{B}_{2n} + \vec{B}_{2t} = 1\hat{y}$$

Problem 5.35



$$\vec{B}_{1n} = \vec{B}_{2n}, \vec{H}_{1t} = \vec{H}_{2t}$$

$$B_{1n} = B_{1z}$$

$$B_{2n} = B_{2z} = B_{1z} = B_{1n} = 8 = B_{2n} //$$

$$\frac{\vec{B}_{1t}}{\mu_1} = \frac{\vec{B}_{2t}}{\mu_2} \Rightarrow \vec{B}_{2t} = \frac{\mu_2}{\mu_1} \vec{B}_{1t}$$

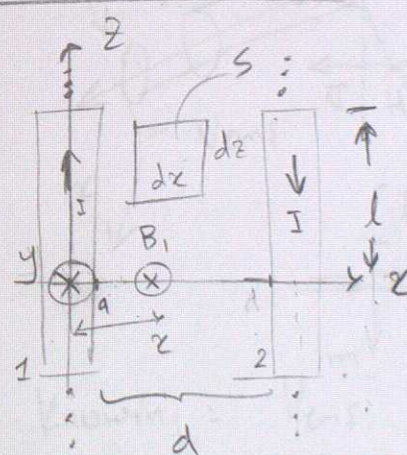
$$= \frac{\mu_2}{\mu_1} (\hat{x}4 - \hat{y}6)$$

$$\vec{B}_{2t} = 20k\hat{x} - 30k\hat{y} //$$

$$\vec{B}_2 = \vec{B}_{2n} + \vec{B}_{2t}$$

$$\vec{B}_2 = 20,000\hat{x} - 30,000\hat{y} + 8\hat{z}$$

Problem 5.37



$$\vec{B}_1 = \hat{y} \frac{\mu I}{2\pi x}$$

$$\vec{B}_2 = \hat{y} \frac{\mu I}{2\pi(d-x)}$$

$$\vec{B} = \vec{B}_1 + \vec{B}_2 = \hat{y} \frac{\mu I}{2\pi} \left[\frac{1}{x} + \frac{1}{d-x} \right]$$

$$\vec{B} = \hat{y} \frac{\mu I d}{2\pi x(d-x)} \Rightarrow \oint \vec{B} \cdot d\vec{s} = ?$$

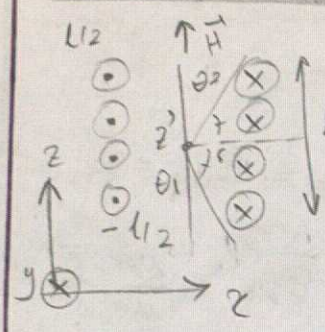
$$d\vec{s} = \hat{y} dx dz$$

$$\Phi = \int_0^l \int_a^{d-a} \hat{y} \frac{\mu I d}{2\pi x(d-x)} \cdot \hat{y} dx dz = \frac{\mu I d l}{2\pi} \int_a^{d-a} \frac{1}{x(d-x)} dx$$

$$\Phi = \frac{\mu I d l}{2\pi} \left[\frac{1}{d} \ln\left(\frac{x}{d-x}\right) \right]_a^{d-a} = \frac{\mu I l}{\pi} \ln\left(\frac{d-a}{a}\right) //$$

$$L = \frac{\Phi}{I} = \frac{\mu l}{\pi} \ln\left(\frac{d-a}{a}\right) \Rightarrow L' = \frac{L}{l} = \frac{\mu}{\pi} \ln\left(\frac{d-a}{a}\right) [H/m]$$

Problem 5.38 (eq. 5.89)



$$\vec{H} = \hat{z} \frac{nI}{2} (\sin\theta_2 - \sin\theta_1)$$

$$= \hat{z} \frac{nI}{2} \left[\frac{\frac{l}{2} - z'}{r} - \frac{-(\frac{l}{2} + z')}{r} \right]$$

$$|\vec{H}| = \frac{nI}{2} \left[\frac{\frac{l}{2} - z'}{r} + \frac{\frac{l}{2} + z'}{r} \right] \Rightarrow$$

Problem 5.39 (eq. 5.99)

$$L' = \frac{\mu_0}{2\pi} \ln\left(\frac{l}{a}\right) = \frac{L}{l} \Rightarrow L = \frac{\mu_0 l}{2\pi} \ln\left(\frac{l}{a}\right)$$

$$L = 416 \text{ nH} \quad \text{and energy} = \frac{1}{2} LI^2$$

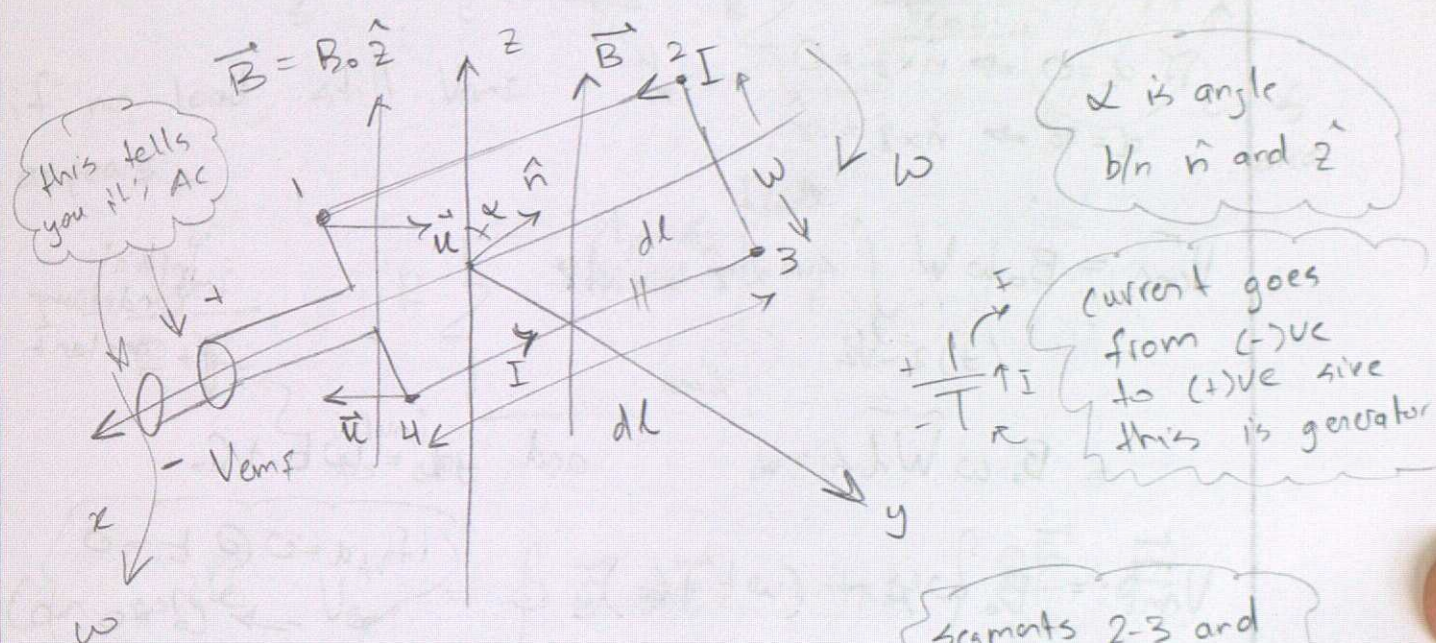
$$W = \frac{1}{2} (416 \text{ n}) (I^2) = 208 I^2 \text{ [nJ]}$$

Problem 5.40

6.5 : Electromagnetic Generators

* converse of motor

* consider a generator where a loop is rotating by a prime-mover in a magnetic field c.w., then motional emf (V_{emf}) is produced in the loop



Knowing: $V_{emf}^m = \oint_1 (\vec{u} \times \vec{B}) \cdot d\vec{l}$

segments $\begin{cases} 1-2 \\ 3-4 \end{cases} \Rightarrow \begin{cases} \vec{u} = \hat{n} \omega \frac{W}{2} \\ \vec{u} = -\hat{n} \omega \frac{W}{2} \end{cases}$

segments 2-3 and 1-4 do not contribute

$$\vec{u} = r\omega$$

$$\vec{u} = \omega \frac{W}{2} \hat{n}$$

$$V_{emf}^m = \int_2^1 (\vec{u} \times \vec{B}) \cdot d\vec{l} + \int_4^3 (\vec{u} \times \vec{B}) \cdot d\vec{l}$$

$$= \int_{-l/2}^{l/2} \left(\hat{n} \omega \frac{W}{2} \times \hat{z} B_0 \right) \cdot \hat{z} dz + \int_{-l/2}^{l/2} \left(-\hat{n} \omega \frac{W}{2} \times \hat{z} B_0 \right) \cdot -\hat{z} dz$$

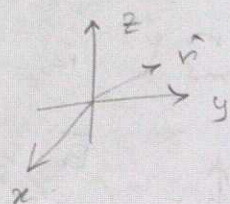
$$V_{emf} = \omega W B_0 \int_{-1/2}^{1/2} (\hat{n} \times \hat{z}) \cdot \hat{x} dx$$

note: angle b/n is α and is rotating @ ω

$$\hat{n} \times \hat{z} = \sin \alpha \hat{x}$$

$$\text{if } \alpha = 0 \Rightarrow \hat{n} \times \hat{z} = 0$$

$$\alpha = 90^\circ \Rightarrow \hat{n} \times \hat{z} = \hat{x}$$



$$V_{emf} = B_0 \omega W \int_{-1/2}^{1/2} \sin \alpha \hat{x} \cdot \hat{x} dx$$

$$= B_0 \omega W L \sin \alpha$$

$$\text{and } \alpha = \omega t + C_0$$

$$V_{emf} = B_0 \omega A \sin(\omega t + C_0)$$

if $\alpha = 0$ @ $t = 0$
 $\Rightarrow C_0 = 0$

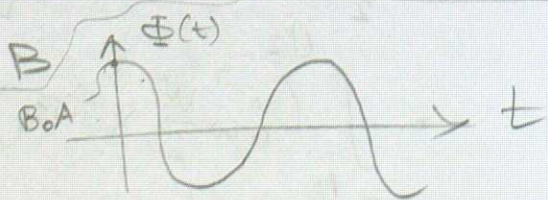
$$\text{if } C_0 \Rightarrow V_{emf} = B_0 \omega A \sin(\omega t)$$

Method 2

Apply Faraday's Law: $V_{emf} = -\frac{d\Phi}{dt}$

note: this is the general case and does not care if change in flux is due to charge in area or change in B

$$V_{emf} = -\frac{d}{dt} (\Phi(t))$$



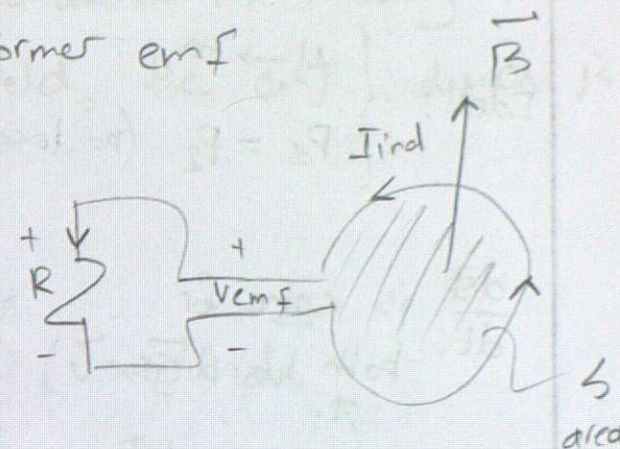
6-2: Stationary Loop in a Time Varying Mag Field

* emf is induced when $\vec{B}$ changes

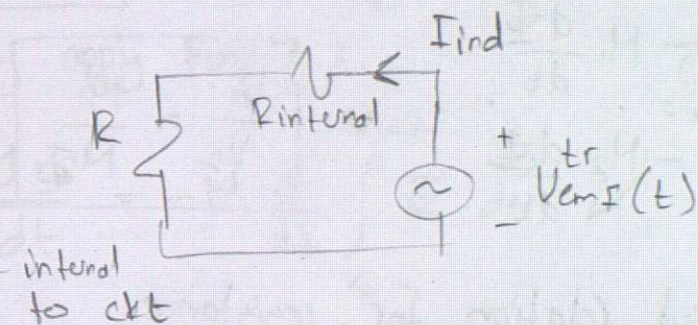
* this emf is called Transformer emf

$$V_{emf}^{tr} = -N \int_S \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s}$$

* if no load, still V_{emf} appears



$$I = \frac{V_{emf}^{tr}}{R + R_i}$$



* Can write $V_{emf}^{tr} = \oint_C \vec{E} \cdot d\vec{l} = -N \int_S \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s}$

* for $N=1 \Rightarrow \oint_C \vec{E} \cdot d\vec{l} = - \int_S \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s}$

* Apply Stokes's:

can equate

$$\oint_C \vec{E} \cdot d\vec{l} = \int_S (\nabla \times \vec{E}) \cdot d\vec{s} \Rightarrow \int_S (\nabla \times \vec{E}) \cdot d\vec{s} = - \int_S \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s}$$

$$\Rightarrow \boxed{\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}} \quad \text{Faraday's Law (differential form)}$$

6-3: Ideal Transformer

+ has 2 coils of windings with N_1, N_2

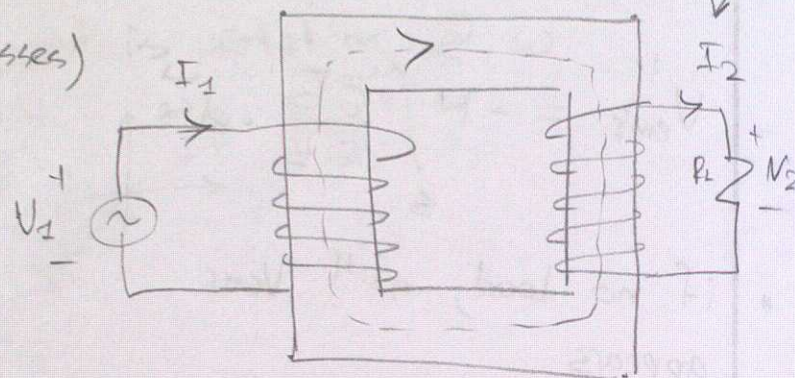
+ Ideal: $\begin{cases} \mu \rightarrow \infty \\ P_1 = P_2 \text{ (no losses)} \end{cases}$

$\frac{d\Phi}{dt}$ is same for both windings

$$\begin{cases} V_1 = -N_1 \frac{d\Phi}{dt} \\ V_2 = -N_2 \frac{d\Phi}{dt} \end{cases}$$

$\rightarrow$

$$\boxed{\frac{V_1}{V_2} = \frac{N_1}{N_2}} \quad \boxed{\frac{I_1}{I_2} = \frac{V_2}{V_1} = \frac{N_2}{N_1}}$$



+ want to find relation for resistance

$$R_{in} = \frac{V_1}{I_1} = V_2 \frac{N_1}{N_2} \cdot \frac{1}{I_1} = V_2 \frac{N_1}{N_2} \cdot \frac{1}{I_2 \frac{N_2}{N_1}} = \frac{V_2}{I_2} \cdot \frac{N_1^2}{N_2^2}$$

$$\Rightarrow \boxed{\frac{R_{in}}{R_L} = \left(\frac{N_1}{N_2}\right)^2}$$

if impedance

$$\boxed{\frac{Z_{in}}{Z_L} = \left(\frac{N_1}{N_2}\right)^2}$$

6-6: Moving Conductor in a time-varying mag field

+ in a general case where a conductor is moving in a time-varying magnetic field, the emf induced is:

$$V_{emf} = V_{emf}^{tr} + V_{emf}^{m}$$

$$= -N \int \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s} + \oint_C (\vec{v} \times \vec{B}) \cdot d\vec{l}$$

+ or can directly apply Faraday's

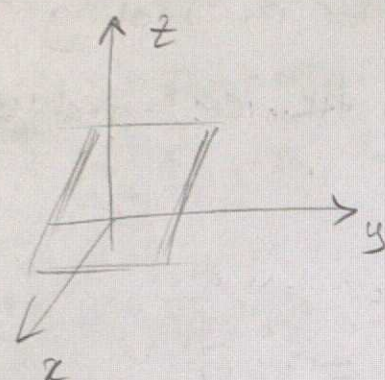
$$V_{emf} = -N \frac{d\Phi}{dt} = -N \frac{d}{dt} \int \vec{B} \cdot d\vec{s}$$

choose which based in case...

6.3

$$V_{\text{emf}} = -N \frac{d\Phi}{dt}$$

$$\Phi = \int d\Phi = \int \vec{B} \cdot d\vec{s}$$



$$d\vec{s} = \hat{z} dx dy$$

$$\begin{aligned} \text{a) } \Phi &= \int \vec{B} \cdot d\vec{s} = \int \hat{z} 20e^{-3t} \cdot \hat{z} dx dy \\ &= 20e^{-3t} \int_{-0.125}^{0.125} dx \int_{-0.125}^{0.125} dy = 20e^{-3t} (0.25)(0.25) \\ &= 1.25e^{-3t} \end{aligned}$$

$$V_{\text{emf}} = -N \frac{d\Phi}{dt} = -100 [(-3)(1.25)e^{-3t}] = \underline{375e^{-3t} \text{ [V]}}$$

$$\begin{aligned} \text{b) } \Phi &= \int \vec{B} \cdot d\vec{s} = 20 \int_{-0.125}^{0.125} \cos x dx \int_{-0.125}^{0.125} dy \times \cos 10^3 t \\ &= (20)(0.25)(0.25) \cos 10^3 t \\ V_{\text{emf}} &= -100 \frac{d}{dt} [1.25 \cos 10^3 t] \\ &= \underline{124.6 \sin 10^3 t \text{ [V]}} \end{aligned}$$

$$\begin{aligned} \text{c) } \Phi &= \int \vec{B} \cdot d\vec{s} = 20 \cos 10^3 t \int_{-0.125}^{0.125} \cos x dx \int_{-0.125}^{0.125} 4 \ln 2 y dy \\ V_{\text{emf}} &= -100 \frac{d\Phi}{dt} = 0 \quad \therefore V_{\text{emf}} = 0 \text{ [V]} \end{aligned}$$

6.4

$$V_{\text{emf}} = 5 \text{ A} \times 0.5 \Omega = 2.5 \text{ V}$$

$$\therefore I_{\text{max}} = 1 \text{ A}$$

$$I = \frac{V_{\text{emf}}}{2 + 0.5} = \frac{2.5 \text{ V}}{2.5 \Omega} = 1 \text{ A}$$

6.5

$$\Phi = \vec{B} \cdot \vec{A} = BA \cos \theta \leftarrow \text{max when B and A aligned so all the B flows through all the A}$$

$$B = B_0 \cos[(6\pi \times 10^8)t + \phi_0] \quad \text{and} \quad V_{\text{emf}} = -N \frac{d\Phi}{dt}$$

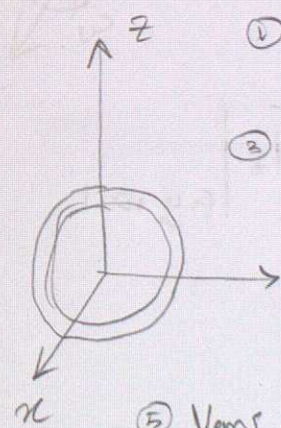
$$V_{\text{emf}} = -0.02 \frac{d}{dt} [B_0 \cos((6\pi \times 10^8)t + \phi_0)]$$

$$30 \times 10^{-3} = (0.02)(6\pi \times 10^8) B_0 \sin[(6\pi \times 10^8)t + \phi_0] \quad \text{at max, } = 1$$

$$\rightarrow B_0 = 8 \times 10^{-8} \text{ [T]}$$

6.8

a)



$$\begin{aligned} \text{① } V_{\text{emf}} &= -N \frac{d\Phi}{dt}, \quad \Phi = \int \vec{B} \cdot d\vec{s} \\ \text{② } \Phi &= \int_a^b \frac{\mu_0 I \cos \omega t}{2\pi r} c dr \times \mu r \\ \vec{B} &= \hat{z} \frac{\mu_0 I_0 \cos \omega t}{2\pi r} \end{aligned}$$

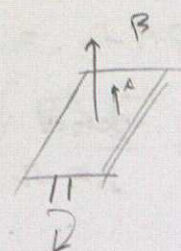
$$\text{③ } \Phi = \frac{\mu_0 I_0 \cos \omega t}{2\pi} \ln(b/a) \mu r$$

$$\text{⑤ } V_{\text{emf}} = -N \frac{d}{dt} \left[\frac{\mu_0 I_0 \ln(b/a)}{2\pi} \cos \omega t \right] = + \frac{N \mu_0 I_0 \ln(b/a)}{2\pi} \omega \sin \omega t$$

$$\text{b) plug } \Rightarrow V_{\text{emf}} = 5.54 \sin 377 t \text{ [V]}$$

6.9 $\omega = \frac{2\pi \times 7200}{60} = 240\pi \text{ rad/s}$

$A = 50 \times 10^{-4} \text{ m}^2$



$\Phi = BA$
 $= A_0 B \cos(\omega t + \phi_0)$

$(V_{\text{emf}})_{\text{peak}} = (1) A \omega B_0$
 $= (50 \times 10^{-4})(240\pi)(6 \times 10^{-6})$
 $= \underline{22.6 \times 10^{-6} \text{ V}}$

6.11 (eq. 6.26) $\rightarrow V_{\text{emf}} = \oint (\vec{u} \times \vec{B}) \cdot d\vec{\ell}$

$\vec{B} = -\hat{z} \frac{\mu_0 I_1}{2\pi r}$ $\vec{u} \times \vec{B} = -(\hat{y} \times \hat{z})(7.5) \frac{\mu_0 I_1}{2\pi r}$
 $= \hat{z} \frac{\mu_0 I_1}{2\pi r}$

$V_{\text{emf}} = \int_0^{0.2} \hat{z} \frac{\mu_0 I_1}{2\pi r} \cdot \hat{z} dz \Big|_{r=y_0} + \int_{0.2}^0 \hat{z} \frac{\mu_0 I_1}{2\pi r} \cdot \hat{z} dz \Big|_{r=y_0+0.1}$
 $= 3 \times 10^{-6} \left(\frac{1}{y_0} - \frac{1}{y_0+0.1} \right)$

$I_2 = \frac{V_{\text{emf}}}{2R} = \underline{150 \times 10^{-9} \left(\frac{1}{y_0} - \frac{1}{y_0+0.1} \right) \text{ [A]}}$

6.12

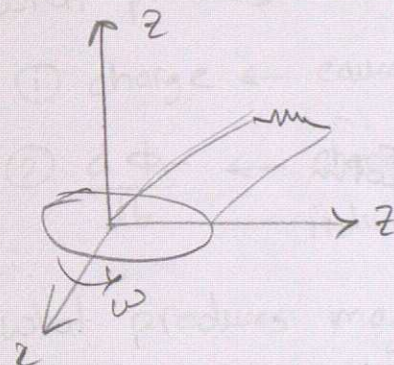
$\Phi = BA \cos(\omega t + \phi_0)$ and $\omega = \frac{3600 \times 2\pi}{60} = 120\pi$
 $= BA \cos(120\pi t + \phi_0)$

$V_{\text{emf}} = +NBA\omega \sin(120\pi t + \phi_0)$
 set = 1

$(V_{\text{emf}})_{\text{pk}} = (0.4)(0.1)(120\pi) = 15.08 \text{ V}$

$I_{\text{pk}} = \frac{(V_{\text{emf}})_{\text{pk}}}{R} = \frac{15.08 \text{ V}}{150 \Omega} = 0.1 \text{ A}$ $\therefore \underline{I_{\text{pk}} = 0.1 \text{ A}}$

6.13



$\vec{u} = \omega \vec{r} = \hat{\phi} \omega r$

$\vec{B} = \hat{z} B_0$

$d\vec{\ell} = \hat{r} dr$

$V_{\text{emf}} = \int (\vec{u} \times \vec{B}) \cdot d\vec{\ell}$

$= \int_0^a (\hat{\phi} \times \hat{z}) \cdot \hat{r} \omega r B_0 dr$
 $= \omega B_0 \int_0^a r dr = \frac{\omega B_0 a^2}{2}$

Week 11: Lecture 1

6-7: Displacement Current

Ampere's Law: $\oint \vec{H} \cdot d\vec{l} = I_{enc} = \int \vec{J} \cdot d\vec{s}$

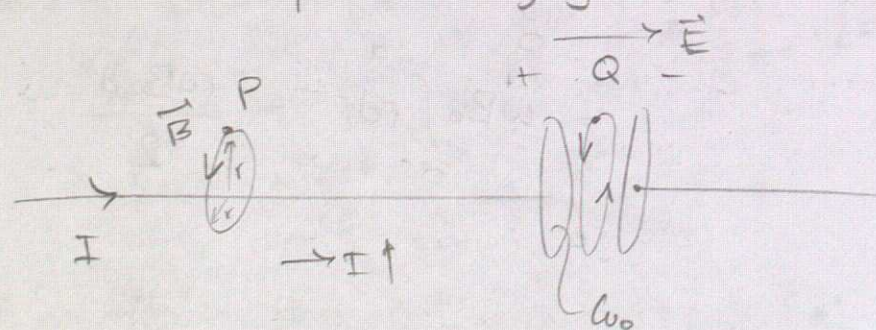
Maxwell added displacement current

$$\left[\oint \vec{H} \cdot d\vec{l} = \int_s \left(\vec{J} + \frac{\partial \vec{D}}{\partial t} \right) \cdot d\vec{s} \right] \rightarrow \text{integral form}$$

conduction current
displacement current

$$\left[\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t} \right] \rightarrow \text{point form}$$

* Consider a capacitor charging as I increases:



* Find B @ P and Q

* apply Ampere's Law: $\oint \vec{B} \cdot d\vec{l} = \mu_0 I_{enc}$

@ $P \Rightarrow B(2\pi r) = \mu_0 I \Rightarrow B = \frac{\mu_0 I}{2\pi r}$ [1]

@ $Q \Rightarrow I_{enc} = 0 \Rightarrow B_Q = 0$
 ? how? $\rightarrow$

* But experiment gives $B_Q \neq 0$

* in fact, $B_Q|_{\text{experiment}} = B_Q|_{\text{Ampere's law}}$

* Ampere: says current produces B

But $I = 0$ inside cap $\Rightarrow$ why is there B_Q ?

* Maxwell: maybe there is something else that is missing in Ampere's Law

* what produces electric field?

① charge $\leftarrow$ causes electric field

② $\frac{d\Phi_m}{dt} \leftarrow$ changing magnetic flux ... Faraday's Law
 induces $V_{emf} \Rightarrow$ electric field, $E = \frac{V}{d}$ ($V = Ed$)

* what produces magnetic field?

① current

② $\frac{d\Phi_E}{dt} \leftarrow$ changing electric field ... Maxwell hypothesized
 that if: change in Φ_m produces $\vec{E}$, then
 change in Φ_E produces $\vec{H}$

* does this answer the capacitor question and the existence of B_Q

* when I increases, then cap charges and E is formed inside cap

* that means electric flux starts increasing

$$\Phi_E = \oint \vec{D} \cdot d\vec{s} \Rightarrow \Phi_E = \epsilon_0 \oint \vec{E} \cdot d\vec{s} \Rightarrow \frac{d}{dt} \Phi_E$$

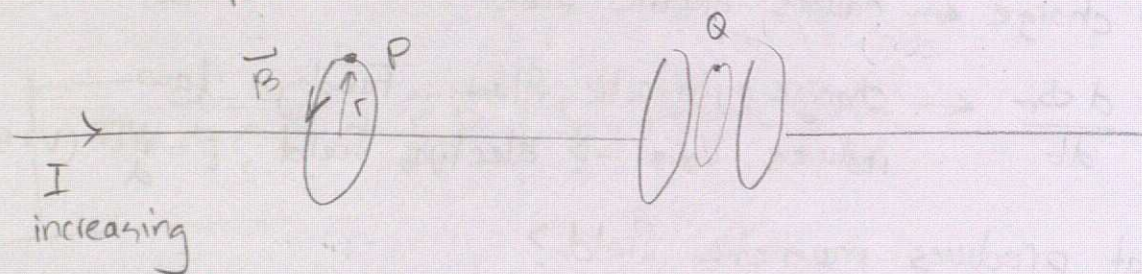
- Maxwell added the missing term to the Ampere's law and called it Displacement Current

$$\oint \vec{H} \cdot d\vec{l} = \int_S \left(\vec{J} + \frac{\partial \vec{D}}{\partial t} \right) \cdot d\vec{S}$$

[A/m²]

can write $\oint \vec{B} \cdot d\vec{l} = \mu_0 \left(I_{enc} + \frac{d\Phi_E}{dt} \right)$

- back to cap: Find $\vec{B}$ @ P and Q



$$\oint \vec{B} \cdot d\vec{l} = \mu_0 \left(I_{enc} + \frac{d\Phi_E}{dt} \right)$$

@ P: $\Phi_E = \epsilon_0 \int \vec{E} \cdot d\vec{S}$ ideal wire $\sigma \rightarrow \infty$
 $R = 0$
 $V = 0 \Rightarrow E = 0$
 $\Phi_E = 0$

$$\therefore B(2\pi r) = \mu_0 (I + 0) \Rightarrow B_P = \frac{\mu_0 I}{2\pi r} \text{ [T]}$$

from next page: $B_P = B_Q$

@ Q: $\Phi_E = \epsilon_0 \int \vec{E} \cdot d\vec{S} = \epsilon_0 EA = \epsilon_0 E(\pi r^2)$

Recall: parallel plate $\vec{E} = \frac{\rho_s}{\epsilon_0}$ or $D = \rho_s$

$$\Rightarrow \Phi_E = \epsilon_0 \frac{\rho_s}{\epsilon_0} \pi r^2 = \rho_s \pi r^2$$

[C/m²] [C/m²]
↙ ↘
A
C/Area

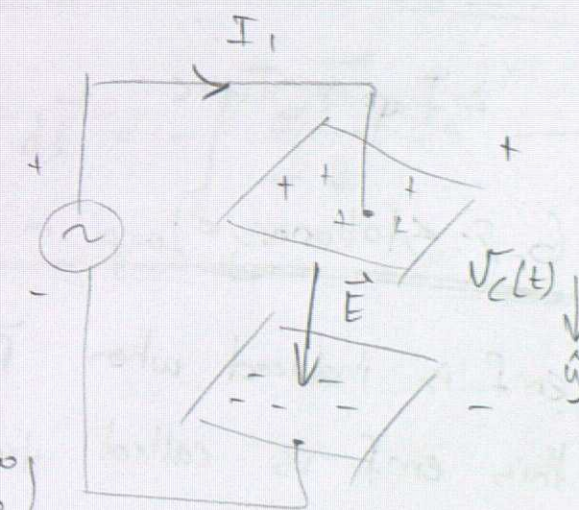
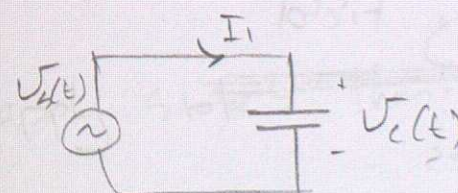
$$\therefore \rho_s \pi r^2 = Q, \text{ and } \frac{d\Phi_E}{dt} = \frac{dQ}{dt} = I$$

ideal cap $\Rightarrow \sigma = 0, R \rightarrow \infty \Rightarrow I_{conduction} = 0$

$$\Rightarrow B(2\pi r) = \mu_0 (0 + I) \Rightarrow B_Q = \frac{\mu_0 I}{2\pi r} \text{ [T]}$$

Consider Capacitor

$$V_s(t) = V_0 \cos \omega t \text{ [V]}$$



perfect wire: $\vec{E} = \vec{D} = 0$ ($\sigma \rightarrow \infty$, $R \rightarrow 0$)

$$\Rightarrow I_{displ} = \int_S \frac{\partial \vec{D}}{\partial t} \cdot d\vec{S} = 0 \text{ (no displacement current)}$$

- the conduction (I_c) is the same as the current charging cap

$$\Rightarrow I_c = C \frac{dV_c}{dt} = C \frac{dV_s}{dt} = C \frac{d}{dt} V_0 \cos \omega t \Rightarrow I_c = -C V_0 \omega \sin \omega t$$

$$I_{\text{total (wire)}} = I_c + I_{\text{D}} = -C V_0 \omega \sin \omega t \text{ [A]}$$

* perfect cap: $\sigma = 0$, $R \rightarrow \infty \Rightarrow I_{\text{zc}} = 0$

$$\vec{E} = \hat{y} \frac{V_c}{d} = \hat{y} \frac{V_0}{d} \cos \omega t \text{ [V/m]} \Rightarrow \vec{D} = \epsilon_0 \vec{E}$$

$$I_{\text{ED}} = \int_s \frac{\partial \vec{D}}{\partial t} \cdot d\vec{s} = \int_s \frac{\partial}{\partial t} \left(\hat{y} \frac{\epsilon_0 V_0}{d} \cos \omega t \right) \cdot \hat{y} d\vec{s}$$

$$= -\frac{\epsilon_0 A V_0 \omega \sin \omega t}{d} \text{ [A]}$$

$$\int d\vec{s} = A$$

$$\frac{\epsilon_0 A}{d} = C$$

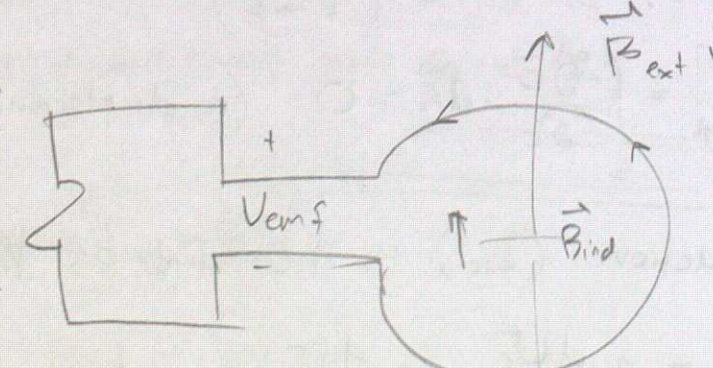
$$I_{\text{cap total}} = -C V_0 \omega \sin \omega t \text{ [A]}$$

$$\therefore I_{\text{cap}} = I_{\text{wire}}$$

6.2: Stationary Loop in t-varying Field

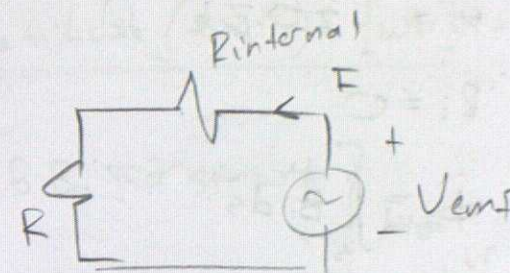
* emf is induced when $\vec{B}$ changes

* this emf is called transformer emf

$$V_{\text{emf}}^{\text{tr}} = -N \int_s \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s}$$


* Note: If no load, still V_{emf} appears

$$I = \frac{V_{\text{emf}}^{\text{tr}}}{R + R_i}$$



* can also write

$$V_{\text{emf}}^{\text{tr}} = \oint_C \vec{E} \cdot d\vec{l} \text{ and } V_{\text{emf}}^{\text{tr}} = - \int_s \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s}$$

for $N=1$

$$\oint_C \vec{E} \cdot d\vec{l} = - \int_s \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s} \quad \text{--- (1)}$$

* apply Stoke's thm:

Ex: Find V_1, V_2 , Area = 4 m^2

$$\vec{B} = -\hat{z} 0.3t \text{ [T]}$$

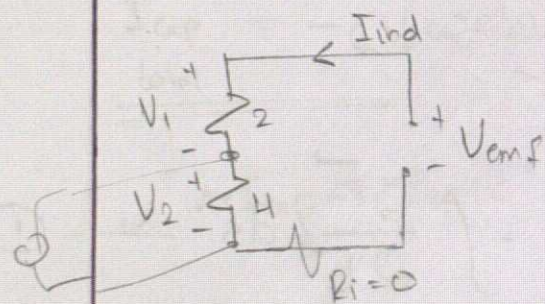
$$R_i = 0$$

$$\Phi_{\text{applied}} = \int_s \vec{B} \cdot d\vec{s}$$

$$= \int (-\hat{z} 0.3t) \cdot \hat{z} ds$$

$$= -0.3t (\text{Area}) = -0.3(4)t = -1.2t \text{ [wb]}$$

$$V_{\text{emf}} = -N \frac{d\Phi_{\text{app}}}{dt} = -(1) \frac{d}{dt} (-1.2t) = 1.2 \text{ [V]}$$



$$I = \frac{V_{\text{emf}}}{R_1 + R_2} = \frac{1.2}{2 + 4} = 0.2 \text{ [A]}$$

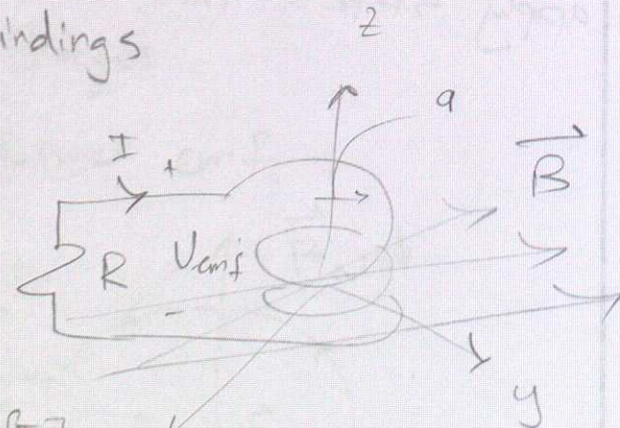
$$V_1 = 2 \times 0.2 = 0.4 \text{ [V]}$$

$$V_2 = 4 \times 0.2 = 0.8 \text{ [V]}$$

Ex: Given N turns of windings

of loop radius a with R

$$\vec{B} = B_0(\hat{y} 2 + \hat{z} 3) \sin \omega t \text{ [T]}$$



a) Flux $\leftarrow I_{\text{ind}}$

b) V_{emf} if $N=10$, $B_0=0.2 \text{ [T]}$

$a=10 \text{ cm}$, $\omega=10^3 \text{ rad/s}$

c) polarity of V_{emf} at $t=0$

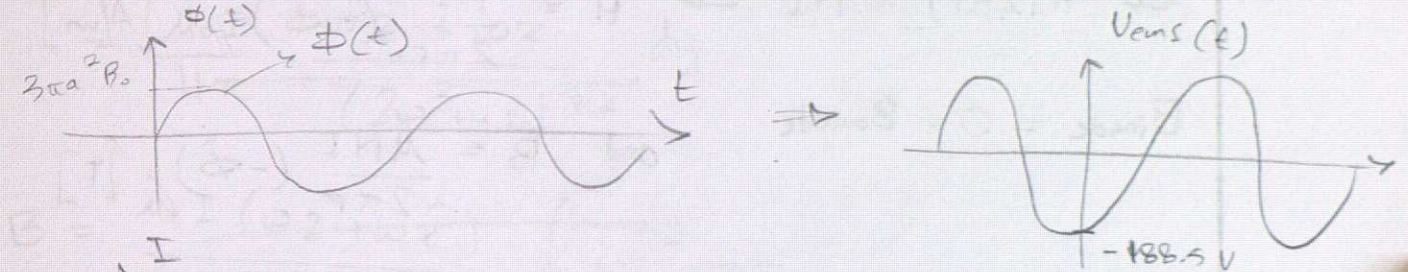
d) I_{ind} for $R=1 \text{ k}\Omega$ and $R_i \ll R$

$$\begin{aligned} \text{a) } \Phi &= \int \vec{B} \cdot d\vec{s} = \int B_0(\hat{y} 2 + \hat{z} 3) \sin \omega t \cdot \hat{z} ds \\ &= \int 3 B_0 \sin \omega t ds = 3 B_0 \sin \omega t (\pi a^2) \text{ [wb]} \end{aligned}$$

$$\text{b) } V_{\text{emf}} = -N \frac{d\Phi}{dt} = -N \frac{d}{dt} [3 B_0 \pi a^2 \sin \omega t]$$

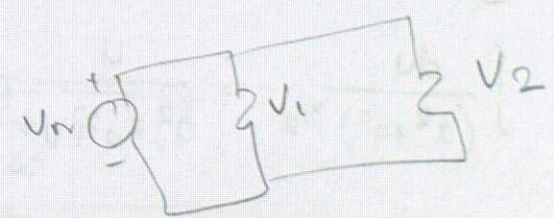
$$V_{\text{emf}} = -N 3 B_0 \pi a^2 \omega \cos \omega t \text{ [V]} \rightarrow \text{plug: } V_{\text{emf}}^{\text{tr}} = -188.5 \cos(10^3 t) \text{ [V]}$$

$$\text{c) } V_{\text{emf}}^{\text{tr}}(0) = -188.5 \cos(0) = -188.5 \text{ [V]}$$



$$\begin{aligned} \text{d) } V_{\text{emf}} &= -188.5 \cos(\omega t) \\ I &= \frac{-(-188.5 \cos \omega t)}{10^3} = 0.19 \cos(10^3 t) \text{ [A]} \end{aligned}$$

Eddy Current



★ Ex: Find magnetic field inside a toroidal coil

turns = N
current = I } Find $\vec{H}$ and $\vec{B}$

* RHR gives direction of $\vec{H}$: $-\hat{\phi}$

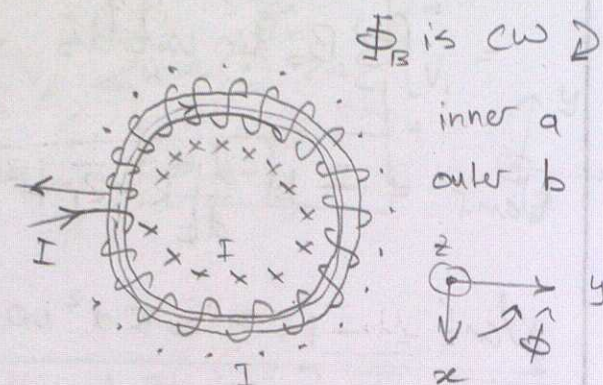
* Apply Ampere's Law:

$$\oint \vec{H} \cdot d\vec{\ell} = I_{enc} \rightarrow I_{enc} = N \cdot I$$

$$\Rightarrow H(2\pi r) = NI \Rightarrow \vec{H} = \frac{NI}{2\pi r} (-\hat{\phi}) \quad [A/m]$$

$B_{inside} = 0 = B_{outside}$

$$\text{and } \vec{B} = \frac{\mu_0 NI}{2\pi r} (-\hat{\phi}) \quad [T]$$



Ex: The square loop shown has current I and is defined by 4 vertices:

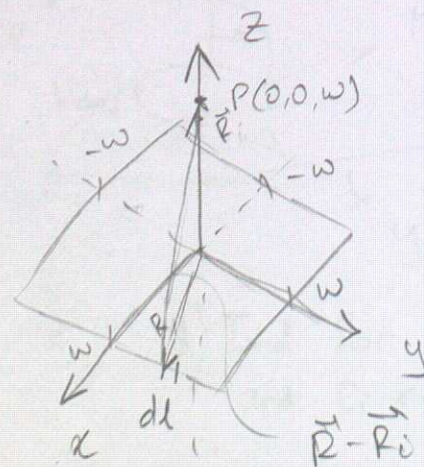
$(w, -w, 0), (-w, w, 0), (-w, -w, 0), (w, w, 0)$

Derive expression for B @ $P(0, 0, w)$

using Biot Savart Law using

$$\int \frac{du}{(a^2 + u^2)^{3/2}} = \frac{u}{a^2 \sqrt{a^2 + u^2}}$$

$$\text{B.S. Law: } d\vec{B} = \frac{\mu_0}{4\pi} \frac{I d\vec{\ell} \times \vec{R}}{R^2}$$



$$d\vec{\ell} = dy \hat{y}, \quad \vec{R} = w \hat{z}, \quad \vec{R}_i = w \hat{x} + y \hat{y}$$

$$\vec{R} - \vec{R}_i = -w \hat{x} - y \hat{y} + w \hat{z}$$

$$d\vec{B} = \frac{\mu_0}{4\pi} \frac{I d\vec{\ell} \times (\vec{R} - \vec{R}_i)}{|\vec{R} - \vec{R}_i|^3}$$

$$= \frac{\mu_0 I}{4\pi} \frac{dy \hat{y} \times (-w \hat{x} - y \hat{y} + w \hat{z})}{(w^2 + y^2 + w^2)^{3/2}}$$

$$= \frac{\mu_0 I}{4\pi} \frac{w \hat{z} + w \hat{x}}{(2w^2 + y^2)^{3/2}} dy$$

$$\vec{B} = \frac{\mu_0 I (w \hat{z} + w \hat{x})}{4\pi} \int_{-w}^w \frac{dy}{(2w^2 + y^2)^{3/2}}$$

$$\vec{B} = \frac{\mu_0 I w (\hat{z} + \hat{x})}{4\pi} \left(\frac{y}{2w^2 \sqrt{2w^2 + y^2}} \right)_{-w}^w$$

$$\vec{B} = \frac{\mu_0 I (\hat{x} + \hat{z})}{4\pi} \frac{1}{\sqrt{3} w^2} \Rightarrow \vec{B} = \frac{\mu_0 I}{4\pi \sqrt{3} w} (\hat{x} + \hat{z}) \quad [T]$$

$$\vec{B}_{tot} = 4\vec{B} \Rightarrow \vec{B}_{tot} = \frac{\mu_0 I}{\sqrt{3} \pi w} \hat{z} \quad [T]$$

* note that $\hat{x}$ comp. cancel out with $-\hat{x}$ comp. and likewise for $\hat{y}$.

Ex: $\vec{B}_{ext}$ changing

A) shows $\vec{B}_{ext}$ (+)ve

B) shows $-\vec{B}_{ext}$ (-)ve

C) both $\vec{B}_{ext}$ and $\vec{B}_{ind}$ are (+)ve

D) none of the above



Week 12: Lecture 2

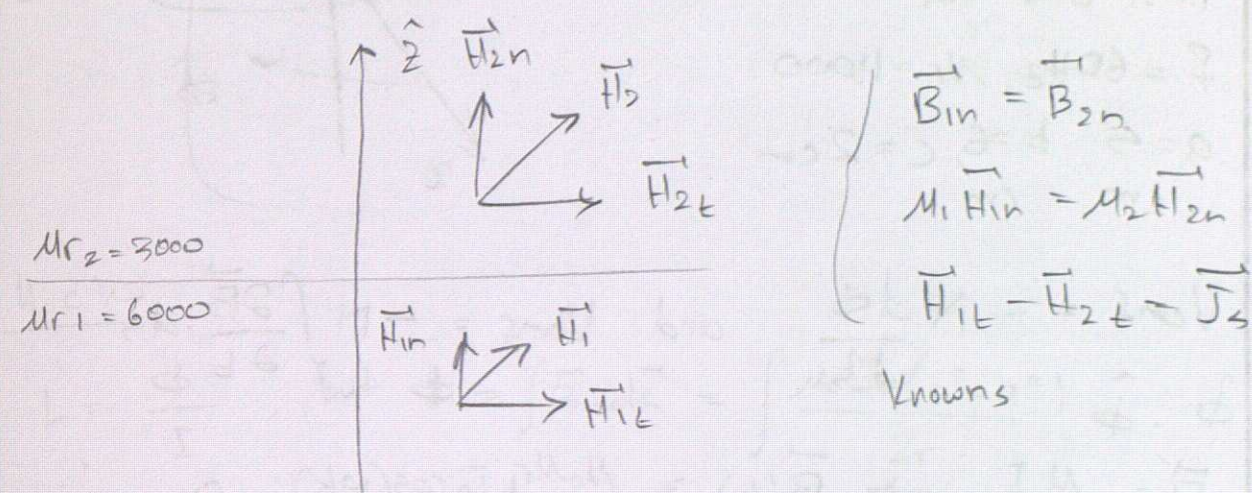
Apr 2, 2025

Ex: the magnetic field is given by

$$\vec{H}_1 = 6\hat{x} + 2\hat{y} + 3\hat{z} \text{ [A/m]} \text{ in medium}$$

with a $\mu_{r1} = 6000$ that exists in $z < 0$

Find $\vec{H}_2$ in medium with $\mu_{r2} = 3000$ for $z > 0$



$$\vec{H}_{1n} = 3\hat{z} \quad \text{and} \quad \vec{H}_{1t} = 6\hat{x} + 2\hat{y}$$

$$\vec{B}_{1n} = \mu_0 \mu_{r1} \vec{H}_{1n} = \mu_0 (6000) (3\hat{z}) = \mu_0 18000 \hat{z}$$

$$\text{Knowing } \vec{B}_{1n} = \vec{B}_{2n} \implies \vec{B}_{2n} = 18000 \mu_0 \hat{z}$$

$$\mu_1 \vec{H}_{1n} = \mu_2 \vec{H}_{2n} \implies \vec{H}_{2n} = \frac{6000}{3000} (3\hat{z}) = 6\hat{z} \text{ [A/m]}$$

$$\vec{H}_{1t} - \vec{H}_{2t} = \vec{J}_s \implies \vec{J}_s = 0$$

$$\vec{H}_{1t} = \vec{H}_{2t} = 6\hat{x} + 2\hat{y} \implies \underline{\underline{\vec{H}_2 = 6\hat{x} + 2\hat{y} + 6\hat{z} \text{ [A/m]}}}$$

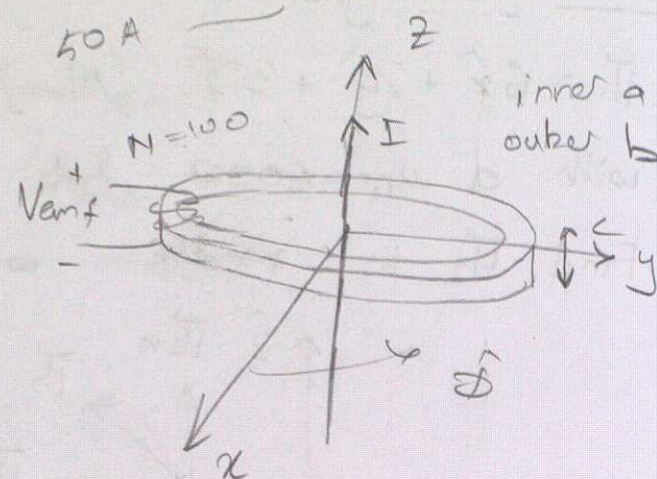
Ex: Consider a toroid and $I = I_0 \cos(\omega t)$ [A]

a) develop expression for emf

b) Find emf for

$$f = 60 \text{ Hz}, N = 4000$$

$$a = 5 \text{ cm}, b = 6 \text{ cm}, c = 2 \text{ cm}$$



$$V_{emf} = -N \frac{d\Phi}{dt} \quad \text{and} \quad V_{emf} = -N \int \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s}$$

$$\vec{B} = \frac{\mu I}{2\pi r} \Rightarrow \vec{B}(t) = \frac{\mu_0 N I_0 \cos(\omega t)}{2\pi r} \hat{\phi}$$

$$V_{emf} = -N \int_a^b \int_0^c \frac{\partial B}{\partial t} dz dr$$

$$= -N \int_a^b \int_0^c \frac{\mu_0 N I_0}{2\pi r} (-\omega \sin \omega t) dz dr$$

$$V_{emf} = \frac{N \mu_0 N I_0 c \omega \sin \omega t}{2\pi} \ln(b/a) \text{ [V]}$$

plug: $V_{emf} = 5.5$

Week 12: Lec 3

Apr 4, 2025

Past Exam

$$B = \begin{cases} 0 & r < a \\ \frac{\mu_0 J_0 (r^2 - a^2)}{2r} & a < r < b \\ 0 & r > b \end{cases}$$

$$q = CV$$

$$C = \frac{Q}{V}$$

$$L = \frac{\Phi}{I}$$

4.c)

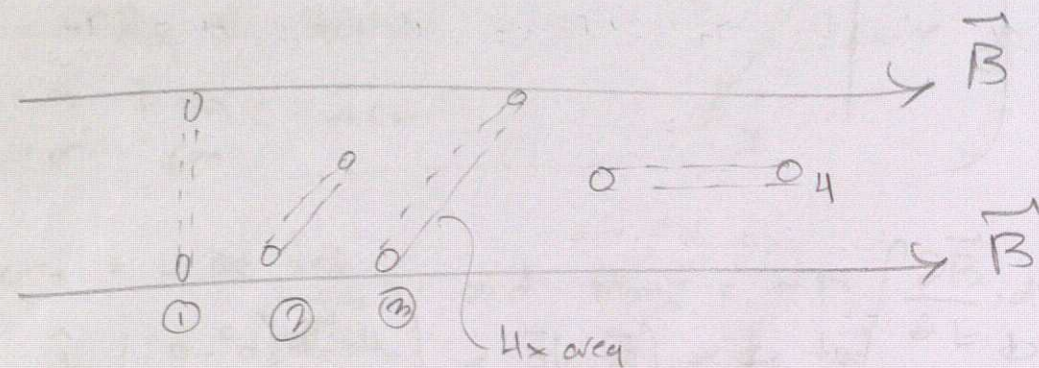
$$L = \frac{\Phi}{I}, \text{ but } \Phi = \int \vec{B} \cdot d\vec{s} = \int \frac{\mu_0 J_0 (b^2 - a^2)}{2r} \hat{\phi} \cdot \hat{\phi} dr dz$$

$$\Phi = \frac{\mu_0 J_0 (b^2 - a^2)}{2} \int_0^d dz \int_h^{h+d} \frac{1}{r} dr = \frac{\mu_0 J_0 (b^2 - a^2)}{2} (d) \ln\left(\frac{h+d}{h}\right)$$

$$L = \frac{\Phi}{I} = \frac{\mu_0 J_0 (b^2 - a^2)}{2} \times d \ln\left(\frac{h+d}{h}\right) \div J_0 \pi (b^2 - a^2)$$

$$\Rightarrow L = \frac{\mu_0 d}{2\pi} \ln\left(\frac{h+d}{h}\right) \text{ [H]}$$

Ex: Consider 4 loops perpendicular to the page. radius of loops 3, 4 are twice loops 1 and 2. B is same. Rank in order from largest to smallest fluxes



$$\pi r^2 \rightarrow 4\pi r^2$$

3, 1, 2, 4

$$\Phi = BA \cos \theta = B(\pi r^2) \cos \theta$$

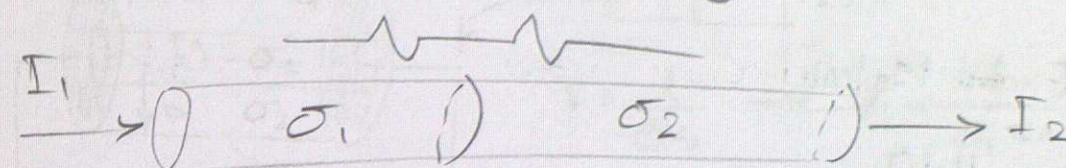
$$\Phi_1 = B \pi (1)^2 \cos 0 = B \pi$$

$$\Phi_2 = B \pi (1)^2 \cos 45^\circ = 0.707 B \pi$$

$$\Phi_3 = B \pi (2)^2 \cos 45^\circ = 0.707 (4) B \pi$$

$$\Phi_4 = B \pi (2)^2 \cos 90^\circ = 0$$

Ex: A wire consists of two equal-diameter with $\sigma_2 > \sigma_1$. The current in segment 1 is I_1 .



a) compare values of currents in the two segments
Is $I_2 >, <, \text{ or } =$ to I_1 ?

Due to KCL (conservation of current)
 $I_1 = I_2$

b) Compare strengths of J_1 and J_2

$$I = JA \rightarrow J_1 = \frac{I_1}{A_1}, J_2 = \frac{I_2}{A_2} = \frac{I_1}{A_1}$$

$$\therefore J_1 = J_2$$

c) Compare strength of electric fields E_1 and E_2 in 2 segments

$$E_2 < E_1$$

ohm's Law
 $J = \sigma E$

$$E_1 = \frac{J_1}{\sigma_1}, E_2 = \frac{J_2}{\sigma_2}$$

$\sigma_2 > \sigma_1$

Final Exam Practice

Midterm Material

* Ch. 4.1 - 4.10

Final Exam Material

* Ch. 4.1 - 4.10

* Ch. 5.1 - 5.8 (-5.4 - 5.5.1) } Focus

* Ch. 6.1 - 6.9

Tutorials

1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11
 midterm final exam

Calc 3 Review

Divergence Theorem

$$\oint_{S=\partial R} \vec{F} \cdot \hat{n} dS = \iiint_R \nabla \cdot \vec{F} dV$$

↓ Gauss Law

$$\oint_S \vec{D} \cdot d\vec{s} = Q_{enc}$$

$$\nabla \cdot \vec{D} = \rho_v$$

$$\nabla \times \vec{D} = 0$$

$$\iiint \nabla \cdot \vec{D} dV = \iiint \rho_v dV = Q_{enc}$$

Stoke's Theorem

$$\oint_{C=\partial S} \vec{F} \cdot \hat{T} ds = \iint_S (\nabla \times \vec{F}) \cdot \hat{n} dS$$

↓ Ampere's Law

$$\oint_C \vec{B} \cdot d\vec{l} = \mu I_{enc}$$

$$\nabla \cdot \vec{B} = 0$$

$$\nabla \times \vec{B} = \mu \vec{J}_s$$

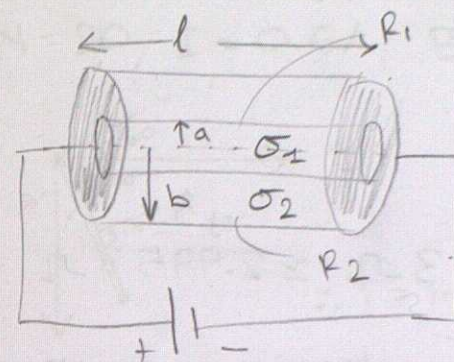
$$\iint_S (\nabla \times \vec{B}) \cdot d\vec{s} = \mu \iint_S \vec{J}_s \cdot d\vec{s} = \mu I_{enc}$$

$$\vec{D} = \epsilon_0 \epsilon_r \vec{E} = \epsilon \vec{E}$$

$$\vec{B} = \mu_0 \mu_r \vec{H} = \mu \vec{H}$$

ECE221 Tutorial 6

✓ 4.44 (from Tut 5)



$$R_T = \frac{R_1 R_2}{R_1 + R_2}$$

$$R = \frac{l}{\sigma S} \rightarrow R_1 = \frac{l}{\sigma_1 \pi a^2}, R_2 = \frac{l}{\sigma_2 \pi (b^2 - a^2)}$$

$$R_1 R_2 = \frac{l^2}{\sigma_1 \sigma_2 \pi^2 a^2 (b^2 - a^2)}$$

$$\frac{1}{R_T} = \frac{1}{R_1} + \frac{1}{R_2} = \frac{\sigma_1 \pi a^2}{l} + \frac{\sigma_2 \pi (b^2 - a^2)}{l} = \frac{\pi (\sigma_1 a^2 + \sigma_2 b^2 - \sigma_2 a^2)}{l}$$

$$R_T = \frac{l}{\pi a^2 (\sigma_1 + \sigma_2 b^2 - \sigma_2)} = \frac{l}{\pi (\sigma_1 a^2 + \sigma_2 (b^2 - a^2))} \quad [2] \quad \checkmark$$

✓ 4.45

$$R_T = \frac{l}{\pi (\sigma_1 a^2 + \sigma_2 (b^2 - a^2))}, \quad \sigma_1 = 0, a = 0.02 \text{ m}, b = 0.03 \text{ m}$$

$$\sigma_2 = 3 \times 10^4, l = 0.2 \text{ m}$$

$$R_T = \frac{0.2}{\pi (3 \times 10^4) (0.03^2 - 0.02^2)} = 4.244 \text{ m}\Omega \quad \checkmark$$

✓ 4.46

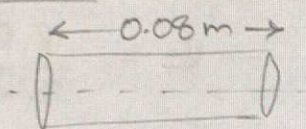
$$\sigma_{Al} = 3.5 \times 10^7, \quad \text{box } 2 \times 10^{-3} \times 10^{-2} = 2 \times 10^{-5} \text{ m}$$

$$\text{sides } 0.05 \times 0.05 \text{ m}$$

$$a) R = \frac{l}{\sigma S} = \frac{0.05}{(3.5 \times 10^7) (2 \times 10^{-5}) (0.05)} = 1.43 \text{ m}\Omega \quad \checkmark$$

$$b) R = \frac{l}{\sigma S} = \frac{2 \times 10^{-5}}{(3.5 \times 10^7) (0.05)^2} = 2.3 \times 10^{-10} \Omega \quad \checkmark$$

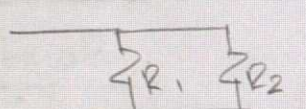
4.47

a)  $\leftarrow 0.08\text{m} \rightarrow$
 $\uparrow 0.5\text{mm} = 0.5 \times 10^{-3}$

$$\sigma_{cr} = 3.4 \times 10^4 \quad \sigma_{cp} = 5.8 \times 10^7$$

$$R = \frac{l}{\sigma A} = \frac{0.08}{(3.4 \times 10^4) \pi (0.5 \times 10^{-3})^2} = 3 \Omega \approx 2.9959 \Omega$$

b) $R_{\text{new}} = 0.60 \times 2.9959 = 1.7975$ $t = b - a$
 $a = 0.5 \times 10^{-3}$

 $R_{\text{new}} = \frac{l}{\pi(\sigma_1 a^2 + \sigma_2 (b^2 - a^2))}$
 $\pi R_{\text{new}} (\sigma_1 a^2 + \sigma_2 b^2 - \sigma_2 a^2) = l$

$$b = \left(\left[\left(\frac{l}{\pi R_{\text{new}}} \right) - \sigma_1 a^2 + \sigma_2 a^2 \right] \frac{1}{\sigma_2} \right)^{1/2}$$

$$b = \left(\left[\left(\frac{0.08}{\pi (1.7975)} \right) + (0.5 \times 10^{-3})^2 (5.8 \times 10^7 - 3.4 \times 10^4) \right] \frac{1}{5.8 \times 10^7} \right)^{1/2}$$

$$b = a + t = 5.000976936 \times 10^{-4}$$

$$t = b - a = 0.0977 \mu\text{m} = t$$

★ 4.62, 5.2

✓ 5.1 $\vec{u} = 8(10)^6 \hat{x}$, $\vec{B} = 4\hat{x} - 3\hat{z}$ $F = m\vec{a}$
 $a = \frac{F}{m}$
 $e = 1.6 \times 10^{-19}$, $m_e = 9.1 \times 10^{-31}$ $\hat{y}$

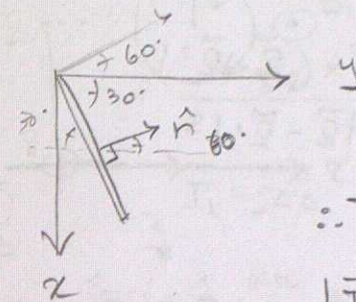
$$\vec{F} = q(\vec{u} \times \vec{B}) = -e(8(10)^6 \hat{x} \times 4\hat{x} - 3\hat{z})$$

$$a = \frac{-(1.6 \times 10^{-19})(8 \times 10^6)(-3)(-\hat{y})}{9.1 \times 10^{-31}} = -4.22 \times 10^{18} \hat{y} \text{ [m/s}^2\text{]} \checkmark$$

ECE221 Tutorial 7

5.4

$N = 20$, $I = 0.5\text{A}$, $\vec{B} = \hat{y} 2.4\text{T}$, $\vec{\tau} = \vec{m} \times \vec{B}$, $\tau = mB \sin \theta$



θ is angle b/n $\hat{n}$ and $\hat{y} \rightarrow \theta = 60^\circ$

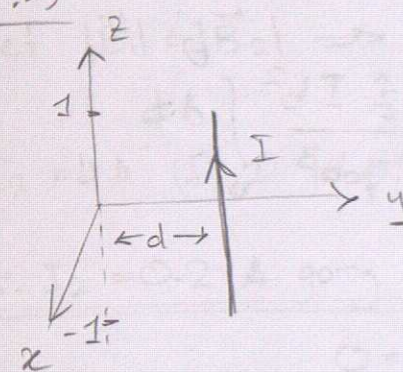
$$\vec{m} = N A I \hat{n}$$

$$\therefore \tau = mB \sin \theta = (20)(0.4 \times 0.2)(0.5)(2.4) \sin 60^\circ$$

$$|\vec{\tau}| = 1.66 \text{ N}\cdot\text{m} \checkmark, \text{ direction CW } \checkmark$$

5.5

a)



$$\vec{F}_m = I(\vec{L} \times \vec{B}), \vec{L} = 2\hat{z}, \vec{B} = \hat{r} 0.2 \cos \phi$$

$$= 5(2\hat{z} \times \hat{r} 0.2 \cos \phi), \phi = \frac{\pi}{2}$$

$$\vec{F}_m = 0 \checkmark$$

b) $\omega = \vec{F} \cdot \vec{d} \Rightarrow d\omega = \vec{F} \cdot d\vec{L} = \vec{F} \cdot \hat{\phi} r d\phi, r = 0.04$

$$\vec{F} = 5(2\hat{z} \times \hat{r} 0.2 \cos \phi) = 2 \cos \phi \hat{\phi}$$

$$\begin{vmatrix} \hat{r} & \hat{\phi} & \hat{z} \\ 0 & 0 & 2 \\ Br & 0 & 0 \end{vmatrix} = -\hat{\phi}(-2Br) = 2Br = 0.4 \cos \phi \hat{\phi}$$

$$\omega = \int \vec{F} \cdot d\vec{L} = \int_{\phi=0}^{\phi=2\pi} 2 \cos \phi \hat{\phi} \cdot 0.04 \hat{\phi} d\phi = 2(0.04) \int_0^{2\pi} \cos \phi d\phi$$

$$= 0$$

$$\therefore \omega_{\text{total}} = 0 \text{ J } \checkmark$$

c)

$$\vec{F} = 2 \cos \phi \hat{\phi} \leftarrow \text{max when}$$

$$\cos \phi = 1 \Rightarrow \phi = 0, \pm \pi, \pm 2\pi \dots \checkmark$$

✓ 5.9 $B = \mu H = \frac{\mu I}{4\pi} \oint \frac{d\vec{l}' \times (\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3}$

$$\therefore d\vec{H} = \frac{I}{4\pi} \frac{d\vec{l}' \times (\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3}$$

①: $d\vec{l}' = -\hat{\phi} r d\phi = -\hat{\phi} b d\phi$

$\vec{r} = 0, \vec{r}' = \hat{r} b \Rightarrow \vec{r} - \vec{r}' = -\hat{r} b$ $\hat{z} \quad \hat{r} \quad \hat{\phi}$
 $|\vec{r} - \vec{r}'|^3 = (b^2)^{3/2} = b^3$ $\hat{\phi} \times \hat{r} = -\hat{z}$

$$\vec{H}_1 = \frac{I}{4\pi} \int_0^\theta \frac{-\hat{\phi} b d\phi \times -\hat{r} b}{b^3} = \frac{-\hat{z} I b^2}{4\pi b^3} \int_0^\theta d\phi$$

$$\vec{H}_1 = -\hat{z} \frac{I\theta}{4\pi b}$$

②: $\vec{H}_2 = 0$ since $d\vec{l}' = \hat{r}$ and $\hat{r} \times \hat{r} = 0$

③: $d\vec{l}' = \hat{\phi} a d\phi$

$\vec{r} = 0, \vec{r}' = a\hat{r} \Rightarrow \vec{r} - \vec{r}' = -\hat{r} a$

$|\vec{r} - \vec{r}'|^3 = (a^2)^{3/2} = a^3$

$\hat{\phi} \times \hat{r} = -\hat{z}$
 $\hat{\phi} \times -\hat{r} = \hat{z}$

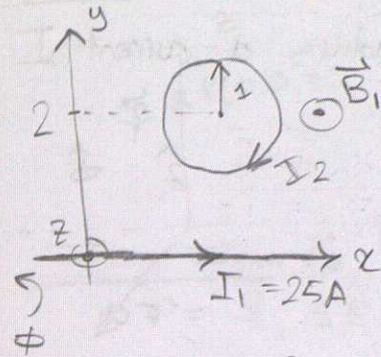
$$\vec{H}_3 = \frac{I}{4\pi} \int_0^\theta \frac{\hat{\phi} a d\phi \times -\hat{r} a}{a^3} = \hat{z} \frac{I\theta}{4\pi a}$$

④: $\vec{H}_4 = 0$ for same reason as ②

$$\therefore \vec{H} = \vec{H}_1 + \vec{H}_2 + \vec{H}_3 + \vec{H}_4 = -\hat{z} \frac{I\theta}{4\pi b} + 0 + \hat{z} \frac{I\theta}{4\pi a} + 0$$

$$\therefore \vec{H} = \frac{I\theta}{4\pi} \left(\frac{1}{a} - \frac{1}{b} \right) \hat{z} \quad \checkmark$$

✓ 5.11



Using R.H.R, $\vec{B}_1$ is in $\hat{z}$. For $\vec{B}$ to be zero at centre of loop, $\vec{B}_2$ must be $-\hat{z}$ and $\therefore$ by RHR, direction of loop current $-\hat{\phi}$ ✓

$$\vec{B}_1 = \frac{\mu I_1}{4\pi} \oint \frac{d\vec{l}' \times (\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3} = \frac{\mu I_1}{2\pi(2)}$$

$$\vec{B}_2 = \frac{\mu I_2}{4\pi} \int_0^{2\pi} \frac{-d\phi \hat{\phi} \times -\hat{r}}{1^3} = -\hat{z} \frac{2\pi \mu I_2}{4\pi} = -\hat{z} \frac{\mu I_2}{2}$$

$-\hat{\phi} \times -\hat{r} = -\hat{z}$

set $|\vec{B}_1| = |\vec{B}_2| \Rightarrow \frac{\mu I_1}{24\pi} = \frac{\mu I_2}{2} \Rightarrow I_2 = \frac{I_1}{2\pi} = \frac{25}{2\pi} \approx 4 \text{ A}$

$I_2 = 4 \text{ A}$ is 1 loop, but since 20 loops, $I_2 = \frac{I_{\text{total}}}{20} = \frac{4}{20} = 0.2$

$\therefore I_2 = 0.2 \text{ A going CW}$ ✓

✓ 5.12 (assume $\otimes$ is (-ve), $\odot$ is (+ve))

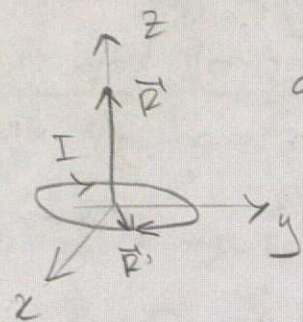
from Biot-Savart theory, we know $\vec{B}_{\text{inf line}} = \frac{\mu I}{2\pi R}$:

$$\therefore \vec{B}_P = \vec{B}_{P1} + \vec{B}_{P2} = -\frac{\mu I_1}{2\pi 0.5} + -\frac{\mu I_2}{2\pi 1.5} = -\frac{\mu}{2\pi} \left(\frac{I_1}{0.5} + \frac{I_2}{1.5} \right)$$

$$\vec{B}_P = \frac{4\pi \times 10^{-7}}{2\pi} \left(\frac{6}{0.5} + \frac{6}{1.5} \right) = 3.2 \mu\text{T [into page]} = \vec{B}_P \quad \checkmark$$

5.14

Derive the $\vec{B}$ at $P(0,0,z)$ for loop radius a current I



$$d\vec{B} = \frac{\mu I}{4\pi} \frac{d\vec{l} \times (\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3}$$

$$d\vec{l} = -\hat{\phi} a d\phi, \quad \vec{r} = \hat{z} z, \quad \vec{r}' = \hat{r} a$$

$$\vec{r} - \vec{r}' = \hat{z} z - \hat{r} a, \quad |\vec{r} - \vec{r}'| = (z^2 + a^2)^{1/2}$$

$$d\vec{l} \times (\vec{r} - \vec{r}') = -\hat{\phi} a d\phi \times (\hat{z} z - \hat{r} a) = -\hat{r} a z d\phi - \hat{z} a^2 d\phi$$

by inspection, $\hat{r}$ component of $\vec{B}$ cancels out

$$\therefore d\vec{B} = \frac{\mu I}{4\pi} \frac{-\hat{z} a^2 d\phi}{(z^2 + a^2)^{3/2}} \Rightarrow \vec{B} = -\hat{z} \frac{\mu I a^2}{4\pi (z^2 + a^2)^{3/2}} \int_0^{2\pi} d\phi$$

$$\vec{B}_m(0,0,z) = -\hat{z} \frac{\mu I a^2}{2(z^2 + a^2)^{3/2}} \quad [T] \quad \text{given } a = 3, I = 40$$

$$\begin{aligned} \text{a) } \vec{B}_T(0,0,0) &= \vec{B}_m(0,0,0) + \vec{B}_m(0,0,-2) \\ &= -\hat{z} \frac{\mu a^2 I}{2} \left(\frac{1}{a^3} + \frac{1}{(2^2 + a^2)^{3/2}} \right) = -\hat{z} 1.32 \times 10^{-5} [T] \end{aligned}$$

$$\text{b) } \vec{B}_T(0,0,1) = \vec{B}_m(0,0,1) + \vec{B}_m(0,0,-1) = -\hat{z} 1.43 \times 10^{-5} [T]$$

$$\text{c) } \vec{B}_T(0,0,2) = \vec{B}_m(0,0,2) + \vec{B}_m(0,0,0) = -\hat{z} 1.32 \times 10^{-5} [T]$$

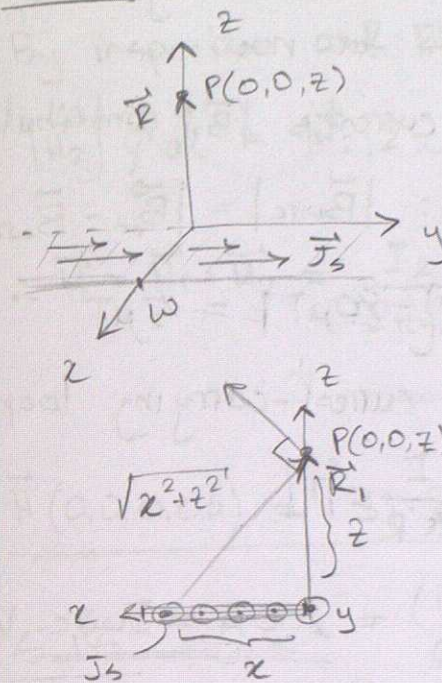
$$\therefore \vec{B} @ 0 = -\hat{z} 13.2 \mu T \quad \checkmark$$

$$@ 1 = -\hat{z} 14.3 \mu T \quad \checkmark$$

$$@ 2 = -\hat{z} 13.2 \mu T \quad \checkmark$$

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5.10



By inspection and RHP, $\vec{B}$ @ P should have no $\hat{y}$ component and positive $\hat{z}$ and $\hat{x}$ components.

We know $I = \int J_s$, and considering a thin infinitely-in-the- y wire, the current in each thin wire is: $\frac{I}{w} = \frac{J_s w}{w} = J_s$

Recall that the $\vec{B}$ at a radial distance R from an infinite wire current is $\vec{B} = \frac{\mu I}{2\pi R} \hat{\phi}$

$$\therefore |d\vec{B}| = \frac{\mu}{2\pi} \frac{J_s dx}{\sqrt{z^2 + x^2}} \quad \text{and we can integrate over } x$$

$$\text{direction: } \hat{y} \times \left(\frac{z}{\sqrt{z^2 + x^2}} \hat{z} - \frac{x}{\sqrt{z^2 + x^2}} \hat{x} \right) \Rightarrow \dots \hat{z} + \hat{x}$$

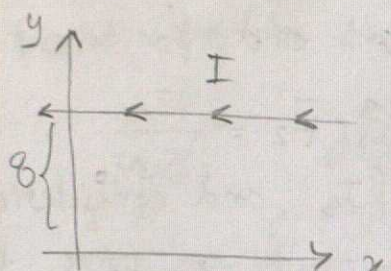
$$\Rightarrow \vec{B} = \frac{\mu J_s}{2\pi} \left[\hat{z} \int_0^w \frac{x}{(\sqrt{z^2 + x^2})^2} dx + \hat{x} \int_0^w \frac{z}{(\sqrt{z^2 + x^2})^2} dx \right]$$

$$= \frac{5\mu}{2\pi} \left[\hat{z} \int_0^w \frac{x}{x^2 + z^2} dx + \hat{x} z \int_0^w \frac{1}{x^2 + z^2} dx \right]$$

$$= \frac{5\mu}{2\pi} \left[\hat{z} \left(\frac{1}{2} \ln(x^2 + z^2) \right)_0^w + \hat{x} z \left(\frac{1}{z} \arctan\left(\frac{x}{z}\right) \right)_0^w \right]$$

$$\vec{B} = \frac{5\mu}{2\pi} \left[\hat{z} \frac{1}{2} \ln\left(\frac{w^2 + z^2}{z^2}\right) + \hat{x} \arctan\left(\frac{w}{z}\right) \right] [T] \quad \checkmark$$

5.13



Since question asks for magnitude, disregard direction for now.
Observe that the current's $|\vec{B}|$ contribution can be found by: $|\vec{B}_{\text{wire}}| = |\vec{B}_{\text{on}} - \vec{B}_{\text{off}}|$
 $\therefore |\vec{B}_{\text{wire}}| = |15\mu\text{T} - 20\mu\text{T}| = 5\mu\text{T}$

Recall that the $\vec{B}$ due to an infinite current-carrying loop at a radial distance R is $|\vec{B}| = \frac{\mu I}{2\pi R} [\text{T}]$

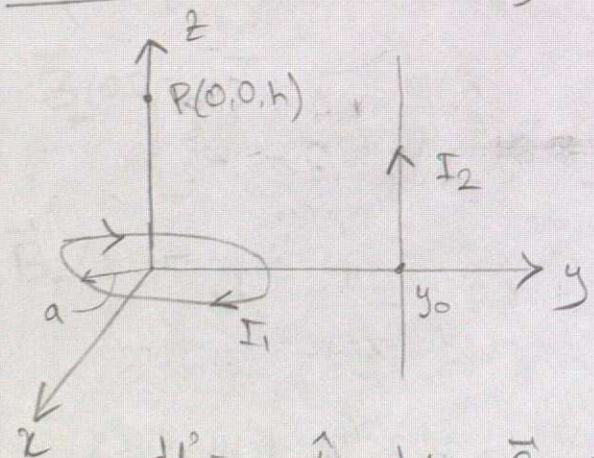
$$\therefore I_{\text{wire}} = \frac{2\pi R |\vec{B}_{\text{wire}}|}{\mu} = \frac{2\pi (8) (5\mu)}{4\pi \times 10^{-7}} = 200\text{A} = I_{\text{wire}} \checkmark$$

5.15

$$B = \mu H$$

We apply superposition:

$$\left. \begin{array}{l} \vec{H}_1 \text{ due to } I_1 \\ \vec{H}_2 \text{ " " } I_2 \end{array} \right\} \vec{H} = \vec{H}_1 + \vec{H}_2$$



$$d\vec{H} = \frac{I}{4\pi} \frac{d\vec{l}' \times (\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3}$$

$$d\vec{l}' = -\hat{\phi} a d\phi, \vec{r} = \hat{z} h, \vec{r}' = \hat{r} a$$

$$\vec{r} - \vec{r}' = -a\hat{r} + h\hat{z} \rightarrow d\vec{l}' \times (\vec{r} - \vec{r}') = -a^2 d\phi \hat{z} - ah d\phi \hat{r}$$

by inspection and RHR, $\vec{H}_1$ has only $\hat{z}$ -comp ($\hat{r}$ comp cancels out)

$$\therefore d\vec{H}_1 = \frac{I_1}{4\pi} \frac{-a^2 d\phi \hat{z}}{(a^2 + h^2)^{3/2}} \Rightarrow \vec{H}_1 = -\hat{z} \frac{\mu I_1 a^2}{4\pi (a^2 + h^2)^{3/2}} \int_0^{2\pi} d\phi$$

$$\therefore \vec{H}_1 = -\hat{z} \frac{I_1 a^2}{2(a^2 + h^2)^{3/2}} [\text{H/m}]$$

For I_2 , use Ampere's Law due to symmetry: $\oint \vec{H} \cdot d\vec{l} = I_{\text{enc}}$
By inspection and RHR, direction of $\vec{H}_2$ is $\hat{x}$.

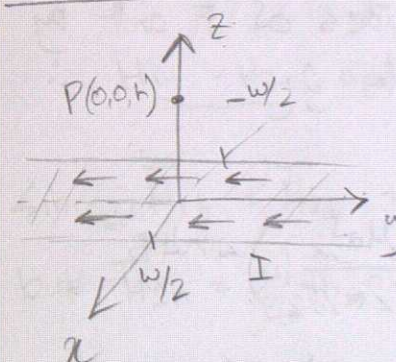
$$|\vec{H}_2| \oint d\vec{l} = |\vec{H}_2| 2\pi y_0 = I_{\text{enc}} = I_2 \Rightarrow |\vec{H}_2| = \frac{I_2}{2\pi y_0} \hat{x}$$

$$\therefore \vec{H} = \vec{H}_1 + \vec{H}_2 = \frac{I_2}{2\pi y_0} \hat{x} - \frac{I_1 a^2}{2(a^2 + h^2)^{3/2}} \hat{z} [\text{H/m}] = \vec{H}(0,0,h) \checkmark$$

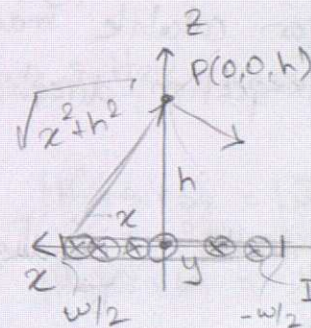
$$b) \vec{H}(0,0,0.04) = 31.83 \hat{x} - 36 \hat{z} [\text{H/m}] \checkmark$$

5.18

a)



could cancel out



Due to RHR and symmetry:

- * direction of $\vec{B}$ is in (+)ve $\hat{z}$ and (-)ve $\hat{z}$
- * can find contribution of 0 to $w/2$ and multiply result by 2

$$|\vec{B}| = \frac{\mu I}{2\pi R} = \frac{\mu I w}{2\pi \sqrt{x^2 + h^2}}, \text{ direction } -\hat{y} \times \left(\frac{-x}{\sqrt{x^2 + h^2}} \hat{x} + \frac{h}{\sqrt{x^2 + h^2}} \hat{z} \right)$$

$$\text{due to symmetry, } \hat{z} \text{ comp. gone} \Rightarrow \frac{-x}{\sqrt{x^2 + h^2}} \hat{z} - \frac{h}{\sqrt{x^2 + h^2}} \hat{z}$$

$$\therefore \vec{B} = 2 \times \vec{B}_{\text{one side}} = \frac{2\mu I}{2\pi w \sqrt{x^2 + h^2}} \left(-\hat{z} \int_0^{w/2} \frac{h}{\sqrt{x^2 + h^2}} dx \right)$$

$$= -\frac{\hat{z} \mu I h}{\pi w} \int_0^{w/2} \frac{1}{x^2 + h^2} dx \Rightarrow \vec{B} = -\frac{\hat{z} \mu I}{w\pi} \arctan\left(\frac{w}{2h}\right) [\text{T}] \checkmark$$

✓ b)

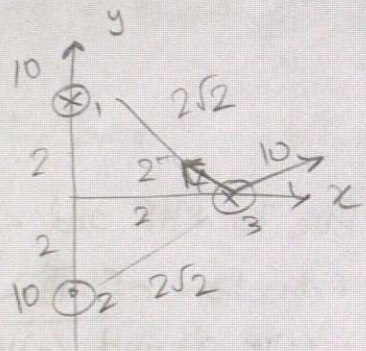
$$\vec{F} = I(\vec{L} \times \vec{B})$$

$$\vec{L} = \hat{y}, \quad \vec{B} = \frac{\mu I \arctan(w/2h)}{\pi w} (-\hat{x})$$

$$\hat{z} \times \hat{y} = \hat{x}$$

$$\therefore \vec{F}_{\text{wire due to sheet}} = \hat{z} \frac{\mu I^2 \arctan(w/2h)}{\pi w} [N] \quad \checkmark$$

✓ 5.19



$$\vec{F}_3 = \vec{F}_{3,1} + \vec{F}_{3,2}$$

Due to symmetry and equal currents, can calculate magnitudes of $\vec{F}$ and by inspection, direction is $\hat{y}$

$$\vec{F}_3 = \hat{y} I_3 \left(\frac{\mu_0 I_1}{2\pi 2\sqrt{2}} \right) \sin 45^\circ + \hat{y} I_3 \left(\frac{\mu_0 I_2}{2\pi 2\sqrt{2}} \right) \sin 45^\circ$$

$$= \hat{y} \frac{2I^2 \mu_0}{4\pi \sqrt{2}} \sin 45^\circ = \hat{y} 1 \times 10^{-5} [N] = \vec{F} \quad \checkmark$$

✓ 5.25

$$\vec{H} = \hat{\phi} \frac{2}{r} [1 - (4r+1)e^{-4r}] [A/m] \text{ for } r \leq 0.05$$

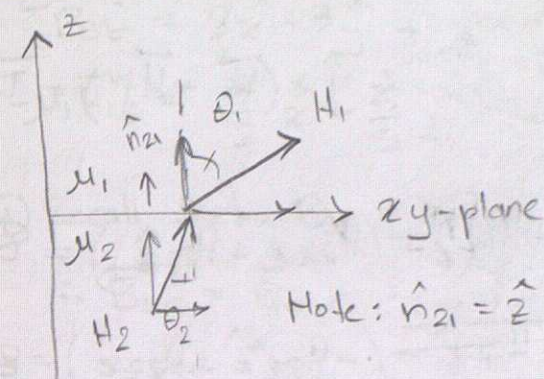
$$\oint_C \vec{H} \cdot d\vec{l} = I_{\text{enc}} = \int_0^{2\pi} \hat{\phi} \frac{2}{r} [1 - (4r+1)e^{-4r}] \cdot \hat{\phi} 0.05 d\phi$$

$$I_{\text{enc}}(0.05) = \frac{4\pi(0.05)}{0.05} [1 - (4 \times 0.05 + 1)e^{-4 \times 0.05}] = 0.2202 \text{ A} \quad \checkmark$$

✓

5.32

a)



$$\text{Let } \vec{H}_1 = \vec{H}_{1n} + \vec{H}_{1t} = \vec{H}_{1z} + \vec{H}_{1x} + \vec{H}_{1y}$$

$$\vec{H}_2 = \vec{H}_{2n} + \vec{H}_{2t} = \vec{H}_{2z} + \vec{H}_{2x} + \vec{H}_{2y}$$

Recall $B_{1n} = B_{2n} \Rightarrow H_{2n} = \frac{\mu_1}{\mu_2} H_{1n}$

$$\mu_1 H_{1n} = \mu_2 H_{2n} \Rightarrow H_{2z} = \frac{\mu_1}{\mu_2} H_{1z}$$

Since $\vec{J}_s = 0$, then $\hat{z} \times (\vec{H}_1 - \vec{H}_2) = 0$

$$\hat{z} \times (\vec{H}_{1x} + \vec{H}_{1y} - (\vec{H}_{2x} + \vec{H}_{2y})) = 0$$

$$\vec{H}_{1y} - \vec{H}_{1x} - (\vec{H}_{2y} - \vec{H}_{2x}) = 0 \Rightarrow \vec{H}_{1y} - \vec{H}_{1x} = \vec{H}_{2y} - \vec{H}_{2x}$$

$$\therefore H_{1y} = H_{2y} \text{ and } H_{1x} = H_{2x} \Rightarrow \vec{H}_2 = H_{1x} \hat{x} + H_{1y} \hat{y} + \frac{\mu_1}{\mu_2} H_{1z} \hat{z}$$

b) Since $\vec{H}_{1t} = \vec{H}_{2t} \Rightarrow |\vec{H}_1| \sin \theta_1 = |\vec{H}_2| \sin \theta_2$

but $\vec{H}_{2n} = \frac{\mu_1}{\mu_2} \vec{H}_{1n} \Rightarrow |\vec{H}_1| \cos \theta_1 = \frac{\mu_1}{\mu_2} |\vec{H}_2| \cos \theta_2$

divide $\frac{\sin \theta}{\cos \theta} = \tan \theta$

$$\tan \theta_1 = \frac{\mu_1}{\mu_2} \tan \theta_2 \quad \checkmark$$

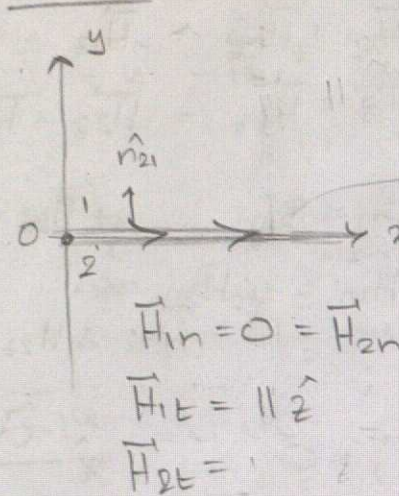
c) $\vec{H}_1 = 2\hat{x} + 0\hat{y} + 4u\hat{z}$ and $\mu_1 = \mu_0, \mu_2 = 4\mu_0$

$$\vec{H}_2 = 2\hat{x} + 0\hat{y} + \frac{\mu_0}{4\mu_0} \cdot 4u\hat{z} = 2\hat{x} + 0\hat{y} + (10)^{-6} \hat{z} [A/m] = \vec{H}_2 \quad \checkmark$$

$$\theta_1 = \arctan\left(\frac{H_{1t}}{H_{1n}}\right) = \arctan\left(\frac{2}{4u}\right) = 89.9999^\circ$$

$$\theta_2 = \arctan\left(\frac{\mu_2}{\mu_1} \tan(\theta_1)\right) = 89.9999^\circ$$

✓ 5.33



$$\hat{x} \quad \hat{y}$$

Note that $\hat{n}_{21} = \hat{y}$

$$\vec{J}_3 = 8\hat{x} \text{ [A/m]} \quad \therefore \hat{y} \times (\vec{H}_1 - \vec{H}_2) = \vec{J}_3$$

$$\hat{y} \times (H_{1x}\hat{x} + H_{1z}\hat{z} - (H_{2x}\hat{x} + H_{2z}\hat{z})) = 8\hat{x}$$

$$\vec{H}_{1n} = 0 = \vec{H}_{2n}$$

$$\vec{H}_{1t} = 11\hat{z}$$

$$\vec{H}_{2t} =$$

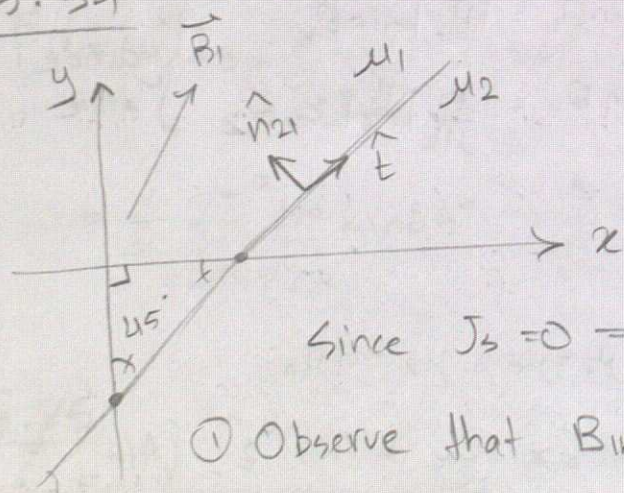
$$-H_{1z}\hat{x} + H_{1z}\hat{x} - (-H_{2z}\hat{x} + H_{2z}\hat{x}) = 8\hat{x}$$

$$-H_{1z}\hat{x} + H_{1z}\hat{x} - H_{2z}\hat{x} = 8\hat{x}$$

$$\hat{x}: H_{1z} - H_{2z} = 8 \rightarrow H_{1z} = 11 - 8 = 3$$

$$\therefore \vec{H}_2 = 0\hat{x} + 0\hat{y} + 3\hat{z} \text{ [A/m]} \quad \checkmark$$

✓ 5.34



$$\hat{n}_{21} = -\frac{1}{\sqrt{2}}\hat{x} + \frac{1}{\sqrt{2}}\hat{y}$$

$$\vec{B}_1 = 2\hat{x} + 3\hat{y}$$

Since $J_3 = 0 \rightarrow B_{1n} = B_{2n}, H_{1t} = H_{2t}$

① Observe that $B_{1n} = \hat{n}_{21} \cdot \vec{B}_1$

$$B_{1n} = -\frac{2}{\sqrt{2}} + \frac{3}{\sqrt{2}} = \frac{\sqrt{2}}{2}$$

$$\textcircled{2} \text{ But } \hat{n}_{21} = \frac{\vec{B}_{1n}}{|\vec{B}_{1n}|} = \frac{\vec{B}_{1n}}{B_{1n}} \Rightarrow \vec{B}_{1n} = \hat{n}_{21} |\vec{B}_{1n}| = \hat{n}_{21} B_{1n}$$

$$\vec{B}_{1n} = \frac{\sqrt{2}}{2} \left(-\frac{1}{\sqrt{2}}\hat{x} + \frac{1}{\sqrt{2}}\hat{y} \right) = -\frac{1}{2}\hat{x} + \frac{1}{2}\hat{y} //$$

③ Observe that $\vec{B}_1 = \vec{B}_{1n} + \vec{B}_{1t} \Rightarrow \vec{B}_{1t} = \vec{B}_1 - \vec{B}_{1n}$

$$\vec{B}_{1t} = 2\hat{x} + 3\hat{y} + \frac{1}{2}\hat{x} - \frac{1}{2}\hat{y} = \frac{5}{2}\hat{x} + \frac{5}{2}\hat{y}$$

$$\mu_1 \vec{H}_{1t} = \frac{5}{2}\hat{x} + \frac{5}{2}\hat{y}$$

④ Recall that $B_{1n} = B_{2n}$ and $H_{1t} = H_{2t}$

$$\therefore \vec{B}_{2n} = \vec{B}_{1n} = -\frac{1}{2}\hat{x} + \frac{1}{2}\hat{y} //$$

$$\therefore \mu_1 \vec{H}_{2t} = \frac{5}{2}\hat{x} + \frac{5}{2}\hat{y}, \text{ but } \vec{B}_{2t} = \mu_2 \vec{H}_{2t} \Rightarrow \vec{H}_{2t} = \frac{\vec{B}_{2t}}{\mu_2}$$

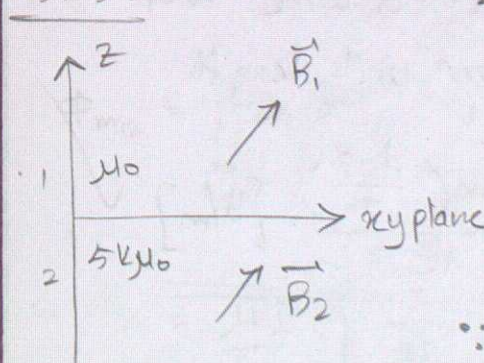
$$\frac{\mu_1}{\mu_2} \vec{B}_{2t} = \frac{5}{2}\hat{x} + \frac{5}{2}\hat{y} = \frac{5\mu_2}{\mu_2} \vec{B}_{2t} = 5\vec{B}_{2t}$$

$$\therefore \vec{B}_{2t} = \frac{1}{5}\hat{x} + \frac{1}{5}\hat{y}$$

$$\textcircled{5} \text{ Since } \vec{B}_2 = \vec{B}_{2n} + \vec{B}_{2t} = -\frac{1}{2}\hat{x} + \frac{1}{2}\hat{y} + \frac{1}{5}\hat{x} + \frac{1}{5}\hat{y} = 1\hat{y}$$

$$\therefore \vec{B}_2 = 1\hat{y} \quad \checkmark$$

✓ 5.35



Since no J_3 mention: $B_{1n} = B_{2n}, H_{1t} = H_{2t}$

$$\vec{B}_1 = 4\hat{x} - 6\hat{y} + 8\hat{z}$$

$$\therefore B_{1n} = B_{2n}, \therefore \vec{B}_{2n} = 8\hat{z} //$$

$$\therefore \vec{B}_{1t} = \mu_1 \vec{H}_{1t} = 4\hat{x} - 6\hat{y} = \mu_1 \vec{H}_{2t}$$

$$\text{and } \vec{H}_{2t} = \frac{\vec{B}_{2t}}{\mu_2}, \therefore \frac{\mu_1}{\mu_2} \vec{B}_{2t} = 4\hat{x} - 6\hat{y}$$

$$\frac{\mu_1}{5\mu_2} \vec{B}_{2t} = 4\hat{x} - 6\hat{y}$$

$$\vec{B}_{2t} = 20\hat{x} - 30\hat{y} //$$

$$\therefore \vec{B}_2 = 20000\hat{x} - 30000\hat{y} + 8\hat{z} \quad \checkmark$$

✓ 5.37

Recall that self inductance $L = \frac{N\Phi_m}{I}$ and observing the symmetry, we can compute contribution due to one wire and multiply by 2:

① $\vec{B} = \frac{\mu I}{2\pi x} \hat{y}$ (recall $\vec{B}$ due to infinite line current, can derive using Ampere's Law)

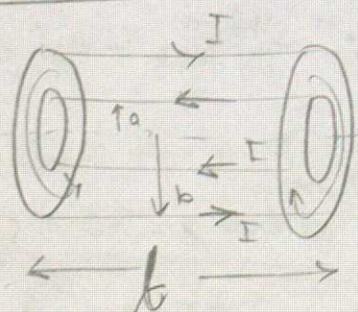
② $\Phi_m = \iint_S \vec{B} \cdot d\vec{A} = \int_a^{d-a} \int_0^l \frac{\mu I}{2\pi x} \hat{y} \cdot dz dx \hat{y}$
 $= \frac{\mu I}{2\pi} \int_0^l dz \int_a^{d-a} \frac{dx}{x} = \frac{\mu I l}{2\pi} \ln\left(\frac{d-a}{a}\right)$

③ $L = \frac{N\Phi_m}{I} = \frac{1 \times \frac{\mu I l}{2\pi} \ln\left(\frac{d-a}{a}\right)}{I} = \frac{\mu l}{2\pi} \ln\left(\frac{d-a}{a}\right)$

④ multiply L by 2 to account for second wire and divide by l to get inductance per unit length

$\frac{2L}{l} = \frac{2\mu l}{2\pi} \ln\left(\frac{d-a}{a}\right) = \frac{\mu \ln\left(\frac{d-a}{a}\right)}{\pi} \text{ [H/m]} \checkmark$

✓ 5.39



$W = \frac{1}{2} L I^2$

$L = \frac{1 \times \Phi_m}{I} = l(b-a)$

$W = \frac{1}{2} \iiint_V \vec{B} \cdot \vec{H} dV = \frac{1}{2} \iiint_V \mu H^2 dV = \frac{1}{2} \int_0^l \int_a^b \int_0^{2\pi} \mu H^2 r d\phi dr dz$

Ampere's Law: $\oint_C \vec{B} \cdot d\vec{l} = \mu I \Rightarrow H(2\pi r) = I$

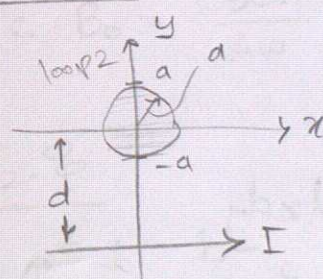
$H = \frac{I}{2\pi r} \Rightarrow W = \frac{1}{2} \mu \int_0^l \int_a^b \int_0^{2\pi} \frac{I^2}{4\pi^2 r^2} r d\phi dr dz$

$W = \frac{\mu I^2 l}{8\pi^2} \int_a^b \frac{1}{r} dr = \frac{\mu I^2 l}{4\pi} \ln\left(\frac{b}{a}\right)$

$\therefore W = \frac{\mu I^2 (3)}{4\pi} \ln(2) = 2(10)^{-4} I^2 \text{ [J]} \checkmark$



5.40



$L_{12} = \frac{N_2 \Phi_{m12}}{I_1} = \frac{1 \times \iint_S \vec{B}_1 \cdot d\vec{S}_2}{I_1}$

$|\vec{B}_1| = \frac{\mu I_1}{2\pi d}, d\vec{S}_2 = \hat{z} r d\phi$
 $x^2 + y^2 = a^2$
 $x = \sqrt{a^2 - y^2}$

$\Phi_{m12} = \iint_S \vec{B}_1 \cdot d\vec{S}_2 = \int_{-a}^a \int_{-\sqrt{a^2-y^2}}^{\sqrt{a^2-y^2}} \frac{\mu I}{2\pi(d+y)} \cdot dx dy$

$= \frac{\mu I}{2\pi} \int_{-a}^a \frac{1}{d+y} 2\sqrt{a^2-y^2} dy$

✓ 6.3

$$V_{\text{emf}} = -N \frac{d}{dt} \Phi_B$$

$$= -N \frac{d}{dt} \iint_S \mathbf{B} \cdot d\mathbf{s}$$

a) If $\vec{B} = \hat{z} 20e^{-3t}$ [T]

$$V_{\text{emf}} = -100 \frac{d}{dt} \int_0^{0.25} \int_0^{0.25} 20e^{-3t} \hat{z} \cdot \hat{z} dx dy$$

$$= -2000(0.25)^2 (-3)e^{-3t}$$

$$V_{\text{emf}} = 375 e^{-3t} \text{ [V]} \quad \checkmark$$

b) If $\vec{B} = \hat{z} 20 \cos x \cos 10^3 t$ [T]

$$V_{\text{emf}} = -100 \frac{d}{dt} \int_0^{0.25} \int_0^{0.25} \hat{z} 20 \cos x \cos 10^3 t \hat{z} dx dy$$

$$= -2000(0.25) \int_0^{0.25} \cos x dx \frac{d}{dt} \cos 10^3 t$$

$$= -2000(0.25) \sin(0.25) (10)^3 (-\sin 10^3 t)$$

$$V_{\text{emf}} = -123.74 \sin 10^3 t \text{ [V]} \quad \checkmark$$

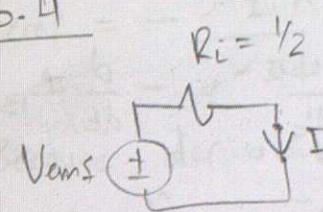
c) $V_{\text{emf}} = -100 \frac{d}{dt} \int_0^{0.25} \int_0^{0.25} 20 \cos x \sin 2y \cos 10^3 t$

$$= -2000 \sin(0.25) \left(-\frac{1}{2} \cos(0.5) + \frac{1}{2} \cos(0) \right) (-\sin 10^3 t)$$

$$V_{\text{emf}} = 30.29 \sin 10^3 t \text{ [V]}$$

wrong since
bounds have
to be $\int_{-0.125}^{0.125} \rightarrow 0$

✓ 6.4

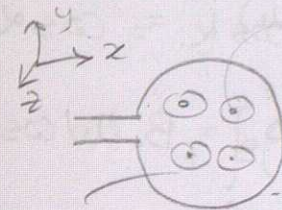


$$V = IR = 5 \times \frac{1}{2} = 2.5 \text{ V}$$

$$I = \frac{V}{R_L} = \frac{2.5}{2.5} = 1 \text{ A}$$

$$\therefore I = 1 \text{ [A]}$$

✓ 6.5



$$\vec{B} = \hat{z} B_0 \cos(\omega t) \rightarrow \omega = 2\pi f = 600\pi \text{ Mrad/s}$$

$$V_{\text{emf}} = -N \frac{d}{dt} \Phi_B = -\frac{d}{dt} B \cdot A \cdot \cos \alpha$$

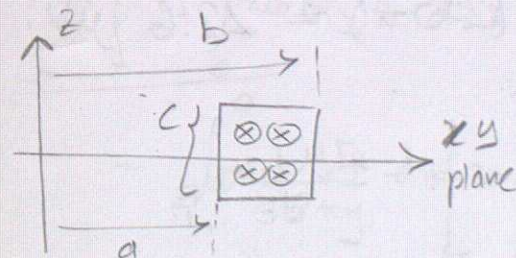
← angle b/n loop and B

area = 0.02 m² Since oriented for max response, $\alpha = 0^\circ \rightarrow \cos \alpha = 1$

$$\therefore 30\text{m} = -A \frac{d}{dt} B_0 \cos(\omega t) = A \omega B_0 \sin(\omega t) \rightarrow \text{set } \sin(\omega t) = 1 \text{ for max } B_0$$

$$\therefore B_0 = \frac{30\text{m}}{A \omega} = \frac{30\text{m}}{(0.02)(600\pi\text{M})} = 795.8 \text{ [pT]} \quad \checkmark$$

✓ 6.8



Recall that $\vec{B}_{\text{line}} = \frac{\mu I(t)}{2\pi R} \hat{\phi}$

$$\therefore |\vec{B}(t)| = \frac{\mu I_0 \cos \omega t}{2\pi x}$$

$$\Phi_B = \iint_S \mathbf{B} \cdot d\mathbf{s} = \int_{-b/2}^{b/2} \int_a^b \frac{\mu I_0 \cos \omega t}{2\pi x} dx dy$$

$$\therefore \Phi_B = \frac{\mu I_0 \cos \omega t}{2\pi} \ln(b/a) \Rightarrow V_{\text{emf}} = -N \frac{d}{dt} \Phi_B$$

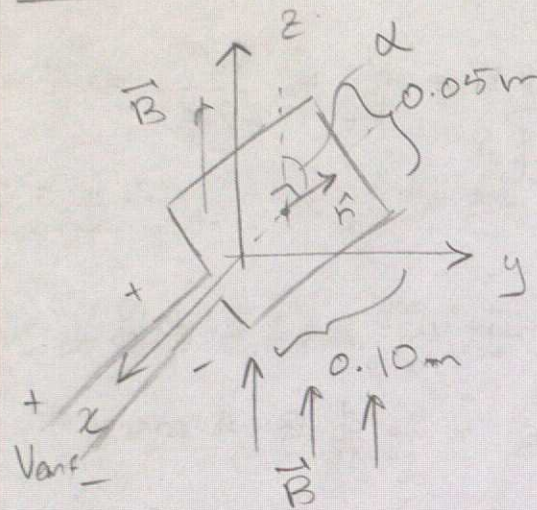
a) $V_{\text{emf}} = + \frac{N \mu I_0 \ln(b/a)}{2\pi} \omega \sin \omega t \text{ [V]}$

since $\mu_r = 4000$

b) $V_{\text{emf}} = 4000(0.02)(4\pi \times 10^{-7})(50) \ln(6/5) 2\pi(60) \sin(602\pi t) \text{ [V]}$

$$V_{\text{emf}} = 5.5 \sin(377t) \text{ [V]} \quad \checkmark$$

✓ 6.9



$$V_{emf} = -N \frac{d\Phi_B}{dt} = -\frac{d}{dt} \Phi_B$$

$$\Phi_B = \iint_S \vec{B} \cdot d\vec{S} = \iint_S B_0 \hat{z} \cdot \hat{n} dz dy$$

$$\hat{z} \cdot \hat{n} = |\hat{z}| |\hat{n}| \cos \alpha = \cos \alpha$$

$$\alpha = \omega t \Rightarrow \Phi_B = B_0 l W \cos \omega t$$

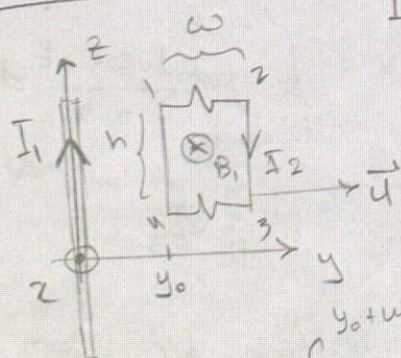
$$V_{emf} = -\frac{d}{dt} [B_0 l W \cos \omega t] = B_0 l W \sin \omega t$$

peak vltage implies $\sin \omega t = 1$

$$\omega = \frac{7200 \text{ rev}}{1 \text{ min}} \times \frac{1 \text{ min}}{60 \text{ s}} \times \frac{2\pi \text{ rad}}{1 \text{ rev}} = 240\pi \text{ rad/s}$$

$$\therefore V_{emf, \text{pk}} = (6\mu)(0.05)(0.10)(240\pi) = 22.6 \text{ } [\mu\text{V}] \quad \checkmark$$

★ 6.11



$$I_2 = \frac{V_{emf}}{2R}, \quad V_{emf} = -1 \times \frac{d}{dt} \Phi_B$$

$$\Phi_B = \iint_S \vec{B} \cdot d\vec{S}$$

$$\vec{B} = -\hat{z} \frac{\mu I_1}{2\pi y}, \quad d\vec{S} = -\hat{z} dz dy$$

$$\Phi_B = \int_{y_0}^{y_0+w} \int_0^h \frac{\mu I_1}{2\pi y} dz dy = \frac{\mu I_1 h}{2\pi} \ln \left(\frac{y_0+w}{y_0} \right)$$

$$\frac{d}{dt} \Phi_B = \frac{\mu I_1 h}{2\pi} \frac{d}{dt} \ln \left(\frac{y_0(t)+w}{y_0(t)} \right)$$

$$V_{emf} = -\frac{\mu I_1 h}{2\pi} \frac{d}{dt} \ln \left(1 + \frac{w}{y_0(t)} \right)$$

Because derivative too trash, try a different method

$$V_{emf} = \oint_C (\vec{u} \times \vec{B}) \cdot d\vec{l} \quad \vec{u} = 7.5 \hat{y} = u_0 \hat{y}, \quad \vec{B} = -\hat{z} \frac{\mu I_1}{2\pi y} = B(y) (-\hat{z})$$

$$= \int_1^2 (u_0 \hat{y} \times -\hat{z} B(y)) \cdot dy \hat{y} + \int_2^3 (u_0 \hat{y} \times -\hat{x} B(y)) \cdot dz \hat{z} + \int_3^4 (u_0 \hat{y} \times -\hat{x} B(y)) \cdot dy \hat{y}$$

$$+ \int_4^1 (u_0 \hat{y} \times -\hat{z} B(y)) \cdot dz \hat{z} = \int_{y_0}^{y_0+w} u_0 B(y) \hat{z} \cdot \hat{y} dy + \int_h^0 u_0 B(y) \hat{z} \cdot d\hat{z} \hat{z} + \int_{y_0}^{y_0+w} u_0 B(y) \hat{z} \cdot d\hat{y} \hat{y}$$

$$+ \int_0^h u_0 B(y) \hat{z} \cdot d\hat{z} \hat{z} = \int_h^0 u_0 \frac{\mu I_1}{2\pi y} dz \Big|_{y=y_0}^h + \int_0^h u_0 \frac{\mu I_1}{2\pi y} dz \Big|_{y=y_0+w}^h$$

$$= \frac{-h u_0 \mu I_1}{2\pi y_0} + \frac{h u_0 \mu I_1}{2\pi (y_0+w)} = \frac{h u_0 \mu I_1}{2\pi} \left(\frac{1}{y_0+w} - \frac{1}{y_0} \right)$$

$$\therefore I_2 = \frac{V_{emf}}{2R} = \frac{h u_0 \mu I_1}{4\pi R} \left(\frac{1}{y_0+w} - \frac{1}{y_0} \right) = 150 \left(\frac{1}{y_0+0.1} - \frac{1}{y_0} \right) [\text{nA}]$$

$$\hat{z} \times \hat{y} = -\hat{x}$$

$$\hat{y} \times \hat{z} = \hat{x}$$

$$\hat{y} \times \hat{x} = -\hat{z}$$

$$\hat{z} \times \hat{x} = \hat{y}$$

$$\hat{x} \times \hat{y} = \hat{z}$$

$$\hat{y} \times \hat{z} = \hat{x}$$

$$\hat{z} \times \hat{x} = \hat{y}$$

$$\hat{x} \times \hat{y} = \hat{z}$$

$$\hat{y} \times \hat{z} = \hat{x}$$

$$\hat{z} \times \hat{x} = \hat{y}$$

$$\hat{x} \times \hat{y} = \hat{z}$$

$$\hat{y} \times \hat{z} = \hat{x}$$

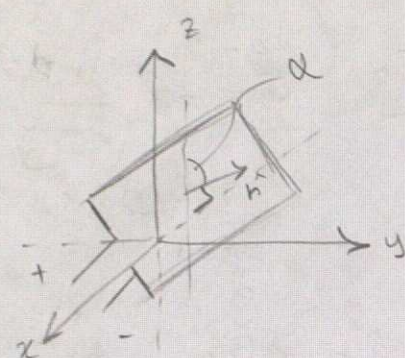
$$\hat{z} \times \hat{x} = \hat{y}$$

$$\hat{x} \times \hat{y} = \hat{z}$$

$$\hat{y} \times \hat{z} = \hat{x}$$

✓ 6.12

$$I = \frac{V_{\text{emf}}}{R}, \quad \mathcal{E}_{\text{emf}} = -1 \frac{d}{dt} \iint \vec{B} \cdot d\vec{s} \stackrel{\text{assum}}{=} -\frac{d}{dt} [B_0 \hat{z} \cdot A \hat{n}]$$



$$= -\frac{d}{dt} [B_0 A \cos \alpha] \text{ where } \alpha = \omega t$$

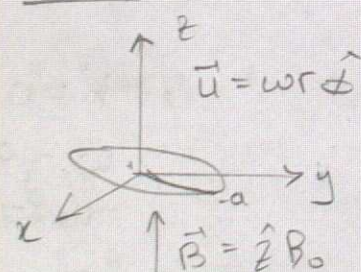
$$= -B_0 A \frac{d}{dt} \cos \omega t \quad \text{set } \sin \omega t = 1$$

$$= +B_0 A \omega \sin \omega t \Rightarrow |V_{\text{emf}}| = B_0 A \omega$$

Note $\omega = \frac{3600 \text{ rev}}{1 \text{ min}} \times \frac{1 \text{ min}}{60 \text{ s}} \times \frac{2\pi \text{ rad}}{1 \text{ rev}} = 120\pi \text{ rad/s}$

$$\therefore I = \frac{V_{\text{emf}}}{R} = \frac{B_0 A \omega}{R} = \frac{(0.4)(0.1)(120\pi)}{150} = \underline{\underline{0.1 \text{ [A]}}} \quad \checkmark$$

6.13



Consider thin "bar" and later integrate

$$\mathcal{E}_{\text{emf}} = \int_C (\vec{u} \times \vec{B}) \cdot d\vec{l} = \int_0^a B_0 \omega r \hat{r} \cdot d\vec{r} \hat{r}$$

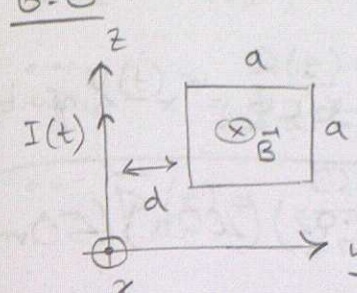
$$= B_0 \omega \int_0^a r dr = \frac{B_0 \omega}{2} a^2 \quad \leftarrow \text{for one thin bar}$$

$$\therefore V_{\text{emf}} = \frac{B_0 \omega a^2}{2} \text{ [V]} \quad \checkmark$$

$$\hat{z} \times \hat{r} = \hat{\phi}$$

✓ 6.6

a)



$$\mathcal{E} = -\frac{d}{dt} \Phi_B, \quad \Phi_B = \iint \vec{B} \cdot d\vec{s}$$

$$|\vec{B}| = \frac{\mu I(t)}{2\pi y}, \quad |d\vec{s}| = dy dz$$

$$a = 0.1 \text{ m}$$

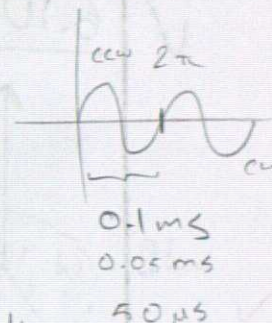
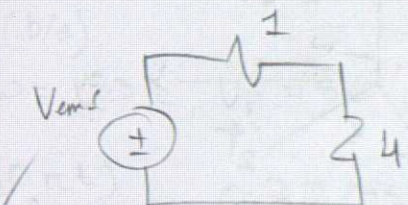
$$d = 0.05 \text{ m}$$

$$\omega = 2\pi \times 10^4$$

$$\Phi_B = \int_d^{d+a} \int_0^a \frac{\mu I(t)}{2\pi y} dy dz = \frac{\mu I(t) a}{2\pi} \ln\left(\frac{d+a}{d}\right)$$

$$V_{\text{emf}} = -\frac{d}{dt} \Phi_B = -\frac{\mu a \ln(d+a/d)}{2\pi} \frac{d}{dt} [5 \cos \omega t]$$

$$= +\frac{\mu a \ln(d+a/d)}{2\pi} (5) \omega \sin \omega t$$

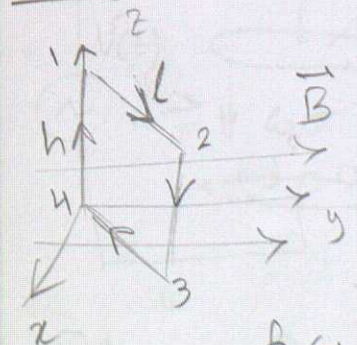


b)

$$V_{\text{emf}} = 6.9 \sin(2\pi \times 10^4 t) \text{ [mV]} \quad \checkmark$$

$$|I| = \frac{V_{\text{emf}}}{5} = 1.38 \text{ mA} \quad \left\{ \begin{array}{l} \text{ccw}, 50 \mu\text{s} (2k+1), k \in 0, \pm 1, \pm 2 \dots \\ \text{cw}, \end{array} \right.$$

✓ 6.7



$$I = \frac{V_{\text{emf}}}{R}, \quad V_{\text{emf}} = \oint_C (\vec{u} \times \vec{B}) \cdot d\vec{l}$$

$$\vec{B} = B_0 \hat{y}, \quad \vec{u}_{11} = 0, \quad \vec{u}_{12} = \vec{u}_{34} = \omega r \hat{\phi}, \quad \vec{u}_{23} = -\omega r \hat{\phi}$$

$$\hat{\phi} \times \hat{y} = (-\sin \phi \hat{x} + \cos \phi \hat{y}) \times \hat{y} = -\sin \phi \hat{z}$$

$$\therefore \oint_C (\vec{u} \times \vec{B}) \cdot d\vec{l} = -\int_1^2 u_{12} B_0 \hat{z} \cdot d\vec{r} \hat{r} + \int_2^3 u_{23} B_0 \hat{z} \cdot d\vec{z} \hat{z} \\ - \int_3^4 u_{34} B_0 \hat{z} \cdot d\vec{r} \hat{r} - \int_4^1 u_{41} B_0 \hat{z} \cdot d\vec{z} \hat{z}$$

$$\hat{z} \cdot \hat{r} = 0$$

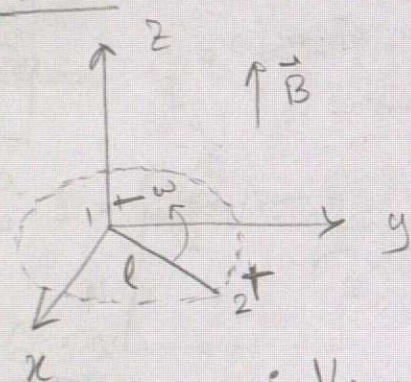
$$\therefore \oint_C (\vec{u} \times \vec{B}) \cdot d\vec{l} = - \int_h^0 u_{23} B_0 dz = hu_{23} B_0$$

$$x - 4 \ln \phi = x - 4 \ln \omega t$$

$$\therefore I = \frac{Q_{enc}}{R}, \therefore I = \frac{hu_{23} B_0}{1/2} = -2(0.03)(0.02)(200\pi)(50m)$$

$$\omega = \frac{6k \text{ rev}}{\text{min}} \times \frac{1}{60} \times 2\pi = 200\pi \Rightarrow I = 37.74 \sin(200\pi t) \text{ [mA]}$$

6.10



$$V_{12} = \int_1^2 (\vec{u} \times \vec{B}) \cdot d\vec{l}$$

$$\vec{u} = r\omega \hat{\phi}, \vec{B} = B_0 \hat{z} \Rightarrow \hat{\phi} \times \hat{z} = \hat{r}$$

$$d\vec{l} = \hat{r} dr$$

$$\omega = 90 \times \frac{2\pi}{60}$$

$$\therefore V_{12} = \int_0^l r\omega B_0 \hat{r} \cdot \hat{r} dr = \frac{\omega B_0 l^2}{2}$$

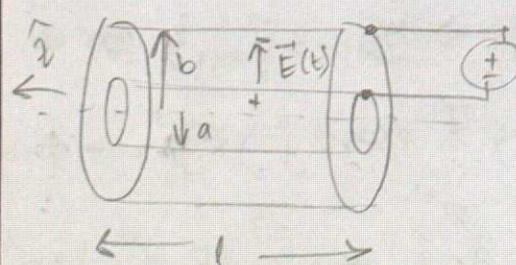
$$-3\pi$$

$$B_0 = 0.2 \text{ m}$$

$$l = 0.5$$

$$\therefore V_{12} = \frac{(3\pi)(0.2 \text{ m})(0.5)^2}{2} = -0.236 \text{ [V]}$$

6.15



$$V(t) = 50 \sin(120\pi t)$$

$$\text{Apply } \nabla \cdot \vec{D} = \rho_s$$

$$\iint_S \vec{D} \cdot d\vec{s} = \iiint_V \rho_s dV = Q_{enc} = +Q$$

$$2\pi r l D = Q, Q = CV, V = \int \frac{D}{\epsilon_0} dl = \frac{Q}{2\pi \epsilon_0 l} \ln(b/a)$$

$$\vec{D} = \frac{Q}{2\pi r l} \hat{r}$$

Since $V(t)$, then $Q(t)$ and $\therefore \vec{D}(t)$

$$\therefore V(t) = \frac{Q(t)}{4\pi \epsilon_0 l} \ln(b/a) \Rightarrow Q(t) = \frac{V(t) 2\pi \epsilon_0 l}{\ln(b/a)}$$

$$\therefore \vec{D}(t) = \frac{Q(t)}{2\pi r l} \hat{r} \Rightarrow \frac{4V(t) 2\pi \epsilon_0 l}{2\pi r l \ln(b/a)} = \frac{4V(t)}{\ln(b/a) r} = \frac{4V_0 \sin \omega t}{\ln(b/a) r} \hat{r}$$

From Ampere - Maxwell Law: $\oint_C \vec{H} \cdot d\vec{l} = \int_S \vec{J} \cdot d\vec{s} + \frac{d}{dt} \int_S \vec{D} \cdot d\vec{s} = I$

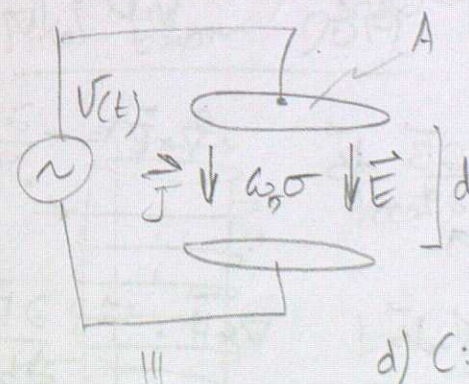
$$I = \oint_C \vec{H} \cdot d\vec{l} = 0 + \frac{d}{dt} \int_0^l \int_0^{2\pi} \frac{4V_0 \sin \omega t}{\ln(b/a) r} \hat{r} \cdot \hat{r} r d\phi dz$$

$$= \frac{d}{dt} \left[\frac{V_0 \sin \omega t 2\pi l}{\ln(b/a)} \right] = \frac{4\pi \epsilon_0 l \omega V_0 \cos \omega t}{\ln(b/a)} \text{ [A]}$$

$$l = 0.06, b = 0.01, a = 0.005, \omega = 120\pi, V_0 = 50, \omega = 9\omega_0$$

$$I = \frac{9\omega_0 2\pi (0.06)(120\pi)(50) \cos(120\pi t)}{\ln(0.01/0.005)} = 0.82 \cos(120\pi t) \text{ [uA]}$$

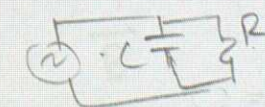
6.16 (Recall $V = Ed \Rightarrow E = \frac{V}{d}$) and assume all surfaces to be uniform



$$I_c = \iint_S \vec{J} \cdot d\vec{s} = JA = \sigma EA = \frac{\sigma VA}{d}$$

$$I_d = \frac{d}{dt} \iint_S \vec{D} \cdot d\vec{s} = \frac{d}{dt} \omega EA = \frac{d}{dt} \omega \frac{VA}{d} = \frac{\omega V(t) A}{d}$$

$$d) C: I_d = C \frac{dV(t)}{dt} \Rightarrow C = \frac{I_d}{V(t)} = \frac{\omega A}{d} = \frac{4\epsilon_0 \omega A}{0.005}$$



$$R: V = IR \Rightarrow R = \frac{V(t)}{I_c} = \frac{d}{\sigma A} = \frac{0.005}{2.5(0.4 \text{ m})}$$

$$A = 4 \text{ cm}^2 \times \left(\frac{1 \text{ m}}{100 \text{ cm}} \right)^2 = 0.4 \text{ m}$$

$$d = 0.005 \text{ m}, \omega = 4, \sigma = 2.5$$

$$\therefore C = 2.8 \text{ [PF]}$$

$$R = 5 \Omega$$

$$1 + sRC = 0$$

$$s = -\frac{1}{RC}$$

✓ 6.18

$$\vec{E} = \hat{z} E_0 \cos \omega t, \quad \omega = 81\omega_0, \quad \sigma = 4 \rightarrow \text{assume scalar integration}$$

$$I_c = \iint_S \vec{J} \cdot d\vec{s} = \sigma E(t) A \rightarrow J_c = \sigma E(t)$$

$$I_d = \frac{d}{dt} \iint_S \vec{D} \cdot d\vec{s} = \frac{d}{dt} A \epsilon_0 E(t) \Rightarrow J_d = \epsilon_0 \omega E'(t)$$

$$J_c = \sigma E_0 \cos \omega t \Rightarrow |J_c| = \sigma E_0$$

$$J_d = \epsilon_0 \omega E_0 \sin \omega t \Rightarrow |J_d| = \epsilon_0 \omega E_0$$

$$\left. \begin{array}{l} |J_c| = \sigma E_0 \\ |J_d| = \epsilon_0 \omega E_0 \end{array} \right\} \frac{|J_c|}{|J_d|} = \frac{\sigma}{\epsilon_0 \omega} = \frac{\sigma}{\omega \epsilon_0}$$

a) $\frac{\sigma}{\omega \epsilon_0} = \frac{4}{81(8.85 \times 10^{-12})2\pi(1k)} = 888079 \checkmark$

b) 888 ✓
c) 0.888 ✓
d) 0.00888 ✓

as ω increases, contribution from displacement current increases

1) $\oiint_S \vec{D} \cdot d\vec{s} = \iiint_V (\nabla \cdot \vec{D}) dV = \iiint_V \rho dV = Q_{enc} \quad \nabla \cdot \vec{D} = \rho_V$

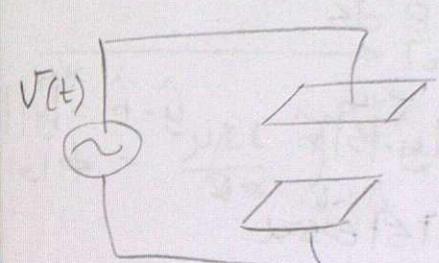
★ 2) $\oint_C \vec{E} \cdot d\vec{l} = \iint_S (\nabla \times \vec{E}) \cdot d\vec{s} = \iint_S -\frac{\partial \vec{B}}{\partial t} \cdot d\vec{s} \quad \nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$

3) $\oint_C \vec{H} \cdot d\vec{l} = \iint_S (\nabla \times \vec{H}) \cdot d\vec{s} = \iint_S (\vec{J} + \frac{\partial \vec{D}}{\partial t}) \cdot d\vec{s} \quad \nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}$

4) $\oiint_S \vec{B} \cdot d\vec{s} = \iiint_V (\nabla \cdot \vec{B}) dV = 0 \quad \nabla \cdot \vec{B} = 0$

ECE221 Stickel Lec 37

✓ Final Exam 2012



$$\nabla \times \vec{H} = \underbrace{\vec{J}}_{I_c} + \underbrace{\frac{\partial \vec{D}}{\partial t}}_{I_d} \quad (\text{Maxwell equ. 4})$$

$$I_c = \iint_S \vec{J} \cdot d\vec{s}, \quad I_d = \iint_S \frac{\partial \vec{D}}{\partial t} \cdot d\vec{s}$$

Given $C, V(t), \omega, \sigma, A$
Knowing $C = \frac{Q}{V}$, but $V = Ed \rightarrow E = \frac{V}{d}$ } Assuming scalar integrals ...

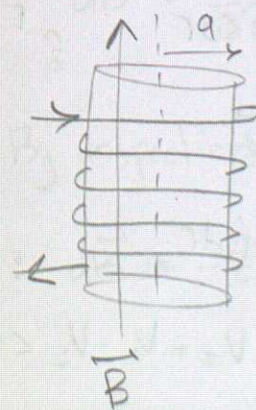
$$\frac{|I_c|}{|I_d|} = \frac{|\iint_S \vec{J} \cdot d\vec{s}|}{|\iint_S \frac{\partial \vec{D}}{\partial t} \cdot d\vec{s}|} = \frac{|JA|}{|\frac{\partial}{\partial t} \epsilon_0 E|} = \frac{|\sigma EA|}{|\frac{\partial}{\partial t} \epsilon_0 \frac{V(t)}{d}|} = \frac{|\sigma V(t)A|}{|\frac{\epsilon_0}{d} V'(t)A|} = \frac{|\sigma V(t)A|}{|\frac{\epsilon_0}{d} V'(t)A|}$$

$$= \frac{|\sigma V_0 \cos \omega t A|}{|\epsilon_0 \omega \sin \omega t|} = \frac{|\sigma V_0 A|}{|\epsilon_0 \omega|} = \frac{\sigma A}{\epsilon_0 \omega} = \frac{(2.12 \times 10^{-8})(3.2 \times 10^{-5})}{(4.22)(8.85 \times 10^{-12})(290)}$$

$\therefore \frac{|I_c|}{|I_d|} = 1.96 \checkmark$

Final Exam 2019 $\vec{B} = \hat{z} \frac{\mu I H}{l}, \quad a = 0.005, \quad l = 2\pi^2 \times 10^{-2}, \quad N = 20$
 $\mu = 5k\mu_0$

a)



Recall that inductance $L = \frac{N \Phi}{I} = \frac{N |B| A}{I}$

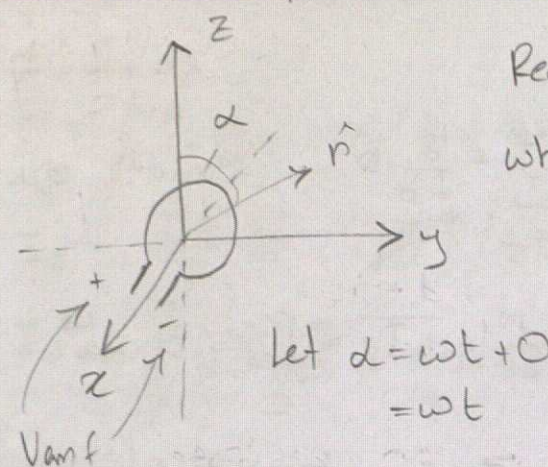
$$L = \frac{N |B| \pi a^2}{I} = \frac{N \mu I H \pi a^2}{l} = \frac{\mu N^2 \pi a^2}{l}$$

$$= \frac{(5k)\mu_0 (20)^2 \pi (0.005)^2}{(2\pi^2 \times 10^{-2})}$$

$L = 1 \text{ [mH]}$

Review Examples 2025

✓ 1)



Recall that $V_{\text{emf}} = -N \frac{d}{dt} \Phi_B$

where $\Phi_B = \iint_S \vec{B} \cdot d\vec{s}$

$= |\vec{B}| \hat{y} \cdot |\vec{s}| \hat{n}$ $\hat{y} \cdot \hat{n} = |\hat{y}| |\hat{n}| \cos \alpha$
 $= |\vec{B}| |\vec{s}| \cos \alpha$
 $= |\vec{B}| (\pi a^2) \cos \alpha$

$= |\vec{B}| (\pi a^2) \cos \omega t$

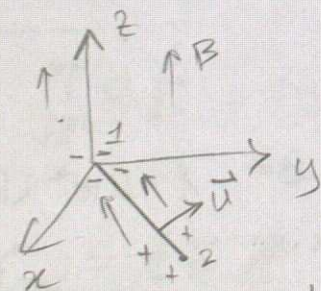
$\therefore V_{\text{emf}} = -1 \frac{d}{dt} [B \pi a^2 \cos \omega t] = B \pi a^2 \omega \sin \omega t$

$RPS \triangleq \frac{1 \text{ rot}}{1s} \Rightarrow \omega = \frac{RPS \text{ rot}}{s} \times \frac{2\pi \text{ rad}}{\text{rot}} \checkmark$ $\text{set} = 1$

$\therefore V_{\text{emf}} = B \pi a^2 RPS \cdot 2\pi, \therefore RPS = \frac{V_{\text{emf}}}{B \pi a^2 2\pi}$

$\therefore RPS = \frac{120}{(0.5 \times 10^{-4}) (\pi^2) (2) (0.05)^2} = 48.6 \frac{\text{million rot}}{s} \checkmark$

✓ 2)



$l = 0.5, \omega = \frac{90 \text{ rev}}{\text{min}} \times \frac{1 \text{ min}}{60s} \times \frac{2\pi \text{ rad}}{\text{rev}} = 3\pi$

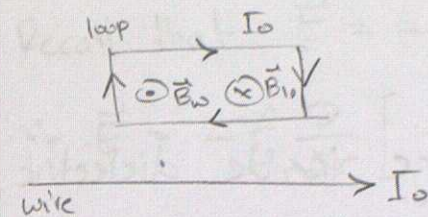
$\vec{B} = \hat{z} (0.2) [\text{mT}], \vec{u} = \hat{\phi} \omega r$ $\hat{z} \hat{r} \hat{\phi}$

$|V_{12}| = \int \vec{E} \cdot d\vec{\ell} = \int (\vec{u} \times \vec{B}) \cdot d\vec{\ell}$

$|V_{12}| = \int_0^l (\hat{\phi} \omega r \times B_0 \hat{z}) \cdot \hat{r} dr \Rightarrow \int_0^l \omega r B_0 \hat{r} \cdot \hat{r} dr$
 $= \omega B_0 \int_0^l r dr = \frac{\omega B_0 l^2}{2}, \text{ and since } V_1 < V_2, V_{12} = V_1 - V_2 < 0$

$\therefore V_{12} = -\frac{(3\pi)(0.2\text{m})(0.5)^2}{2} = -235 [\mu V] \checkmark$

3)



option 1 ✓

$\Phi = \iint_S \vec{B} \cdot d\vec{A} = \int_0^l \int_{d-w/2}^{d+w/2} \frac{\mu I}{2\pi r} \cdot dr dz$

$\Phi = \frac{\mu I l}{2\pi} \int_{d-w/2}^{d+w/2} \frac{1}{r} dr = \frac{\mu I l}{2\pi} \ln \left(\frac{d+w/2}{d-w/2} \right)$

4)

Recall that a perfect conductor is an equipotential surface. $\therefore \vec{E}$ always normal to surface $\rightarrow \vec{E}$

5)

[f]

6)

Recall the: $d\vec{B} = \frac{\mu I}{4\pi} \frac{d\vec{\ell}' \times (\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3}$

★

Consider seg. 1-2

$d\vec{\ell}' = \hat{x} dx, \vec{r} = \hat{z} \omega, \vec{r}' = \hat{z} x + \hat{y} y$

$\vec{r} - \vec{r}' = \hat{z} \omega - \hat{z} x - \hat{y} y = -x\hat{x} - y\hat{y} + \omega\hat{z}$

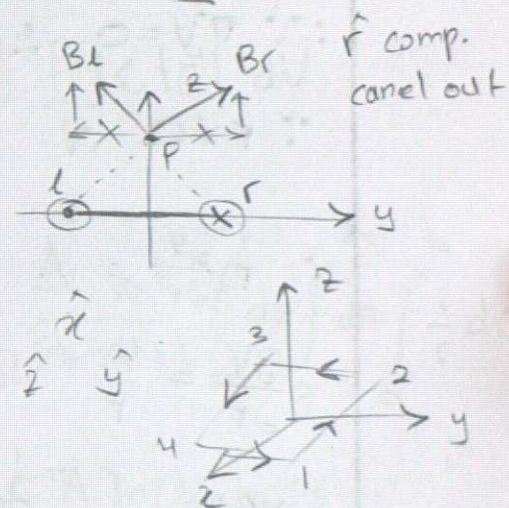
$|\vec{r} - \vec{r}'|^3 = (x^2 + y^2 + \omega^2)^{3/2}$

$\therefore d\vec{B} = \frac{\mu I}{4\pi} \frac{\hat{x} dx \times (-x\hat{x} - y\hat{y} + \omega\hat{z})}{(x^2 + y^2 + \omega^2)^{3/2}} = \frac{\mu I}{4\pi} \frac{-\hat{z} y dx - \hat{y} \omega dx}{(x^2 + y^2 + \omega^2)^{3/2}}$

By inspection and RHR, $\hat{y}$ comp. cancel out

$\therefore d\vec{B} = -\hat{z} \frac{\mu I y}{4\pi} \int_{-\omega}^{\omega} \frac{1}{(y^2 + z^2 + x^2)^{3/2}} dx = -\hat{z} \frac{\mu I y}{2\pi} \left[\frac{x}{(y^2 + z^2) \sqrt{(y^2 + z^2)^2 + x^2}} \right]_{-\omega}^{\omega}$

$\therefore \vec{B}(0,0)$



Question 1

a) Because we assume zero free charge inside dielectric, we recall the Laplacian $\nabla^2 V = 0$

Knowing Boundary conditions $V(a) = V_0$ and $V(b) = 0$:

$$\nabla^2 V = \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial V}{\partial r} \right) + 0 + 0 \quad \text{since we assume } V \text{ is function of } r \text{ only}$$

$$\therefore \nabla^2 V = 0 \quad \therefore \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial V}{\partial r} \right) = 0 \quad \therefore \frac{\partial}{\partial r} [A] = 0$$

$$\therefore r \neq 0 \quad \therefore \frac{\partial}{\partial r} [r \frac{\partial V}{\partial r}] = 0 \quad \therefore A \text{ must be a constant}$$

$$\therefore r \frac{\partial V}{\partial r} = A \quad \text{for } A \text{ a constant}$$

$$\frac{\partial V}{\partial r} = \frac{A}{r} \quad \text{for } r \neq 0$$

$$V(r) = \int \frac{A}{r} dr = A \ln|r| + C$$

Applying boundary cond.

$$V(a) = V_0 = A \ln(a) + C \quad (1)$$

$$V(b) = 0 = A \ln(b) + C \quad (2)$$

$$\text{from (2): } C = -A \ln(b) \Rightarrow (1): V_0 = A \ln(a) - A \ln(b) = A \ln(a/b)$$

$$\text{from (1): } A = \frac{V_0}{\ln(a/b)} \quad \text{and} \quad \therefore C = -\frac{V_0 \ln(b)}{\ln(a/b)}$$

Combining our constants, we see that

$$V(r) = A \ln|r| + C = \frac{V_0 \ln(r)}{\ln(a/b)} - \frac{V_0 \ln(b)}{\ln(a/b)}$$

$$V(r) = \frac{V_0}{\ln(a/b)} [\ln(r) - \ln(b)] \Rightarrow V(r) = \frac{V_0}{\ln(a/b)} \ln\left(\frac{r}{b}\right) [V]$$

b) Recall that $\vec{E} = -\nabla V = -\left(\frac{\partial}{\partial r} V \hat{r} + 0 + 0\right)$ since $V = V(r)$

$$\therefore \vec{E} = -\hat{r} \frac{\partial}{\partial r} \left[\frac{V_0}{\ln(a/b)} \ln(r/b) \right] \quad \frac{1}{r/b} \cdot \frac{1}{b} = \frac{1}{r} \cdot \frac{1}{b}$$

$$= -\hat{r} \frac{V_0}{\ln(a/b)} \left[\frac{1}{r/b} \cdot \frac{1}{b} \right] = -\hat{r} \frac{V_0}{\ln(a/b)} \cdot \frac{1}{r}$$

$$\therefore \vec{E} = -\frac{V_0}{\ln(a/b)} \frac{1}{r} \hat{r} [V/m]$$

d) $C = \frac{Q}{V}$, but $W_e = \frac{1}{2} CV^2 = \frac{1}{2} QV = \frac{1}{2} \iiint_V \epsilon |\vec{E}|^2 dV$

cap 1 ϵ_1

$$W_e = \frac{1}{2} \int_0^{L/2} \int_0^{2\pi} \int_a^b \epsilon_1 - \frac{V_0^2}{\ln^2(a/b)} \frac{1}{r^2} r dr d\phi dz = \frac{-\epsilon_1 V_0^2}{2 \ln^2(a/b)} \int_0^{L/2} dz \int_0^{2\pi} d\phi \int_a^b \frac{1}{r} dr$$

$$= -\frac{\epsilon_1 V_0^2 L 2\pi}{4 \ln^2(a/b)} \ln(b/a) = -\frac{\epsilon_1 V_0^2 L \pi}{2 \ln^2(a/b)} \ln(b/a) [J]$$

cap 2 ϵ_2 : $W_e = -\frac{\epsilon_2 V_0^2 L \pi}{2 \ln^2(a/b)} \ln(b/a) [J]$

$\therefore$ whole cable energy $= W_1 + W_2$

$$W_e = -\frac{\epsilon_0 V_0^2 L \pi \ln(b/a)}{2 \ln^2(a/b)} (\epsilon_1 + \epsilon_2) [J]$$

★ c) Recall $C = \frac{Q}{V} = \frac{\oint \vec{D} \cdot d\vec{s}}{-\int \vec{E} \cdot d\vec{r}} = \frac{\epsilon_0 \oint \vec{E} \cdot d\vec{s}}{\int \vec{E} \cdot d\vec{r}} \quad \text{--- (I)}$

Cap 1 (ϵ_1)

(I): $\epsilon_1 \oint \vec{E} \cdot d\vec{s} = \epsilon_1 \int_0^{L/2} \int_0^{2\pi} -\frac{V_0}{\ln(a/b)} \frac{1}{r} a d\phi dz = -\epsilon_1 V_0 a 2\pi$

Question 2

a) $I_0 = \int \vec{J} \cdot d\vec{s} = |\vec{J}| \int ds = J \frac{4\pi a^2}{2} = J 2\pi (R)^2$

$\therefore \vec{J} = \frac{I_0}{2\pi R^2} \hat{r} \quad [A/m^2]$

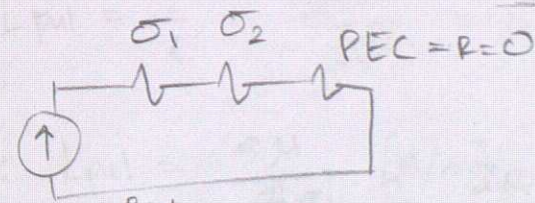
b) Recall that $\vec{E} = \frac{\vec{J}}{\sigma}$

$\sigma_1: \vec{E} = \frac{\vec{J}}{\sigma_1}$

$\sigma_2: \vec{E} = \frac{\vec{J}}{\sigma_2}$

$\therefore \vec{E} = \begin{cases} 0 & , 0 < R < R_1 \\ \frac{I_0}{\sigma_1 2\pi R^2} \hat{r} & , R_1 < R < t_1 \\ \frac{I_0}{\sigma_2 2\pi (R)^2} \hat{r} & , t_1 < R < t_2 \\ 0 & , R > t_2 \end{cases} \quad [V/m]$

c)



$R_1 = \frac{\int_{R_1}^{R_1+t_1} \frac{I_0}{\sigma_1 2\pi R^2} dR}{I_0} = \frac{\left[-\frac{1}{R}\right]_{R_1}^{R_1+t_1}}{\sigma_1 2\pi}$

$R_1 = \frac{l}{\sigma s} = \frac{V}{I} = \left| \frac{\int \vec{E} \cdot d\vec{l}}{\int \vec{J} \cdot d\vec{s}} \right| = \frac{\int \vec{E} \cdot d\vec{l}}{\sigma \int \vec{E} \cdot d\vec{s}}$

d) $P = I^2 R$

$= I_0^2 R$

$R_1 = \left| \frac{\frac{1}{R_1+t_1} - \frac{1}{R_1}}{\sigma_1 2\pi} \right|, R_2 = \left| \frac{\frac{1}{R_1+t_1+t_2} - \frac{1}{R_1+t_1}}{\sigma_2 2\pi} \right|$

$R = \left| \frac{\frac{1}{R_1} - \frac{1}{R_1+t_1}}{\sigma_1 2\pi} \right| + \left| \frac{\frac{1}{R_1+t_1} - \frac{1}{R_1+t_1+t_2}}{\sigma_2 2\pi} \right| \quad [2]$

Question 3

a) $\oint_C \vec{H} \cdot d\vec{\ell} = I_{enc} \Rightarrow \oint_C \vec{B} \cdot d\vec{\ell} = \mu I_{enc}$

inner J (volume current density) $\vec{J} = \frac{I}{\pi a^2} \hat{z}$ [A/m²]

outer J_s (surface current density) $\vec{J}_s = \frac{I}{2\pi b} (-\hat{z})$ [A/m]

for $0 < r < a$

$$2\pi r B = \mu J \pi r^2 \Rightarrow \vec{B} = \frac{\mu J}{2} r \hat{\phi} = \frac{\mu I}{2\pi a^2} r \hat{\phi}$$

$$\therefore \vec{B} = \frac{\mu I r}{2\pi a^2} (-\sin\phi \hat{x} + \cos\phi \hat{y}) \text{ [T]}$$

on xz plane, $\phi = 0$

$$\therefore \vec{B} = \frac{\mu I r}{2\pi a^2} \hat{y} \text{ [T]}$$

b) for $a < r < b$

$$2\pi r B = \mu I \Rightarrow \vec{B} = \frac{\mu I}{2\pi r} \hat{y} \text{ [T]}$$

c) for $r > b$

$$2\pi r B = \mu I_{enc} = \mu(I - I) = 0 \Rightarrow \vec{B} = 0 \text{ [T]}$$

d) $\Phi_B = \iint_S \vec{B} \cdot d\vec{s} = \int_a^b \int_0^l \frac{\mu I}{2\pi r} \hat{y} \cdot \hat{y} dz dr = \frac{\mu I l}{2\pi} \ln(b/a)$

$$\Phi_{Bpul} = \frac{\Phi_B}{l} = \frac{\mu I}{2\pi} \ln(b/a) \text{ [wb/m]} = \Phi_{Bpul}$$

e) $W_m = \frac{1}{2} \iiint_V \vec{B} \cdot \vec{H} dV = \frac{1}{2} \int_V \mu |\vec{H}|^2 dV = \frac{\mu}{2} \int_0^{2\pi} \int_0^l \int_0^a \frac{I^2 r^2}{4\pi^2 a^4} r dr dz d\phi$

$$= \frac{\mu I^2}{8\pi^2 a^4} 2\pi l \int_0^a r^3 dr = \frac{\mu I^2 l}{4\pi a^4} \left[\frac{1}{4} r^4 \right]_0^a = \frac{\mu I^2 l a^4}{16\pi a^4}$$

$$\therefore W_m = \frac{\mu I^2 l}{16\pi} \quad \therefore W_{mpul} = \frac{W_m}{l} = \frac{\mu I^2}{16\pi} \text{ [J/m]} = W_{mpul}$$

f) $L = \frac{2W_m}{I^2}$ and we already know $W_{m1} = \frac{\mu I^2 l}{16\pi}$

$$W_{m2} = \frac{\mu}{2} \int_0^{2\pi} \int_0^l \int_a^b \frac{I^2}{4\pi^2 r^2} r dr dz d\phi = \frac{\mu I^2 2\pi l}{2 \times 4\pi^2} \ln(b/a)$$

$$W_m = W_1 + W_2 = \frac{\mu I^2 l}{16\pi} + \frac{\mu I^2 l}{4\pi} \ln(b/a)$$

forgo!

$$L_{pul} = \frac{L}{l} = \frac{2W_m}{I^2 l} = \frac{2}{l I^2} \left(\frac{\mu I^2 l}{8 \cdot 16\pi} + \frac{\mu I^2 l}{24\pi} \right) = \frac{\mu}{8\pi} + \frac{\mu}{2\pi}$$

$$\therefore L_{pul} = \frac{5\mu}{8\pi} \text{ [H/m]}$$

Question 4

- a) Recall that $\oint_C \vec{H} \cdot d\vec{l} = I_{enc}$, by RHR: $\vec{H} = -\hat{x} |\vec{H}|$
 $2\pi r |\vec{H}| = I_{enc} \Rightarrow \boxed{\vec{B} = -\hat{x} \frac{\mu i(t)}{2\pi y} [T]}$
- b) $\Phi_B = \iint_S \vec{B} \cdot d\vec{S} = \int_{z_0-a/2}^{z_0+a/2} \int_{y_0-b}^{y_0+f(t)+b} -\hat{x} \frac{\mu i(t)}{2\pi y} \cdot (-\hat{x}) dy dz$ $\hat{y} \times -\hat{x} = +\hat{z}$
 $= \frac{\mu i(t)}{2\pi} \int_{z_0-a/2}^{z_0+a/2} dz \int_{y_0-b}^{y_0+f(t)+b} \frac{1}{y} dy$ $z_0 + \frac{a}{2} - z_0 + \frac{a}{2} = a$
 $\Phi_B = \frac{\mu i(t) a}{2\pi} \ln\left(\frac{y_0+f(t)+b}{y_0-b}\right) [Wb]$
- $V_{emf} = \int_A^B (\vec{u} \times \vec{B}) \cdot d\vec{l} = \int_{A'}^{B'} (f'(t) \hat{y} \times -\hat{x} \frac{\mu i(t)}{2\pi y}) \cdot \hat{z} dy$
 $= \int_{A'}^{B'} \frac{f'(t) \mu i(t)}{2\pi y} dy = \frac{f'(t) \mu i(t)}{2\pi} \int_{z_0-a/2}^{z_0+a/2} \frac{1}{y} dy$
 $= \frac{f'(t) \mu i(t)}{2\pi} \ln\left(\frac{\frac{2z_0-a}{2}}{\frac{2z_0+a}{2}}\right)$
- $V_{emf} = \frac{f'(t) \mu i(t)}{2\pi} \ln\left(\frac{2z_0-a}{2z_0+a}\right) [V]$
- c) $V_{emf} = \int_B^C (f'(t) \hat{y} \times -\hat{x} \frac{\mu i(t)}{2\pi y}) \cdot \hat{y} dy \Rightarrow \hat{z} \cdot \hat{y} = 0$
 $\therefore V_{emf} = 0 [V]$

- d) $i_2(t) = \frac{V_{emf}(t)}{R_T}$, $V_{emf}(t) = \iint_S -\frac{\partial}{\partial t} \vec{B}(t) \cdot d\vec{S} = -\frac{\partial}{\partial t} \Phi_B(t)$
 $-\frac{\partial}{\partial t} \Phi_B(t) = -\frac{\partial}{\partial t} \left[\frac{\mu i_1(t) a}{2\pi} \ln\left(\frac{y_0+f(t)+b}{y_0-b}\right) \right] g(t)$
 $= -\frac{\mu a}{2\pi} \frac{\partial}{\partial t} [i_1(t) g(t)] = -\frac{\mu a}{2\pi} (i_1'(t) g(t) + i_1(t) g'(t))$
 $g'(t) = \frac{1}{\frac{y_0+f(t)+b}{y_0-b}} \times \frac{f'(t)}{y_0-b} = \frac{y_0-b}{y_0+f(t)+b} \times \frac{f'(t)}{y_0-b} = \frac{f'(t)}{y_0+f(t)+b}$
 $V_{emf}(t) = -\frac{\mu a}{2\pi} \left[i_1'(t) \ln\left(\frac{y_0+f(t)+b}{y_0-b}\right) + \frac{i_1(t) f'(t)}{y_0+f(t)+b} \right]$
 $R_T = R \times (\text{total length } A'B'C'D') = R(4b+2a)$
 $\therefore i_2(t) = -\frac{\mu a}{2\pi R(4b+2a)} \left[i_1'(t) \ln\left(\frac{y_0+f(t)+b}{y_0-b}\right) + \frac{i_1(t) f'(t)}{y_0+f(t)+b} \right] [A]$

made error in orig. b) calculation $\int_{A'}^B \hat{z} dz$ $\leftarrow dz!!!$ not dy